# TERRESTRIAL SEDIMENT DEPOSITION IN RITTERBUSH POND: IMPLICATIONS FOR HOLOCENE STORM FREQUENCY IN NORTHERN VERMONT

A Thesis Presented

by

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#### ABSTRACT

This thesis provides a well-dated, high-resolution Holocene record of discrete sedimentation events in a New England lake. Ritterbush Pond is located in Eden, Vermont, within the northern Green Mountains, and is surrounded by a 2.2 km<sup>2</sup> watershed with steeply sloping, forested hillslides. The lake sediment record consists primarily of organic-rich gyttja that has accumulated since deglaciation (~12,000 14C yr BP). Unlike other New England lakes cored to construct pollen and deglacial chronologies, the sediments of Ritterbush Pond record episodic watershed erosion events as distinct layers of sand and silt. These inorganic layers reflect the occurrence of large hydrologic events in northern Vermont during the Holocene. The deposition of terrestrially-derived sediment in mountain lakes, and its potential use as a hydrologic proxy record, had received little prior attention in New England.

I collected and analyzed three continuous (4 to 6 m long) sediment cores, one from the lake center and two closer to the lake margin. I used a variety of analytical techniques to characterize the spatial and temporal distribution of the inorganic layers, and to investigate the mechanisms controlling sediment transport and deposition in the lake. The data produced for each core include records of litho-stratigraphy, organic carbon content (loss-on-ignition), X-radiograph and grayscale density, magnetic susceptibility, and paleomagnetism. Intervals of the cores were also analyzed for grain size, carbon / nitrogen ratios, stable carbon isotopes and percent charcoal. Fourteen radiocarbon dates were obtained on macrofossils and gyttja sampled from the three cores. I matched these cores to an existing, well-dated core (RT-2, 14 <sup>14</sup>C ages) and pollen chronology for Ritterbush

Pond (Lin, 1996).

The data support a terrestrial origin for inorganic layers, and suggest episodic, rapid deposition by density currents. The 0.1 to 10 cm-thick sand and silt layers cluster in three intervals, implying an increase in basin-wide hydrologic event frequency prior to 8650 cal yr BP, from 6840 to 6340 cal yr BP and 2620 to 2025 cal yr BP. Charcoal data do not support hillslope-clearing fires as a trigger for layer deposition, nor do pollen data show corresponding vegetation change. The chronology of inorganic sediment layers in Ritterbush Pond cores identifies 52 discrete depositional events, and is reported in both 14C

and calendar yr BP to facilitate comparison with other Holocene records.

Hydrologic event frequency and magnitude, as represented by layer spacing and thickness, has fluctuated throughout the Holocene. The Ritterbush watershed appears to have experienced two different hydrologic regimes. The predominant, quiet regime results in the deposition of layers less than 1 cm thick and alternates with a noisy regime (during the above intervals) where the thickest layers, representing larger events, are clustered. The only layer (1 cm thick) in the last 350 years of the chronology may have been deposited by the largest storm in Vermont's history (1927). This storm appears to represent the smallest magnitude storm necessary to mobilize sediment in the Ritterbush basin, implying that much larger magnitude storms are necessary to deposit the thicker, coarser inorganic layers. Antecedent soil conditions and sediment availability may also influence layer thickness, especially among the thickest layers.

The wider implications of the Ritterbush chronology are still uncertain, due to a lack of similar event records locally and regionally. The Ritterbush record suggests that severe storm events much larger than those historically witnessed, or currently planned for, have occurred in the Ritterbush basin, and perhaps across all of Vermont. The intervals of clustered layers may indicate larger-scale Holocene fluctuations in oceanic and atmospheric circulation patterns that shift northward the flows of tropical air needed to produce extreme

amounts of rainfall.

#### **ACKNOWLEDGEMENTS**

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#### **CHAPTER 1 - Introduction**

#### 1.1 Statement of Problem

In most New England lakes, the sediment record consists of organic debris (gyttja) deposited as a result of the primary productivity of aquatic organisms living in and around the lake, and sand, silt and plant matter eroded from the surrounding watershed. Traditional Holocene lake research has investigated the chemical, biological, and physical characteristics of the gyttja dominant in New England lake sediment records in order to interpret large scale climatic change since deglaciation (Davis and Jacobsen, 1985; Spear et al., 1994; Winkler, 1985a) and investigate internal lake dynamics (Almquist-Jacobson et al., 1992; Anderson et al., 1992; Davis and Ford, 1982). Excepting deposits correlated with the Younger Dryas (Thompson et al., 1996), the deposition of inorganic, terrestrially-derived sediment in mountain lakes and its potential use as a climate proxy has not received much attention in New England.

My research investigates distinct layers of sand and silt that disrupt the background aquatic sedimentation in Ritterbush Pond, a small lake in northern Vermont. Rare but severe erosional events, such as intense storms and forest fires, may briefly but drastically change the sedimentation dynamics of the watershed. The silt and sand layers provide a datable record of the episodic deposition of terrestrial material in the lake. The changing frequency (tens to thousands of years), and magnitude (0.1 cm- to 10 cm-thick) of inorganic sediment deposition in Ritterbush Pond, implies forcing by local or regional climate patterns.

Most paleoclimate reconstructions for New England suggest a simple three-fold division of post-glacial time: gradual warming after deglaciation, increased moisture in the middle Holocene with temperatures peaking around 6,000 <sup>14</sup>C yr. BP, and cooler

conditions in the past few thousand years (Lin et al., 1995; Spear et al., 1994; Webb et al., 1993). The pollen records show no large or systematic changes within these three periods. Using the distribution and magnitude of the depositional events in Ritterbush Pond, I employ a new approach to resolve changes in climate (storm frequency) as expressed by changes in watershed sedimentation dynamics.

#### 1.2 Overview of Thesis

The objectives of this thesis are to:

- 1) describe the lithology of Holocene sediment cores from Ritterbush Pond, a postglacial mountain lake in north-central Vermont (Figure 1.1),
- investigate the biogeochemical and physical properties of the sand and silt layers,
   and determine their spatial and temporal distribution in the cores,
- 3) propose sedimentologic mechanisms for the deposition of the inorganic layers,
- 4) use the inorganic layers to infer a Holocene history of erosion for the lake's drainage basin, and
- 5) compare the inferred hydrologic event chronology with existing Holocene records of local, regional, and global climate change.

I begin with a description of the sampling procedures and analytic techniques used in data collection (Chapter 2), and then present and analyze each data set individually (Chapter 3). I apply and interpret multiple data sets to correlate the cores, determine possible emplacement mechanisms for the inorganic layers, and construct the age model and event chronology (Chapter 4). In Chapter 5, I review and discuss the sedimentation dynamics and hydrologic event chronology of Ritterbush Pond, and compare it to other Holocene climate proxy records. I close with a statement of conclusions and suggestions for future work (Chapter 6).

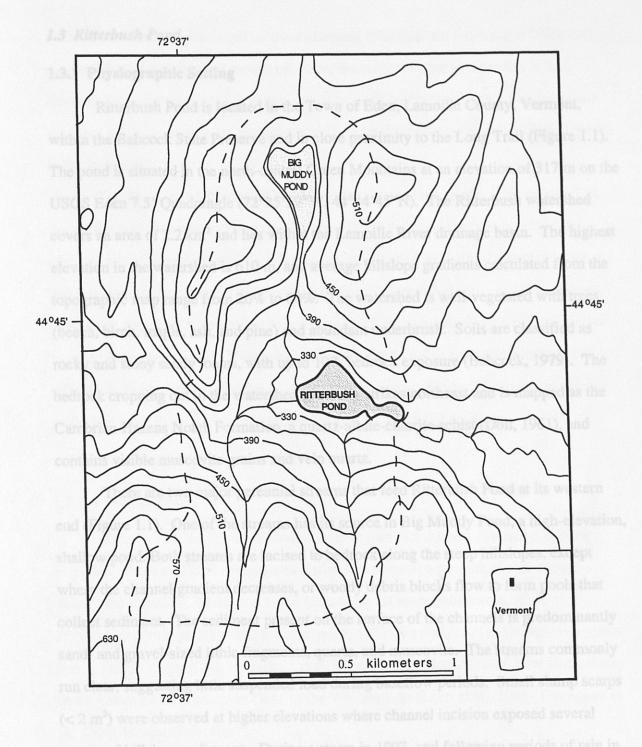


Figure 1.1 Ritterbush Pond Watershed, Eden, VT. Contour interval, 30 meters. Adapted from Eden and Hazens Notch USGS 7.5" topographic quadrangle maps, 1986.

#### 1.3 Ritterbush Pond

#### 1.3.1 Physiographic Setting

Ritterbush Pond is located in the Town of Eden, Lamoille County, Vermont, within the Babcock State Preserve and in close proximity to the Long Trail (Figure 1.1). The pond is situated in the north-central Green Mountains at an elevation of 317 m on the USGS Eden 7.5' Quadrangle (72°35'59"W, 44°44'45"N). The Ritterbush watershed covers an area of 2.2 km² and lies within the Lamoille River drainage basin. The highest elevation in the watershed is 610 m, and average hillslope gradients calculated from the topographic map range from 20% to 60%. The watershed is well-vegetated with trees (beech, birch, maple, ash, and pine) and abundant underbrush. Soils are classified as rocky and stony sandy loams, with up to 10% bedrock exposure (Babcock, 1979). The bedrock cropping out in the watershed generally strikes northeast and is mapped as the Cambrian Hazens Notch Formation, a quartz-albite-chlorite-schist (Doll, 1961), and contains visible muscovite grains and vein quartz.

There are two major perennial streams that feed Ritterbush Pond at its western end (Figure 1.1). One of the streams has its source in Big Muddy Pond, a high-elevation, shallow pond. Both streams are incised to bedrock along the steep hillslopes, except where the channel gradient decreases, or woody debris blocks flow to form pools that collect sediment. The sediment present on the surface of the channels is predominantly sand- and gravel-sized lithic fragments, quartz, and muscovite. The streams commonly run clear, suggesting little suspended load during baseflow periods. Small slump scarps (< 2 m²) were observed at higher elevations where channel incision exposed several meters of hillslope sediments. During a storm in 1997, and following periods of rain in 1997 and 1998, the stream water was brown and contained silt and clay-sized particles.

Several ephemeral channels that were dry in the summer and fall were actively delivering water and sediment to the lake after periods of rain and during spring snow

melt. Even when dry, the larger of these channels often contain fist-sized cobbles and can be followed hundreds of meters up slope; the origin of smaller channels is less discrete, but some originated in slump scarps (<1 m²) on the hillslopes. I observed no evidence for large-scale mass movement, such as landslide scarps or debris flow deposits in the watershed.

The shoreline of Ritterbush Pond is generally shallow, sandy, and vegetated on the southern end, dominated by a marshy area on the western side, and bounded by steeper and rockier slopes to the northeast. On the south and southeastern shores, there are abundant fallen trees and snags with their roots below lake level. At the eastern end of the lake the outlet is controlled by a shallow (0.5 m) bedrock sill on strike with other exposed bedrock outcrops. There does not appear to be active beaver damming. The lake water drains through a series of shallow marshy areas for over 2 km before it joins with Fryingpan Brook to become the White Branch of the Gihon River.

#### 1.3.2 Previous Work

Ritterbush Pond has been studied with regard to mountain glaciation in New England. Wagner (1970) investigated Ritterbush Pond as a possible cirque basin, identifying morainal, kettle, and kame features in the surrounding area. This interpretation was quickly disputed (Connally, 1971; Stewart, 1971). Evidence suggests that mountain glaciers did not remain in either the White Mountains of New Hampshire, or the Green Mountains at the close of the Wisconsinan (Loso et al., 1998; Thompson et al., 1996; Wright et al., 1997).

Sperling (1989) re-examined Wagner's work and cored the western end of the pond (water depth = 9.2 m), interpreting a basal radiocarbon age of  $10,730\pm200$  <sup>14</sup>C yr BP, at the base of the peaty core, as the age of deglaciation. However, Sperling's (1989)

pollen chronology suggests that the watershed was well-vegetated by that time, leading him to concur with Wagner (1970) that ice remained in the Ritterbush area after the recession of the Laurentide ice sheet. The reported core stratigraphy is not sufficiently detailed for comparison with the cores analyzed for this research, but does show three sand and gravel deposits directly below, and two additional sand deposits one meter above, peat dated at 4210±125 <sup>14</sup>C yr BP.

Ritterbush Pond was recently cored in conjunction with pollen and stable isotope research (Lin, 1996; Lini et al., 1995). A pair of overlapping, 2-inch Livingston cores (Cores RT-1 and RT-2) showed distinct variations in organic carbon content as approximated by loss-on-ignition (LOI). Numerous horizons of inorganic sediment (silt and sand) were visually identified within gyttja. Five <sup>14</sup>C dates were obtained from gyttja within the cores to construct a pollen chronology and deglacial climate and vegetation history. Lin (1996) hypothesized that the inorganic layers were deposited as a result of sediment resuspended by flood events. Her climate reconstruction, based solely on pollen, does not address the climatic implications of the horizons.

Subsequent examination of Cores RT-1 and RT-2 included stable isotope analysis and nine additional radiocarbon dates. Systematic variations in  $\delta^{13}$ C values with lithology were interpreted as indicating different organic source material for the gyttja (aquatic) and inorganic layers (terrestrial) (Lini et al., 1995). Three pairs of radiocarbon dates that bracket the thickest inorganic layers demonstrate that the terrestrially derived layers were deposited rapidly (Bierman et al., 1997). Bierman et al. (1997) correlate the deposition of inorganic layers in the Ritterbush cores to periods of hillslope erosion recorded by alluvial fans, and suggest a connection between inorganic sedimentation events, hillslope destabilization, and regional climate patterns. The stratigraphic log and loss-on-ignition (LOI) data for Core RT-2, the 14 radiocarbon dates, and the pollen

chronology will be used for comparison with three new Ritterbush Pond cores (Chapter 4).

#### CHAPTER 2 - Methods

I used a wide variety of methods to investigate sediment cores collected from Ritterbush Pond in order to gain a comprehensive understanding of sediment deposition and distribution in the lake. Most of the methods are routine for lake sediment core retrieval and analysis, and standard procedures required little modification. Additional procedures and equipment were tested and developed as needed. Detailed descriptions of the procedures I used are provided in Appendix A (Field Methods) and Appendix B (Lab Methods). This chapter presents background information on each analytical technique, an overview of the procedure used, and statistical parameters for each data set collected.

#### 2.1 Field Methods

#### 2.1.1 Bathymetry and Sediment Probing

Bathymetry and sediment thickness were measured at Ritterbush Pond in order to estimate sub-aqueous sediment distribution (D. Shaw, unpub. data, 1997) and to help determine locations for coring. Initial bathymetric measurements were made in 1995 (Lin, 1996). I checked and supplemented these measurements in January, 1997. The locations of over 60 holes augered in the ice were surveyed using an electronic total station set to a fixed benchmark on shore. Bathymetry was recorded as the distance from the sediment-water interface to the top of the ice using a weighted (200 g) measuring tape. Magnesium/zirconium core rods were then lowered through the ice and pushed into the sediment. The measured water depth subtracted from the total length of rod lowered provides a minimum estimate of sediment thickness.

#### 2.1.2 Coring

Three cores (Core 2, Core 3, and Core 4) were taken through 30 to 45 cm thick ice in January and March, 1997. All cores were obtained using a modified Reasoner coring device (Reasoner, 1993), a percussion corer fitted with a piston and a core-catcher (Figure 2.1). This device was chosen because it is lightweight, easily transportable, inexpensive to build and maintain, and can be used to obtain a large diameter (7.5 cm) continuous core. The corer is constructed of PVC pipe and has three parts: a core barrel holds the sediment, the core head attaches to the barrel and allows the core to be raised and lowered, and the core driver acts as a hammer to pound the core barrel into the sediment. The head and driver are secured at the ice surface with climbing ropes. The cores were retrieved using a pulley system anchored in the ice to obtain mechanical advantage. In the field, the 6 m-long PVC pipe encasing the core was cut into shorter lengths (1.7 to 3.0 m) for transport back to the University of Vermont (UVM).

#### 2.2 Laboratory Methods

I conducted most analyses at UVM between February 1997 and May 1998.

Paleomagnetic analysis equipment was used at the University of Rhode Island. Grain size was measured at Union College in New York. Radiocarbon sample preparation and dating were performed at Lawrence Livermore National Laboratory in California.

## 2.2.1 Core Processing

In the UVM laboratory, the three cores were cut into a total of eleven segments ranging in length from 1.24 to 1.62 m. I estimate that <1 cm of the core was disturbed by cutting the segments, and the record is therefore considered continuous. During May and

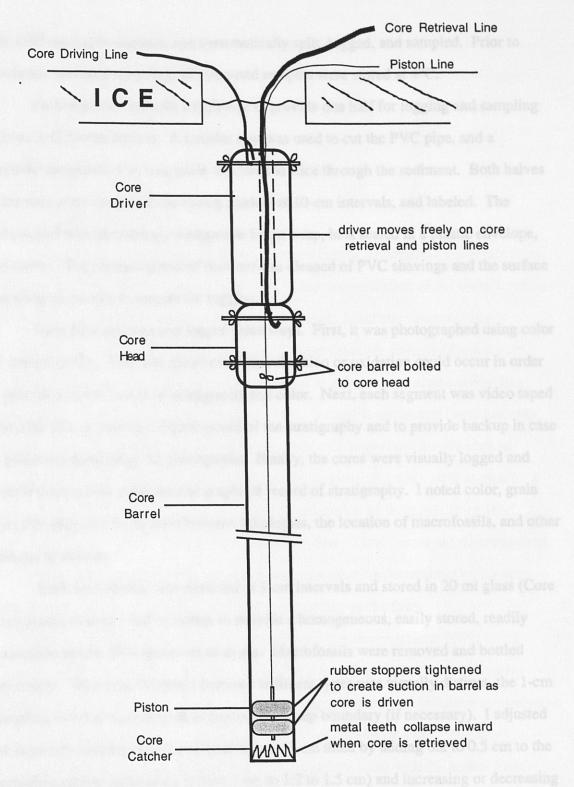


Figure 2.1 Reasoner coring device used to retrieve cores at Ritterbush Pond. A lightweight, PVC percussion corer with piston (Reasoner, 1995). Sketch adapted from J. Robison, unpublished figure, 1998.

June 1997 each core segment was systematically split, logged, and sampled. Prior to processing and after sampling, all cores and samples were stored at 4°C.

Each segment was split lengthwise to provide one half for logging and sampling and one half for the archive. A circular saw was used to cut the PVC pipe, and a specially designed 1.8 m long knife was used to slice through the sediment. Both halves of the core were measured, the casing marked at 10-cm intervals, and labeled. The archive half was immediately wrapped in Saran wrap, heat sealed in a plastic envelope, and stored. The remaining half of the core was cleaned of PVC shavings and the surface was scraped smooth to prepare for logging.

Each core segment was logged three ways. First, it was photographed using color 35 mm print film. This was done before discoloration or oxidation could occur in order to provide a visual record of stratigraphy and color. Next, each segment was video taped with Hi8 film to provide a digital record of the stratigraphy and to provide backup in case of problems developing the photographs. Finally, the cores were visually logged and sketched to provide a written and graphical record of stratigraphy. I noted color, grain size, lithology, the boundaries between lithologies, the location of macrofossils, and other features of interest.

Each section was then dissected at 1-cm intervals and stored in 20 ml glass (Core 2) or plastic (Cores 3 and 4) bottles to provide a homogeneous, easily stored, readily accessible sample for subsequent analyses. Macrofossils were removed and bottled separately. Where the boundary between sediment types was visually distinct, the 1-cm sampling interval was adjusted to capture the sharp boundary (if necessary). I adjusted the interval primarily for silt and sand layers >3 cm thick by adding 0.2 to 0.5 cm to the preceding sample (increasing it from 1 cm to 1.2 to 1.5 cm) and increasing or decreasing the subsequent interval by 0.2 to 0.5 cm respectively. Boundaries less than 0.1 cm off the sampling boundary were incorporated into the appropriate sample without adjustment to

the recorded depth. Sampling intervals range from 0.5 cm to 1.5 cm. Over 1700 sediment and macrofossil samples were collected from the three cores and stored at 4°C. During sampling, subtle changes in sediment type not evident from surface logging were noted on the stratigraphic logs.

# 2.2.2 Magnetic Susceptibility

Magnetic susceptibility is a relative measurement of susceptibility of a sample to magnetization. The value, reported in SI units, is the magnetization of the sample (gauss) divided by the strength of the magnetic field (oersteds). Magnetic susceptibility is commonly used to identify changes in lithology when there are distinct differences in magnetic mineral content, and is routinely reported as a down core measurement in marine and lake sediment studies (Dearing, 1986). Inorganic sediments (sand and silt) have a higher susceptibility than organic sediments, and magnetic minerals such as magnetite will have higher susceptibility than non-magnetic minerals such as quartz. I use peaks in magnetic susceptibility to identify the location of inorganic (magnetic) layers within the primarily organic (non-magnetic) core. These peaks are superimposed on a background signal from the gyttja and peak magnitude is determined by the type, concentration, and amount of magnetic material making up the layer.

I initially measured whole core susceptibility (February, March 1997) using a Sapphire magnetic susceptibility meter and coil, on loan from P.T. Davis of Bentley College in Massachusetts. The coil generates a magnetic field and measures the response of the material within the coil. The Sapphire coil has a width of 4 cm, and each measurement integrates over approximately 10 cm of the core, with the center 4 cm influencing the measurement most strongly. Susceptibility was recorded at 3-cm increments down each unsplit core. Initial runs included empty PVC pipes (blanks) that

demonstrated linear drift of approximately 10% of the background measurement with time (Figure 2.2A). I compensated for this drift by taking free air measurements before and after each core segment was run to determine the magnitude and direction of the drift and adjust the susceptibility records accordingly by linear interpolation. Susceptibility measurements were repeated three times for each segment, stacked, and compiled to create a master record for each core with a standard deviation of 5%.

I repeated susceptibility measurements in February 1998 using a Bartington Magnetic Susceptibility Meter (MS2) with higher resolution (integration over 4 cm) and an automated core-logging system. Split (half-cores) were run once at 1-cm increments and corrected for slight linear drift (<1%) using free air measurements as detailed above. Repeated runs of core segments showed a standard deviation of 1%.

Comparison of the two techniques used to measure magnetic susceptibility shows a strong positive correlation (Figure 2.2B). The Sapphire data, at 3-cm resolution and on whole-cores, show the same peaks as the Bartington measurements on half-cores almost a year later, implying no degradation of the magnetic signal due to core storage (Figures 2.2C, D). The 1-cm resolution Bartington data are presented in Chapter 3, and subsequently used for comparison with other high-resolution data.

# 2.2.3 Paleomagnetic Measurements

Paleomagnetic secular variation (PSV) is the short-period, small-amplitude change in the earth's magnetic field and is measured by the natural remanent magnetism (NRM) (declination, inclination, and intensity) of earth materials (Lund, 1993; King et al., 1983). Lake sediments have been shown to be excellent recorders of this signal where the dominant sedimentation mechanism is slow settling of clay-sized particles, allowing detrital magnetite to align with the earth's magnetic field. Rapid deposition,

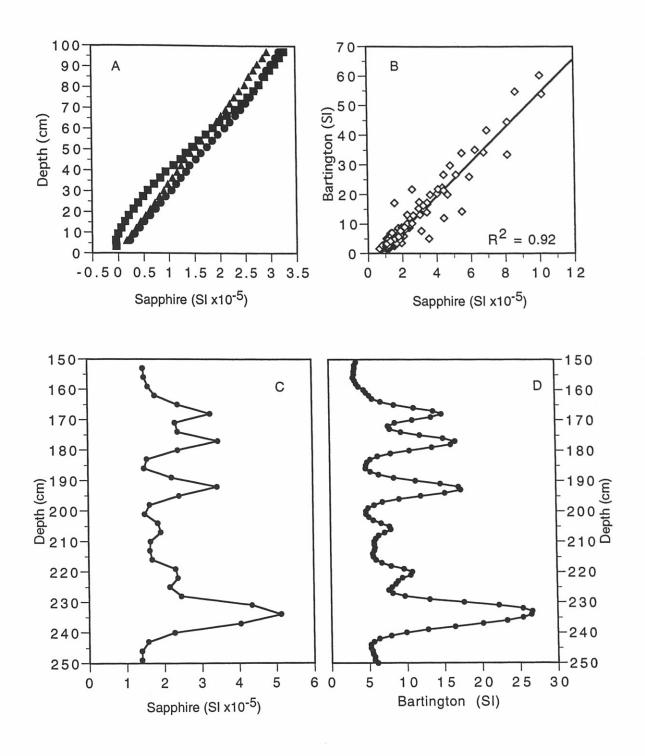


Figure 2.2 Comparison of Sapphire and Bartington magnetic susceptibility data. A) Linear drift of Sapphire signal over 1 m blank core, B) data show good correlation between methods, C) Sapphire, and D) Bartington data over a meter of Core 2 (150 cm to 250 cm), showing higher resolution of Bartington analysis.

reworking of sediment, or bioturbation will obscure the magnetic signal (Verosub, 1977). Reliability criteria, such as the length and continuity of the record, and the stability and reproducibility of the signal, have been established to determine the suitability and robustness of paleomagnetic records for use as PSV records (Thompson, 1985). Secular variation of both declination and inclination has been used to correlate lake sediment records from deglacial and Holocene lakes in New England, North America, and Europe (Lund, 1996; Peck et al., 1996; Ridge et al., 1990).

I performed paleomagnetic analysis on the Ritterbush Pond cores as a potential tool for correlating cores within the lake, and comparing the Ritterbush Pond record with other dated Holocene lake sediment records. I measured NRM for all archived core segments in December 1997, on a cryogenic magnetometer at the Paleomagnetic Laboratory at the University of Rhode Island, under the direction of John King and John Peck. Each core section was demagnetized at 10 mT to remove the unstable portion of the paleomagnetic signal (Zijdeveld, 1964). Declination (degrees), inclination (degrees), and intensity (emu cm<sup>-3</sup>) measurements were taken at 2-cm increments. The magnetometer integrates over approximately 14 cm for each measurement. Average variations for replicate samples are reported to be as great as 8 degrees in inclination and declination (Peck et al., 1996; King et al., 1983).

The original orientation of each core segment with respect to north, and rotation relative to the adjacent core segments, were not recorded, causing significant shifts in measured declination and inclination within and between cores. Continuous records were compiled for each core by adjusting all values for a core segment by the magnitude of the offset from the adjacent segment. Each core record was then normalized to the mean value for the core to allow for comparison between cores.

## 2.2.4 X-radiography

The differential absorption of X-rays by sample material produces a graphic image depicting changes in material type. The absorption of X-rays is dependent on the density (packing and water content) and composition (atomic number) of the sample material (Axelsson, 1983). Marine and lake sediment studies often use x-rays of cores to document and interpret sedimentary structures and for the correlation of laminations between cores (Van Weering and Van Iperen, 1984). X-rays are absorbed by inorganic matter (silt and sand), but pass through organic matter (gyttja), resulting in a black and white picture of core stratigraphy. I used X-radiographs to provide a visual image of the un-opened cores, to identify small-scale structures and changes in lithology not visible to the naked eye, and to construct X-ray density profiles based on the scanned, grayscale images.

I was trained to use the X-ray machine, an apparatus primarily used for medical research, at the UVM Radiation Safety Lab in May, 1997. All eleven core segments were X-radiographed in overlapping, 30-cm sections with depth increments (20 cm) marked with lead. The X-rays are projected from a point source above the table, pass through the cores, and expose film inserted beneath the cores. The conical scattering of the X-rays from the point source slightly distorts the resulting image away from the point directly below the X-ray source. I calculated the degree of distortion for each image by measuring the resulting distance on the developed film between the lead markers.

Distortion was consistent at 2 cm per 30 cm, and was corrected as a linear function of distance away from the center of the image.

I scanned the X-radiographs from Core 2 in order to obtain images that could be digitally analyzed and reproduced. Using a transparency scanner, each image was imported into *Adobe Photoshop 3.0*, and adjusted, using a linear stretch, for the measured distortion of the image. Scanner parameters, such as intensity and resolution, were kept

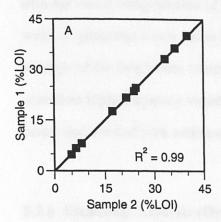
constant for all images. The images were compiled in *CANVAS 3.45*, using the graphic logs to accurately match the images, to create a continuous, graphic record for each segment. *NIH image* was used to develop gray-scale (256 levels) density data for the complete record.

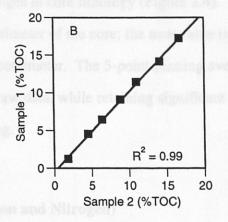
### 2.2.5 Loss-on-ignition (LOI)

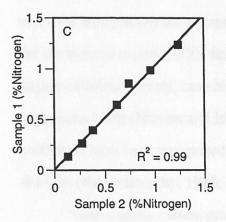
Loss-on-ignition (LOI) is measured as a proxy for organic carbon content.

Percent LOI is calculated as the percent weight lost when a dried sample is combusted (Berglund, 1986). Combustion of a sediment sample ashes the organic matter and releases CO<sub>2</sub>. High loss-on-ignition (LOI) values are associated with organic-rich sediments such as gyttja and peat. Low LOI values indicate inorganic sediments (sand and clay). Loss-on-ignition records are routinely reported in lake and marsh research to characterize lithologic changes in sediment cores with depth (Anderson et al., 1992; Peteet et al., 1990; Thompson et al., 1996). Published LOI records for New England were developed primarily in conjunction with pollen research (Davis and Jacobsen, 1985; Spear, 1989; Spear, 1993). The resolution of these records is rarely better than one sample every 10 cm.

I use LOI to detect down-core trends in organic-matter content, to estimate average carbon content of both gyttja and inorganic layers, and to delineate the boundaries of the inorganic layers. Aliquots from each sample bottle for all three cores were weighed, dried, weighed a second time, combusted at  $450^{\circ}$ C for 2 hours, and weighed a final time. Prior to weighing, the samples cooled to room temperature in open air for 1 hour (P.T. Davis, written comm., 1997). From these measurements, I calculated percent water loss and percent weight loss (LOI) for each centimeter of all three cores. The precision (1 sigma) of the measurement was quantified at  $\pm$  0.05% LOI by running replicates of ten samples spanning the range of LOI values (Figure 2.3A).







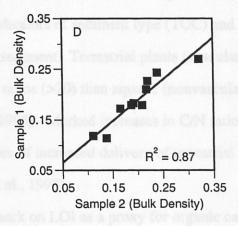


Figure 2.3 Replicate analyses for A) LOI, B) TOC, C) total nitrogen, and D) bulk density.

The centimeter-resolution LOI data are used for comparison with other high-resolution data sets. I have also used a 5-point running average or window to smooth the data for visual interpretation of general changes in core lithology (Figure 2.4). The window generates a new value for each centimeter of the core; the new value is the average of the five values centered on that centimeter. The 5-point running average smoothes high-frequency variations in the raw data, while retaining significant individual peaks that are lost with additional smoothing.

#### 2.2.6 Elemental Analysis (Organic Carbon and Nitrogen)

Elemental analysis measures the percentage of an element (N or C) in a sample by analyzing the gas produced when the sample is combusted. Total organic carbon (TOC) and total nitrogen (N) are interpreted as indicators of sediment type (TOC) and the source for the organic material (C/N ratio) in the sediment. Terrestrial plants (vascular), due to a higher cellulose content, have higher C/N ratios (>20) than aquatic (nonvascular) organisms (<10) (Meyers and Ishiwatari, 1995). Marked increases in C/N ratios in lake sediments have been interpreted as episodes of increased delivery of terrestrial material to the lake (Krishnamurthy, 1986; Meyers et al., 1993).

Total organic carbon provides a check on LOI as a proxy for organic carbon content. Organic molecules are composed of carbon, hydrogen, oxygen, nitrogen, and other minor constituents, with the ratio of elements determined by the type of organic material, and the amount of decomposition that has occurred. Carbon (TOC) generally represents 40% to 60% of the weight of organic material combusted by loss-on-ignition (Bengtsson and Enell, 1986).

I measured total organic carbon and total nitrogen for Core 2 using a CE NA2500 Elemental Analyzer in the Environmental Stable Isotope Laboratory at UVM. An

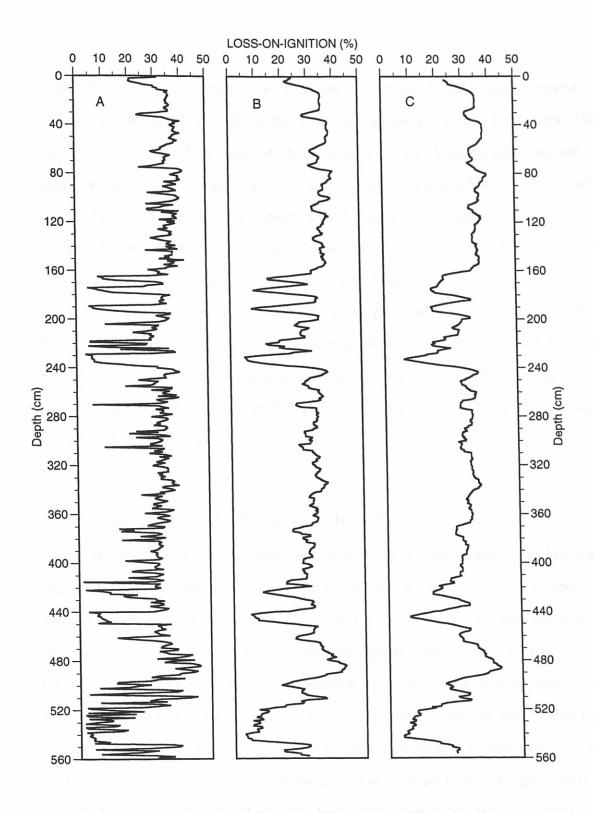


Figure 2.4 Smoothing LOI data for Core 2. A) Raw data, B) 5-point and C) 9-point running averages progressively smooth the data. The 5-point running average maintains resolution while providing enough smoothing to allow for ease of comparison with other records.

aliquot from each sample bottle was weighed into a silver capsule and treated to remove carbonate by adding a drop of HCl to the capsule and allowing it to react for 2 hours. The capsules containing the dried sample were then loaded into the Elemental Analyzer, and combusted at 1020°C. The gas was separated on a gas chromatograph (GC) column and measured by thermal conductivity to produce an elemental chromatogram for carbon and nitrogen. The area under the chromatogram peak and the weight of the original sample were used to calculate percent organic carbon and percent nitrogen.

Drift of the calibration was checked by running 2 standards (peach leaves, NIST #1547) at the start, end, and after every 20 samples of each run. When standards deviated >1% from the expected value, new samples were prepared and analyzed. Replicate samples (Figures 2.3B,C) from 7 depths give a standard deviation of  $\pm$  0.1% for carbon and  $\pm$  0.05% for nitrogen.

# 2.2.7 Charcoal Analysis (Nitric Acid Digestion)

The presence of charcoal particles in modern and Holocene lakes, alluvial fans, and marshes has been utilized to document forest fire-related sedimentation events (Clark, 1988; Whitlock and Millspaugh, 1996). Transport of charcoal and associated debris is often accelerated after a fire due to the removal of vegetation and destabilization of hillslopes (Meyer and Wells, 1997). Deposition and preservation of charcoal particles in lake sediments is influenced by formation temperature, particle size, and water chemistry (Vaughan and Nichols, 1995). Increases in the measured charcoal content of sediments, or the presence of visible charcoal particles, is used to construct local and regional fire-history chronologies (Millspaugh and Whitlock, 1995; Clark, 1988; Winkler, 1985). Visual techniques for charcoal identification require thin section preparation or sieving of samples and investigation under a microscope (Clark, 1988). I used a nitric acid digestion

technique, shown to correlate well with visual identification, to measure percent charcoal in the sediment (Winkler, 1985b).

I analyzed 122 samples from eight intervals in Core 2 to test for association between fire-generated charcoal particles and inorganic layers. Five of the intervals included the thickest inorganic layers in the core. Three intervals were composed entirely of gyttja to provide an estimate of the background fluctuation of charcoal content. Each sample was treated with concentrated nitric acid to oxidize organic material, carbonate, and pyrite, leaving the inorganic material and charcoal particles as residue. Traditionally, this residue is then combusted at 450°C to remove charcoal, and the loss in weight calculated as percent charcoal. My initial tests of this method gave very low and occasionally negative values for charcoal mass, suggesting that my equipment (balance, crucibles) were not accurate enough to measure small weight changes or that there was negligible carbon, charcoal or otherwise, associated with the treated samples. To increase the precision of my measurements, I combusted the residue in the Elemental Analyzer (procedure detailed above and in Appendix B) and recorded TOC as a percentage of the digested sample. This modification produced percent charcoal values comparable to expected values for lake sediments (Winkler, 1985b). Replicate samples were not run.

# 2.2.8 Stable Carbon Isotope Analysis

Stable carbon isotope composition ( $\delta^{13}$ C, relative to PDB standard) of organic matter depends on the CO<sub>2</sub> source, photosynthetic pathway (C3, C4, CAM), and subsequent diagenetic processes (Fogel and Cifuentes, 1993). Fluctuations in the  $\delta^{13}$ C values of lake sediments can be interpreted as changes in organic matter source, lake productivity, and watershed vegetation (Meyers and Ishiwatari, 1995; Winkler, 1994). The organic carbon associated with terrestrial and aquatic sediments in Ritterbush Pond has

been shown to have different stable carbon isotope values (Lini et al, 1995). I use stable carbon isotopes to investigate the degree of mixing between terrestrial and aquatic sediments associated with the deposition of the inorganic layers. Gyttja and macrofossil samples were also analyzed in conjunction with radiocarbon dating (section 2.2.11).

I chose two inorganic layers in Core 2 for  $\delta^{13}$ C analysis, and sampled each centimeter comprising the layer, and one centimeter of gyttja above and below the layer, for a total of 20 samples. Each sample was washed with 1N HCl to remove carbonate, and combusted in quartz tubes with copper and copper oxide at 900°C to produce  $H_2O$ ,  $N_2$  and  $CO_2$ . The  $CO_2$  was isolated on a vacuum line for mass spectrometric analysis. The mass spectrometer (VG SIRA II) measures the ratio of  $^{13}$ C and  $^{12}$ C necessary to calculate  $\delta^{13}$ C with a standard deviation of 0.1%.

#### 2.2.9 Grain-Size Analysis

Grain size is routinely measured in paleoecological studies as an aid in interpreting depositional environments (Aaby and Berglund, 1986). Disruption of the low-energy, deep-water environment of a lake by increased stream flow or sediment load is often recorded by an erosional contact or increase in average sediment grain size (Allen and Collinson, 1986). Variations in grain size within a single inorganic deposit can be used to determine the direction of transport and depositional mechanism for the layer (Gorsline, 1984). Turbidity current deposits, for example, tend to thin and fine away from their source (Walker, 1967), and produce a characteristic vertically graded sequence (Bouma, 1962). I use grain-size analysis to confirm estimates of relative grain size made during visual logging, to trace changes in the grain size of an individual inorganic layer, and to verify the graded nature of the thickest layers.

I chose five representative inorganic layers to sample at a 1 cm interval: three layers from Core 2 and one layer each from Cores 3 and 4. I prepared the resulting 50 samples at UVM for analysis by treating them with HCl to remove carbonate,  $H_2O_2$  to remove organic matter, and NaOH to remove biogenic silica. The samples were then analyzed with a Coulter Laser Diffraction Unit (LS 230) at Union College, NY under the direction of Donald Rodbell. Each grain size diffracts the laser at a characteristic angle, allowing the frequency at which each grain size occurs in the sample to be calculated. Replicate samples produced a standard deviation in mean grain size of  $\pm 5\%$ .

#### 2.2.10 Bulk Density

Bulk density, mass per unit volume, is controlled by the composition (lithology) of the sediment, the amount of pore space between sediment grains, and initial water content (Bendtsson and Enel, 1986). In lake sediment cores, autocompaction, the compaction of sediments under their own weight, results in a decrease of pore space and, when lithology is homogeneous, a systematic increase in density with depth (Baldwin, 1971). To interpret changes in accumulation of sediment through time, the apparent rate of sedimentation (cm yr<sup>-1</sup>) must be adjusted for down-core changes in density (g cm<sup>-3</sup>) in order to calculate the accumulation rate (g cm<sup>-2</sup> yr<sup>-1</sup>). In cores containing interlayered lithologies, differential compaction is accounted for by treating each lithology individually. Organic-rich sediments may compact to 20% of their original thickness; sand layers tend to maintain their original density (Baldwin, 1971; Pizzuto and Schwendt, 1997).

I estimated the bulk density of eighteen samples from ten locations in Core 2 to determine changes in density as a function of depth, and to calculate accumulation rates. Representative gyttja samples (1 cm³) were removed from the archive half of the core,

dried overnight, and weighed. I avoided sampling inorganic layers. Replicate samples were analyzed at eight of the ten locations and have an average standard deviation of 7% (Figure 2.3D).

#### 2.2.11 Radiocarbon Dating

Radiocarbon (14C) is produced in the upper atmosphere through the interaction of <sup>14</sup>N with cosmic radiation, and incorporated into living organisms through photosynthesis. The exponential decay of <sup>14</sup>C, with a half-life of 5730 yr, is used to date organic matter by calculating the time elapsed since the death of the organism(s). Accelerator Mass Spectrometer (AMS) techniques measure the <sup>14</sup>C/<sup>13</sup>C ratio in a sample, and calculate a radiocarbon age based on the assumptions that 1) the original <sup>14</sup>C in the sample was in equilibrium with the atmosphere concentration, and 2) atmospheric <sup>14</sup>C concentration has been constant over time (Olsson, 1986; Nelson, 1986). However, both of these assumptions have been shown to be untrue, requiring adjustment of radiocarbon ages to reflect more accurately calendar years (Tyler, 1997). Isotopic fractionation, resulting in disequilibrium of the organic matter with atmospheric <sup>14</sup>C, is corrected for by measuring the  $\delta^{13}$ C ( $^{13}$ C/ $^{12}$ C) value of the sample (Donahue et al., 1990). Deduced variation in paleo-atmospheric CO<sub>2</sub> is used to calibrate radiocarbon years to an equivalent age in calendar years (Stuiver and Reimer, 1993). I use AMS radiocarbon dates, adjusted for isotopic fractionation and calibrated to calendar years, to confirm the stratigraphic correlation of cores, to provide age control on deposition of inorganic layers, and to calculate sediment accumulation rates for Core 2.

Samples of gyttja and macrofossils, were removed from the refrigerated sample bottles for analysis. In March 1998, I prepared eight samples for AMS dating at Lawrence Livermore National Laboratory, according to standard procedures and under the direction of John Southon. The samples were washed in HCl and NaOH to remove

carbonate and humic acids, and then combusted with CuO in quartz tubes to produce  $CO_2$  gas. The gas was isolated and graphitized on a vacuum line. The graphite was packed into targets for analysis by accelerator mass spectrometry (Nelson et al., 1986). Additional samples were sent to Lawrence Livermore for preparation and processing in September 1997 (2 samples) and June 1998 (4 samples). For 7 samples, acid/base treated sample material was measured for  $\delta^{13}C$  at UVM. When treated sample was unavailable,  $\delta^{13}C$  was estimated as the average of the measured values, -31% for gyttja, and -28% for macrofossils.

The agreement of radiocarbon dates of gyttja and macrofossils from the same stratigraphic horizon was tested at Ritterbush Pond (Bierman et al., 1997). A macrofossil was dated at 8450±60 <sup>14</sup>C yr BP, while the surrounding gyttja was dated at 8900±40 <sup>14</sup>C yr BP, resulting in an age difference of 450 years. Bierman et al. (1997) suggest that the young macrofossil age is due to the lake reservoir effect, and/or sinking of the macrofossil through the unconsolidated gyttja. The lake reservoir effect is caused by a low <sup>14</sup>C/<sup>12</sup>C ratio in the dissolved CO<sub>2</sub> used by the aquatic plants comprising the gyttja. The low <sup>14</sup>C/<sup>12</sup>C ratio is attributed to the introduction of old, <sup>14</sup>C depleted carbon from bedrock, basal sediments, or groundwater (Olsson, 1986). Bulk dates of carbonate-free gyttja have been shown to be hundreds of years (400 to 500 yr) older than AMS dates of terrestrial plant fragments (Wohlfarth et al., 1993). Sinking of the macrofossil may contribute to the observed offset, and would vary with the density of the gyttja at the sediment / water interface and the mass of the macrofossil. Sinking is unlikely, however, to achieve independently the entire observed offset. I accounted for the offset documented at Ritterbush Pond by subtracting 450 <sup>14</sup>C yr from all gyttja ages.

Radiocarbon dates were calibrated to calendar years using CALIB rev3.0.3A (Stuiver and Reimer, 1993). I chose to smooth the bi-decadal tree ring records used for calibration with a 40-yr running average, as each 1 cm sample dated represents at least

20-yr of gyttja accumulation (Taylor, 1997). The analysis results in intercepts (where the <sup>14</sup>C date crosses the calibration curve) and 68% confidence ranges (where the endpoints of the 1 sigma range cross the calibration curve). Due to the shape of the calibration curve, calibration may result in more than one intercept and/or more than one range for some radiocarbon ages. To determine a single date for use in age modeling, I interpret the calibration based on the predicted values (intercepts) and the statistical significance of the standard deviation (range) of the data set. Where one range is reported, I use the intercept or average of the intercepts; where two ranges are reported, I use a weighted average of intercepts, or weighted average of range midpoints where no intercept is reported (Eden and Page, 1997). My best estimate for each calendar age equivalent of each <sup>14</sup>C age is reported to the nearest decade.

### CHAPTER 3 - Data Presentation

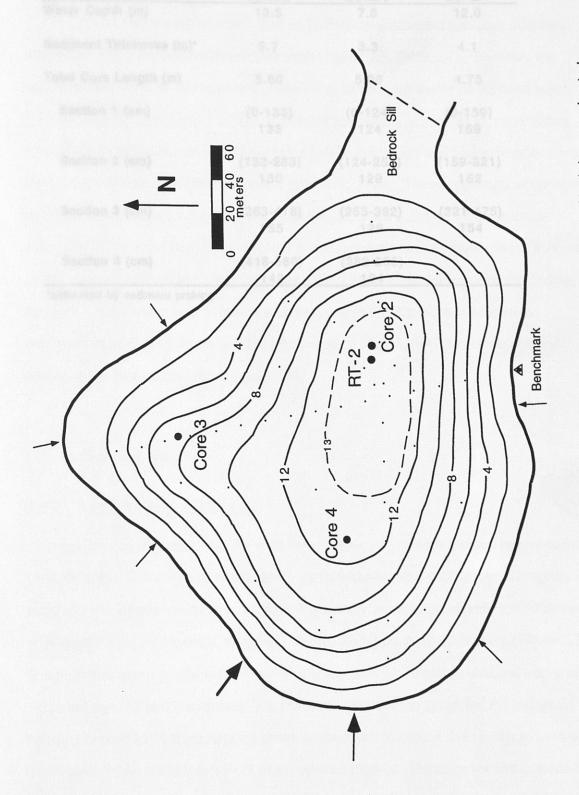
This chapter presents and analyzes the data collected by the methods outlined in Chapter 2. For most analyses, the complete data set is graphed and discussed; for some analyses that produced extensive data, representative data are chosen. Individual inorganic layers are identified by core and depth, and by the lettered correlation presented in section 4.2. Compete field data are given in Appendix C. All laboratory data are tabled in Appendix D.

#### 3.1 Field Data

### 3.1.1 Bathymetry and Sediment Probing

The maximum water depth for Ritterbush Pond, measured during the winters of 1997 and 1998, was 13.6 m (Figure 3.1). Bathymetry data collected in 1995, suggest a maximum depth of just over 14 m. During the spring and summer of 1998, the bedrock sill controlling outflow was at 0.5 m to 0.1 m below the water surface. This observed range suggests that the difference in the bathymetric measurements is probably due to natural water level fluctuation.

Sediment probing underestimated actual sediment thickness (Table 3.1). The length of the retrieved cores exceeded the sediment depth predicted by probing by 0.6 to 1.8 m, except in the center of the pond. The underestimate is most likely due to well-compacted, fine-grained inorganic layers that resisted the small diameter, uncased probe rod at depth. Therefore, sediment probing provides only a minimum sediment thickness estimate.



from Eden USGS 7.5" topographic quadrangle. Broad arrows represent perennial stream inflow; smaller arrows denote Figure 3.1 Ritterbush Pond bathymetry and core location. Contour interval 2 meters. North is approximated intermittent streams.

Table 3.1 Water Depth, Estimated Sediment Thickness, and Core Section Length

	CORE 2	CORE 3	CORE 4
Water Depth (m)	13.5	7.8	12.0
Sediment Thickness (m)*	5.7	3.3	4.1
Total Core Length (m)	5.60	5.06	4.75
Section 1 (cm)	(0-133) 133	(0-124) 124	(0-159) 159
Section 2 (cm)	(133-263) 130	(124-253) 129	(159-321) 162
Section 3 (cm)	(263-418) 155	(253-382) 129	(321-475) 154
Section 4 (cm)	(418-560) 142	(382-506) 124	

<sup>\*</sup>estimated by sediment probing

#### 3.1.2 Core Location

Core locations were selected based on bathymetry, estimated sediment thickness, and likely sources for terrestrial sediment input (Figure 3.1, Table 3.1). To obtain the longest, undisturbed, sediment record, Core 2 was taken in the center of the pond at a water depth of 13.5 m. Core 2 is located within a few meters of core RT-2, maximizing the probability of correlation with the existing pollen chronology and fourteen radiocarbon dates for Ritterbush Pond (Bierman et al., 1997; Lin, 1996). The entire length of the core barrel (5.8 m) was driven, but it did not reach the glacial till underlying the lacustrine sediments. Core 3 and Core 4 were located to determine the lateral distribution of inorganic layers. Core 4 (12.0 m) was placed between Core 2 and the two largest streams feeding the lake. Core 4 was driven to refusal and bottomed in till. Core 3 was located in shallower water (7.8 m) on the gentlest lake marginal slope, below the steepest hills bounding the lake. Core 3 did not reach till.

#### 3.2 Laboratory Data

## 3.2.1 Litho-Stratigraphic Logs

Generalized graphic logs for each core (Figure 3.2) provide a visual reference of core lithology. Black, fine-grained organic gyttja is the dominant lithology. The gyttja is relatively homogenous within each core, and generally increases in coherency and firmness with depth. Fine sand and silt are present as discrete layers in all three cores (Figure 3.3). The inorganic layers can be divided into two types: thick (1-10 cm) graded and non-graded beds, and thin (<1 cm) laminations. The boundary between the gyttja and the inorganic material is generally a sharp contact; however, the lower transition from gyttja to sand or silt in some of the thickest inorganic layers appears gradual. Evidence for bioturbation is present in the upper centimeter of only one inorganic layer. Macrofossils (seeds, leaves,

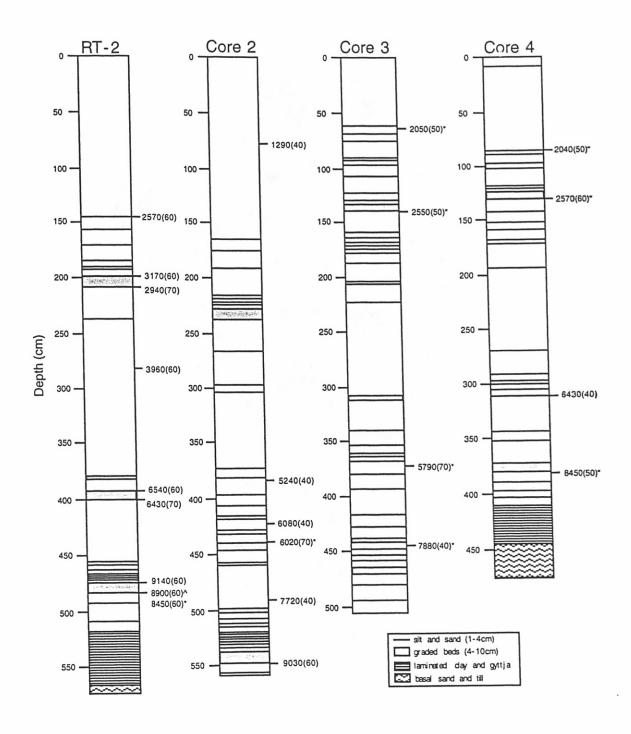


Figure 3.2 Generalized litho-stratigraphic logs for Ritterbush Pond cores. Log for RT-2 is adapted from Lin (1996). Location of inorganic layers within gyttja is shown. All radiocarbon dates are in <sup>14</sup>C yr BP (1 standard deviation). Asterisk (\*) denotes macrofossil ages; carrot (^) is an average of three replicates on one gyttja sample.

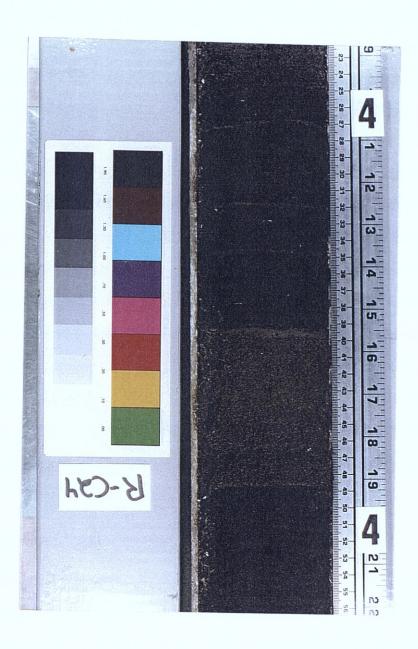


Figure 3.3 Photograph of Core 2, Section 3 showing a thick inorganic layer. The 10-cm thick brown layer has sharp upper and lower contacts with the surrounding black gyttja. Millimeter-scale gray/brown laminations are also visible (depth = 427, 432 and 434.5 cm).

and woody particles) are found above, below, and within the inorganic layers, as well as in the gyttja where visible inorganic layers are absent. The inorganic layers are less frequent in the upper and middle portions of the cores, and appear to cluster within the core. Three clusters of inorganic layers can be identified in each of the cores, and although the number and distribution of the layers varies within each cluster, it is possible to trace visually the thickest graded beds between cores.

The three cores, while sharing general characteristics, exhibit distinct differences in lithology and grain size (Table 3.2) that are a function of water depth and sediment source. Core 3, deposited in the shallowest water and closest to shore, has the coarsest gyttja and inorganic grain size, as well as the highest percentage of macrofossils (wood and leaves) and inorganic material. Core 2, at the center of the pond in the deepest water, shows the finest grain size and the lowest occurrence of inorganic layers and macrofossils. These data suggest that the deposition of gyttja is controlled primarily by the settling of organic and fine, inorganic particles. The coarser grains of the inorganic layers, the visible grading of the thick beds, and the sharp contacts with the gyttja, imply a change in depositional energy and sediment source from the quiet-water settling conditions of the gyttja.

## 3.2.2 Magnetic Susceptibility

The three cores have background magnetic susceptibility levels (<5 SI) that increase slightly with depth, suggesting a general down-core increase in magnetic mineral content (Figure 3.4). Apparent background levels may be elevated by the close spacing of magnetic peaks and the presence of the aluminum core catcher at the base of the core. This increase could also be due to compaction of the cores and indicate an increasing density with depth, or indicate a dilution of the magnetic signal due to increased gyttja sedimentation rates toward the top of the core. Superimposed on this general trend are

Table 3.2 Characteristic Litho-Stratigraphy of Cores 2, 3, and 4

	9	GYTTJA			INORGANIC MATERIAL	: MATERI	AL		INORG/	INORGANIC LAYERS	ERS
	color	arain size		laminations	SL		layers		Number >3 cm >6 cm	>3 cm	>6 cm
			color	thickness	grain size	color	thickness	grain size			
CORE 2	black	clayey silt	gray	< 5 mm	silt	brown/ gray	2 to10 cm	silt/fine sand	23	2	က
CORE 3 brown	brown	fine silt	gray	< 1 cm	coarse silt	brown	2 to 7 cm	silt/sand	45	10	ဗ
CORE 4	black/ brown	clayey silt	gray	v 1 cm	silt	brown/ gray	2 to 7 cm	silt/fine sand	21	2	ო

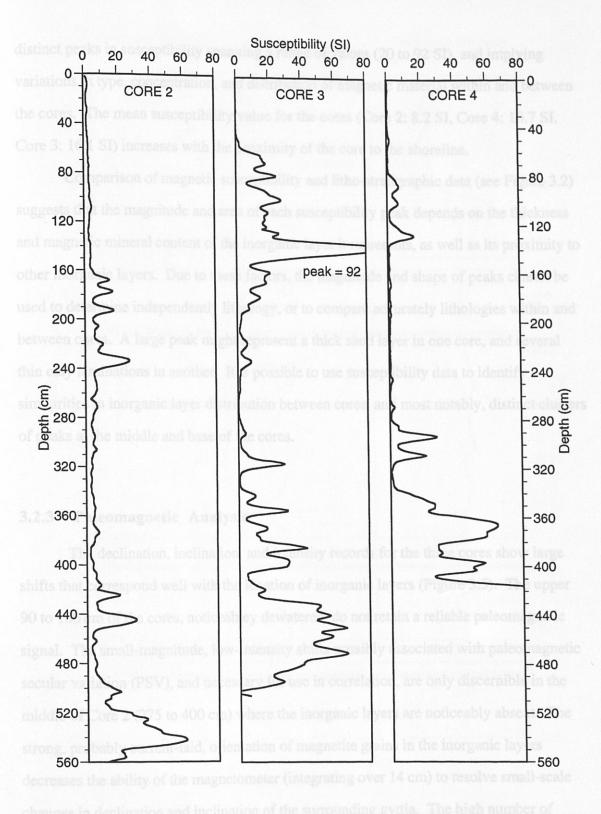


Figure 3.4 Magnetic susceptibility for cores 2, 3, and 4. Gaps in the record indicate section breaks. Peaks of increased susceptibility correspond to inorganic layers. Intervals of low susceptibility are clearly visible in the upper-middle part of each record.

distinct peaks in susceptibility spanning a range of values (20 to 92 SI), and implying variations in type, concentration, and distribution of magnetic material within and between the cores. The mean susceptibility value for the cores (Core 2: 8.2 SI, Core 4: 10.7 SI, Core 3: 16.1 SI) increases with the proximity of the core to the shoreline.

Comparison of magnetic susceptibility and litho-stratigraphic data (see Figure 3.2) suggests that the magnitude and area of each susceptibility peak depends on the thickness and magnetic mineral content of the inorganic layer it represents, as well as its proximity to other inorganic layers. Due to these factors, the magnitude and shape of peaks cannot be used to determine independently lithology, or to compare accurately lithologies within and between cores. A large peak might represent a thick sand layer in one core, and several thin clay laminations in another. It is possible to use susceptibility data to identify similarities in inorganic layer distribution between cores, and most notably, distinct clusters of peaks at the middle and base of the cores.

## 3.2.3 Paleomagnetic Analysis

The declination, inclination, and intensity records for the three cores show large shifts that correspond well with the location of inorganic layers (Figure 3.5). The upper 90 to 100 cm of the cores, noticeabley dewatered, do not retain a reliable paleomagnetic signal. The small-magnitude, low-intensity shifts possibly associated with paleomagnetic secular variation (PSV), and necessary for use in correlation, are only discernible in the middle of Core 2 (275 to 400 cm) where the inorganic layers are noticeably absent. The strong, probably current-laid, orientation of magnetite grains in the inorganic layers decreases the ability of the magnetometer (integrating over 14 cm) to resolve small-scale changes in declination and inclination of the surrounding gyttja. The high number of inorganic layers in Cores 3 and 4 precludes detection of PSV in the records at the

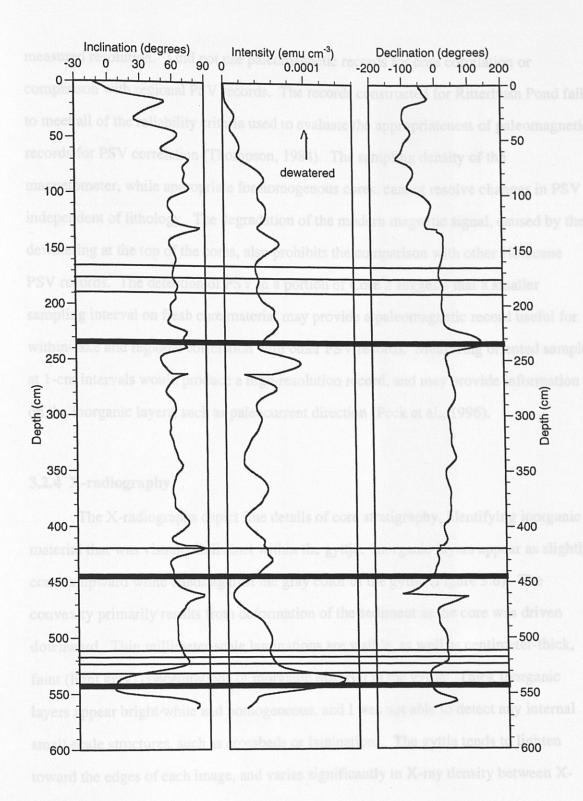


Figure 3.5 Paleomagnetic declination, inclination and intensity for Core 2. Horizontal lines indicate the location of the thickest inorganic layers.

measured resolution. I did not use paleomagnetic records for core correlation or comparison with regional PSV records. The records constructed for Ritterbush Pond fail to meet all of the reliability criteria used to evaluate the appropriateness of paleomagnetic records for PSV correlation (Thompson, 1984). The sampling density of the magnetometer, while appropriate for homogenous cores, cannot resolve changes in PSV independent of lithology. The degradation of the modern magnetic signal, caused by the dewatering at the top of the cores, also prohibits the comparison with other Holocene PSV records. The detection of PSV in a portion of Core 2 suggests that a smaller sampling interval on fresh core material may provide a paleomagnetic record useful for within-lake and regional correlation with other PSV records. Measuring oriented samples at 1-cm intervals would produce a high-resolution record, and may provide information on the inorganic layers, such as paleocurrent direction (Peck et al., 1996).

#### 3.2.4 X-radiography

The X-radiographs depict fine details of core stratigraphy, identifying inorganic material that was visually indistinct within the gyttja. Inorganic layers appear as slightly convex upward white bands against the gray color of the gyttja (Figure 3.6). The convexity primarily results from deformation of the sediment as the core was driven downward. Thin millimeter-scale laminations are visible, as well as centimeter-thick, faint (light gray) concentrations of inorganic material in the gyttja. Thick inorganic layers appear bright white and homogeneous, and I was not able to detect any internal small-scale structures, such as crossbeds or laminations. The gyttja tends to lighten toward the edges of each image, and varies significantly in X-ray density between X-radiographs.

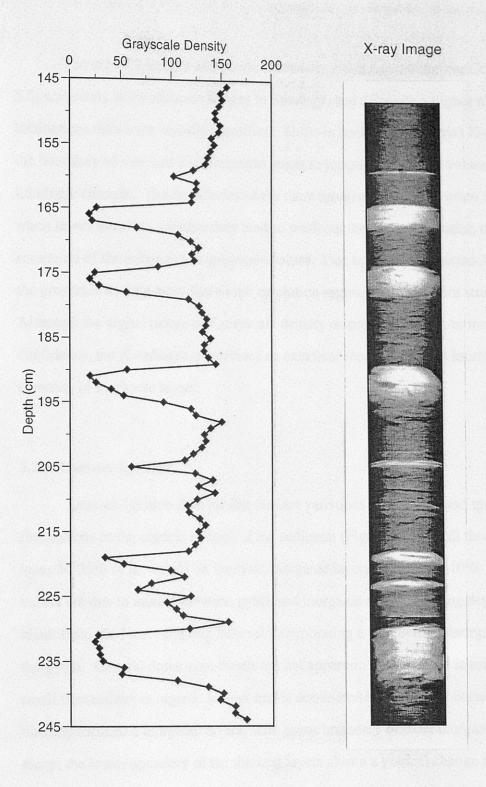


Figure 3.6 X-radiograph and grayscale density for a 1 meter section (145 cm to 245 cm) of Core 2.

The scanned images and grayscale density graph constructed for Core 2 (Figure 3.6) accurately show relative changes in lithology, and delineate a higher number of fine laminations than were visually identified. Shifts in background (gyttja) X-ray density at the boundary of matched X-radiographs result in jumps in grayscale values that mimic lithologic changes. The boundaries of the thick inorganic layers are often indistinct, and when layers are close together they tend to wash out the gyttja separating them, due to the saturation of the image at low grayscale values. Due to these inconsistencies, I do not use the grayscale density record as a high resolution representation of core stratigraphy. Although the digital image and grayscale density record are difficult to manipulate with confidence, the X-radiograph provides an excellent record for visual location and counting of inorganic layers.

#### 3.2.5 Loss-on-Ignition

Loss-on-ignition data exhibit distinct variations with depth, and quantify fluctuations in the organic content of the sediment (Figure 3.7). In all three cores, gyttja loses 30-35% of its weight on ignition; inorganic layers lose only 5-10%. Intermediate values are due to mixing between gyttja and inorganic material during deposition, or result from the 1-cm sampling interval incorporating a <1-cm thick inorganic layer into the gyttja. General down-core trends are not apparent, as the record is sensitive to even small fluctuations in organic matter, and is dominated by peaks that correlate well with visually identified inorganic layers. The upper boundary of most inorganic layers is sharp; the lower boundary of the thickest layers shows a gradual change from gyttja to inorganic values over 1 to 4 cm. The close correlation of peak magnitude and lithology makes LOI records ideal for detecting the location and thickness of inorganic layers.

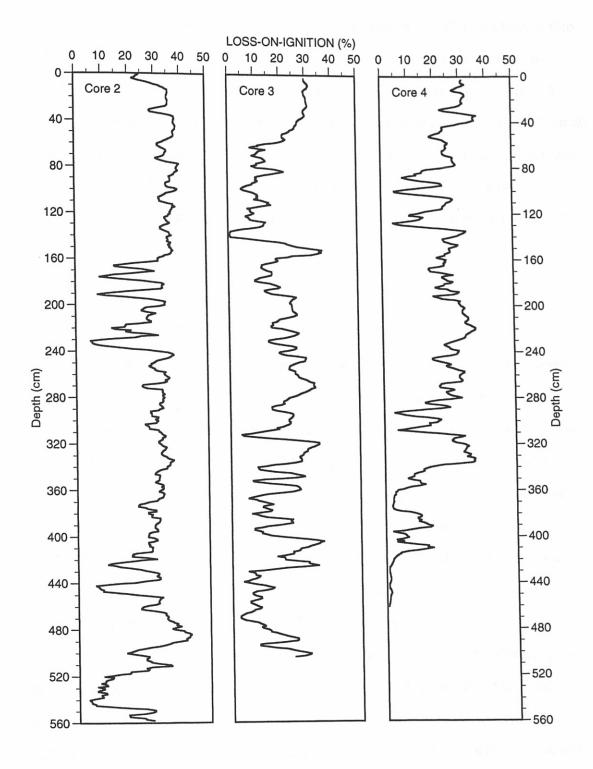


Figure 3.7 Loss-on-ignition for cores 2, 3, and 4. Values <15% indicate significant inorganic layers. Data have been smoothed with a 5-point running average.

Core 2 is characterized by clusters of low LOI values from 160 to 240 cm, 400 to 450 cm, and at the base of the core. Outside of these clusters, LOI values do not drop below 20%, although smaller shifts to low values (25 to 30%) are easily identified. A similar clustering of low values also occurs in Core 4. LOI values of <15% occur from 80 to 140 cm, 280 to 310 cm, and the base of the Core 4. Smaller shifts range in magnitude from 15% to 30%. Core 3 exhibits the most frequent fluctuations in LOI, with values <20% occurring over the entire core length. Shifts of <10% cluster at 60 to 140 cm, and below 320 cm.

#### 3.2.6 Elemental Analysis

Total organic carbon (TOC) values for Core 2 range from 15% to 20% for gyttja and average 5% for inorganic layers (Figure 3.8). The patterns, trends, and relative changes in peak magnitude are nearly identical to LOI records (see above, and section 4.1). To avoid redundancy, I did not measure TOC for Cores 3 and 4, as LOI analysis had already been completed. The LOI values (approximate % organic matter) could be used to estimate percent organic carbon by using a conversion factor obtained from measured values. The conversion calculation for Core 2 (%TOC = 0.53\*%LOI) would provide approximate TOC values, but should be checked with measured values as the carbon content of the organic material will vary slightly between cores.

The highest carbon / nitrogen ratios (16 to 21) generally occur at major inorganic layers in Core 2, while the background ranges widely (9 to 15) (Figure 3.8). If the inorganic layers contained only terrestrial woody plant debris, the C/N values should be >20; if the gyttja was entirely aquatic material, the C/N ratio should be <10 (Meyers and Ishiwatari, 1995). The measured C/N values suggest that mixing between terrestrial and

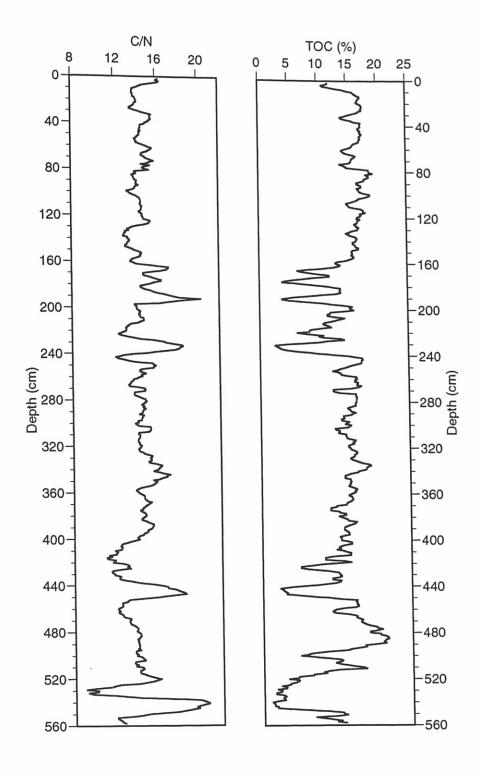


Figure 3.8 Total organic carbon (TOC) and carbon / nitrogen ratio (C/N) for Core 2. Five-point running averages of data show decreases in TOC generally correspond to increases in C/N.

aquatic material occurs in both the inorganic layers and the gyttja. The average C/N ratio of the gyttja still remains lower than the average C/N ratio of the inorganic layers, implying a predominant source for each; the gyttja is dominantly aquatic and the inorganic layers are dominantly terrestrial. One notable exception is at depth 530 cm in Core 2. C/N values drop to 9, the lowest value for the core and typical of nearly pure aquatic material; however, TOC values (5%) suggest an inorganic source. This discrepancy may indicate reworked organic lake sediments within a matrix of terrestrial inorganic material.

### 3.2.7 Charcoal Analysis (Nitric Acid Digestion)

Charcoal values for samples from the five inorganic layers exhibit little deviation and are lower (<0.5%) than values for the sampled gyttja (Figure 3.9). The three sections of gyttja average 2±0.8% (1 sigma) charcoal carbon. Values for the samples collected immediately above and below the inorganic layers fall within the range of values observed for the gyttja. Charcoal values appear to depend on the original carbon content of the gyttja. This may be due to incomplete digestion of the organic material by the nitric acid, or to a background abundance of charcoal in the gyttja.

## 3.2.8 Stable Carbon Isotopes

Two inorganic layers from Core 2, having sharp contacts with gyttja and exhibiting internal grading, show systematic variation in  $\delta^{13}$ C with depth (Figure 3.10). Average gyttja values (-31‰) and inorganic values (-27‰) agree with aquatic and terrestrial values (respectively) previously measured for Ritterbush Pond (Lini et al., 1995). In both layers, down-core changes from gyttja to silt are marked by a jump to less negative (terrestrial) values. The  $\delta^{13}$ C values peak in the upper centimeters of the layers,

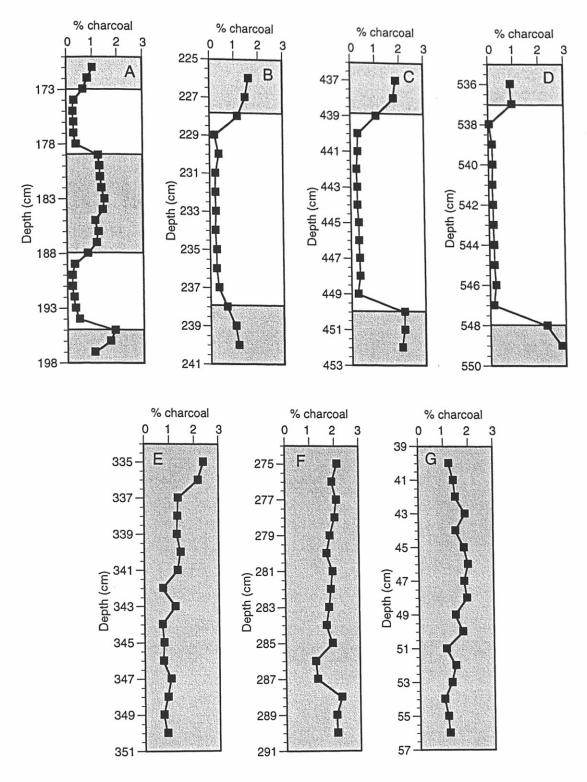


Figure 3.9 Percent charcoal from nitric acid digestion. A-D contain inorganic layers and the surrounding gyttja (shaded). E-G are gyttja only.

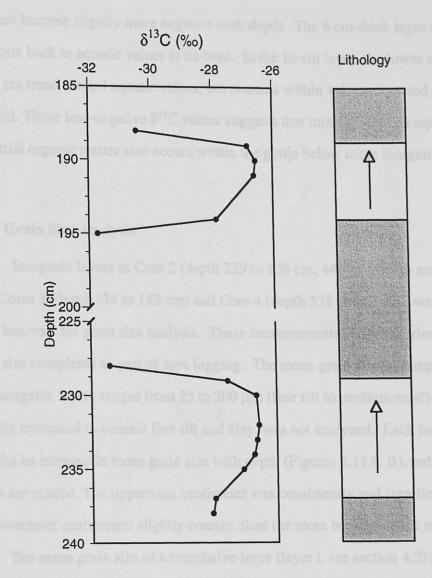


Figure 3.10 Stable carbon isotope data for two inorganic layers in Core 2. Shifts from aquatic ( $\delta^{13}C = -31\%$ ) to terrestrial ( $\delta^{13}C = -27\%$ ) isotopic values occur at the inorganic layers. Arrows indicate grading of inorganic layers.

and then become slightly more negative with depth. The 6 cm-thick layer shows a sharp transition back to aquatic values at its base. In the 10 cm layer, the lower contact shows a 2 to 3 cm trend toward aquatic values, but remains within values expected for terrestrial material. These less-negative  $\delta^{13}$ C values suggests that mixing between aquatic and terrestrial organic matter also occurs within the gyttja below some inorganic layers.

### 3.2.9 Grain Size Analysis

Inorganic layers in Core 2 (depth 229 to 238 cm, 440 to 449 cm and 538 to 547 cm), Cores 3 (depth 134 to 142 cm) and Core 4 (depth 538 to 547 cm), were sampled at 1-cm intervals for grain size analysis. These measurements verify the visual estimates of grain size completed as part of core logging. The mean grain size of samples from the five inorganic layers ranges from 25 to 200 µm (fine silt to medium sand). The gyttja, visually estimated to contain fine silt and clay, was not analyzed. Each inorganic layer exhibits an increase in mean grain size with depth (Figures 3.11A, B), indicating that the layers are graded. The uppermost centimeter was consistently and significantly finer, and the lowermost centimeters slightly coarser, than the more homogeneous middle of the layer. The mean grain size of a correlative layer (layer i, see section 4.2) sampled in each of three cores, decreases with distance away from the lake margin (Figure 3.11B). As grain size corresponds to the velocity of transport, this trend suggests deposition by a decelerating current.

## 3.2.10 Bulk Density

Bulk density of gyttja increases with depth (Figure 3.12). The uppermost sample (depth = 71 cm) had significantly dewatered since the core was logged; there is no evidence for dewatering in other samples. The data generally conform to the expected

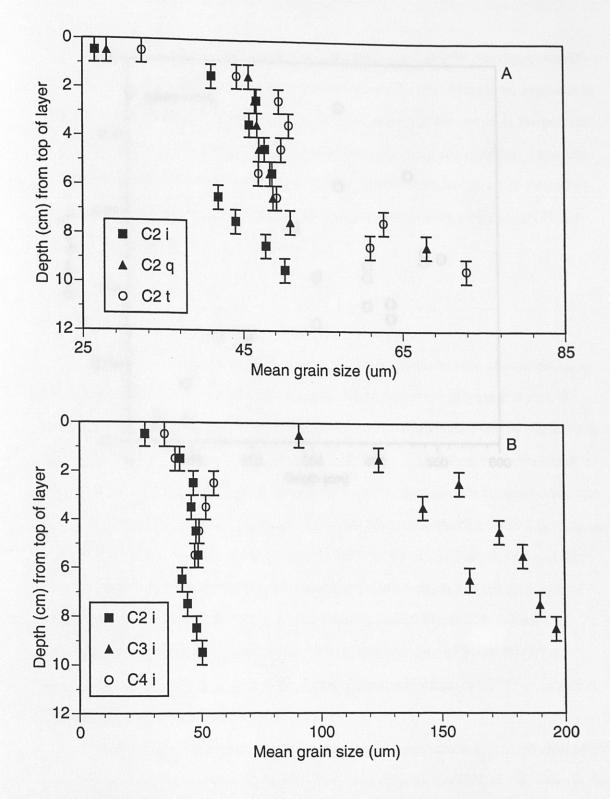


Figure 3.11 Mean grain size data for each cm of the five thickest inorganic layers (6 to 10 cm). A) Three layers (i, q and t) from Core 2 are normally graded, with grain size decreasing toward the top of the layer. B) A single layer (i), correlated between the cores, shows the coarsest grain size in Core 3.

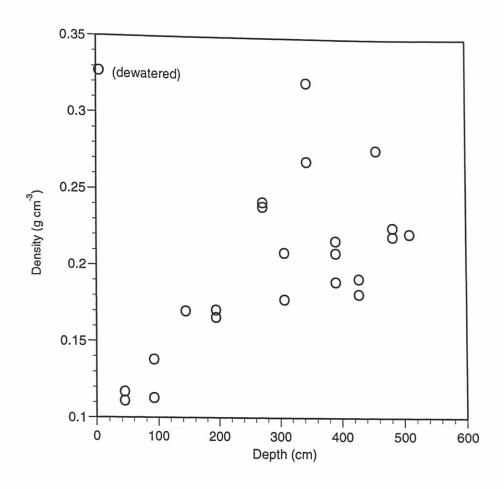


Figure 3.12 Gyttja bulk density for Core 2. Density generally increases with depth.

increase with depth due to autocompaction. The maximum value for density, however, does not occur at the base of the core, but at a depth of 350 cm. There is no evidence to suggest that this high density represents a lithologic change in the gyttja, as the percent organic matter for the measured sample does not suggest inorganic material. I propose that variations in bulk density, in addition to being depth dependent, are also related to the proximity and thickness of inorganic layers that undergo little compaction (Pizzuto and Schwendt, 1997).

#### 3.2.11 Radiocarbon Analysis

Two types of material from the cores, gyttja and macrofossils, were dated using radiocarbon analysis to constrain the timing of deposition of the inorganic layers. I accounted for the gyttja / macrofossil offset measured at Ritterbush Pond by subtracting 450 <sup>14</sup>C yr from all gyttja ages (see section 2.2.11, Table 3.3). When this adjustment is applied to other macrofossil / gyttja dates correlated stratigraphically between cores, the offset is systematic within and between cores. Samples correlated from RT-2 (gyttja) and Core 4 (macrofossil) both result in ages of 5980 <sup>14</sup>C yr BP (Core 2 depth 448 cm) and 8450 <sup>14</sup>C yr BP (Core 2 depth 547 cm). Samples at Core 2 depth 164 cm give ages of 2120±60 (RT-2, gyttja), 2050±50 (C3, macrofossil), and 2040±50 (C4, macrofossil), while samples correlated to Core 2 depth 238 cm result in ages of 2490±70 (RT-2, gyttja), and 2550±50 (C3, macrofossil), giving a maximum offset of 80 <sup>14</sup>C yr, which is within the analytic uncertainty of the dates.

Calibration of the radiocarbon ages to calendar years results in a small shift of 30 years at the youngest date (Core 2 depth = 164), and a maximum shift of 990 years at the oldest date (Core 2 depth 548) (Figure 3.13). The age-depth model compiled for Core 2, from all samples dated from all four cores, is a decreasing exponential. This exponential

CAMS#	Core	Depth (cm)	Core 2	material	²delta 13C	¹⁴C age	adjusted	<sup>4</sup> Calibrated Age (calendar yr B.P.)	best age estimate
33132	RT-2	96	164	gyttja	-31.7	2570 ± 60	2120	2146 (2093) 1993	2090
33135	RT-2	142	228	gyttja	-31.5	3170 ± 60	2720	2855 (2787) 2767	2790
33352	RT-2	154	238	gyttja	-29.5	2940 ± 70	2490	2717 (2707, 2629, 2499) 2475	2610
22993	RT-2	220	300	gyttja	-30.6	3960 ± 60	3510	3843 (3817, 3782, 3732) 3700	3780
33351	RT-2	339	439	gyttja	-32.0	$6540 \pm 60$	0609	7014 (6915) 6871	6920
20195	RT-2	348	448	gyttja	-32.4	6430 ± 70	5980	6884 (6833, 6826, 6799) 6742	6820
32856	RT-2	416	537	gyttja	-32.7	9140 ± 60	8690	9666 (9638) 9533	9640
32854	RT-2	426	547	gyttja	-31.8	8870 ± 60	8420	9469 (9434) 9374	9430
33134	RT-2	426	547	gyttja	-31.8	8950 ± 50	8500	9469 (9467) 9444	9470
33350	RT-2	426	547	gyttja	-31.8	8890 ± 60	8440	9471 (9440) 9385	9440
32855	RT-2	426	547	seed	-28	8450 ± 60	8450	9475 (9442) 9389	9440
46942	8	77	77	gyttja	-31	1290 ± 40	840	771 (733) 699	730
46943	8	383	383	gyttja	-31	5240 ± 40	4790	5587 (5578) 5566 5540 (5510, 5505) 5473	5520
46944	8	424	424	avttia	-31	6080 ± 40	5630	6456 (6412) 6394	6410
40775	8	439.7	439.7	twig	-28	+	6020	6932 (6866) 6767	6870
46945	8	489	489	gyttja	-31	7720 ± 40	7270	8081 (8060, 8039) 8021 8017 (8001) 7981	8030
40776	3	548	548	avttia	-31	9030 ± 60	8580	9571 (9505) 9459	9510
44693	8	63.5	164	poom	-26.5	2050 ± 50	2050	2060 (1990) 1931	1990
44695	ខ	144	238	poom	-27.6	2550 ± 50	2550	2751 (2726) 2709 2622 () 2502	2610
44697	8	375	432	poom	-28	5790 ± 70	5790	6677 (6626) 6504	6630
44600	3 8	444	510	hark	-32.0	7880 ± 50	7880	8718 (8582) 8540	8580
44694	3 2	81	164	leaves	-28.0	+1	2040	2042 (1980) 1916	1980
44696	2	132	238	gyttja / leaves	-29.5	2570 ± 60	2570 <sup>6</sup>	2761 (2734) 2709 2623 () 2502	2630
44698	3	311	448	gyttja / leaves	-23.3	6430 ± 40	5980	6860 (6833, 6826, 6799) 6774	6820
44700	25	380	547	poom	-30.6	8450 ± 50	8450	9473 (9442) 9399	9440

3 1/C ages were adjusted for measured gyttja / macrofossil offset by subtracting 450 14C years from each gyttja age.

<sup>4</sup>all adjusted <sup>14</sup>C ages calibrated using CALIB rev3.0.3A (Stuiver and Reimer, 1993). A 1 sigma range encloses reported intercepts in ().

<sup>5</sup> intercept or average of intercepts where 1 range is reported, weighted average of intercepts (or midpoint of range where

<sup>6</sup> sample not adjusted for gyttja / macrofossil offset due to ambiguity of material dated and agreement with expected age. no intercept is reported) where 2 ranges are reported. Ages rounded to nearest decade

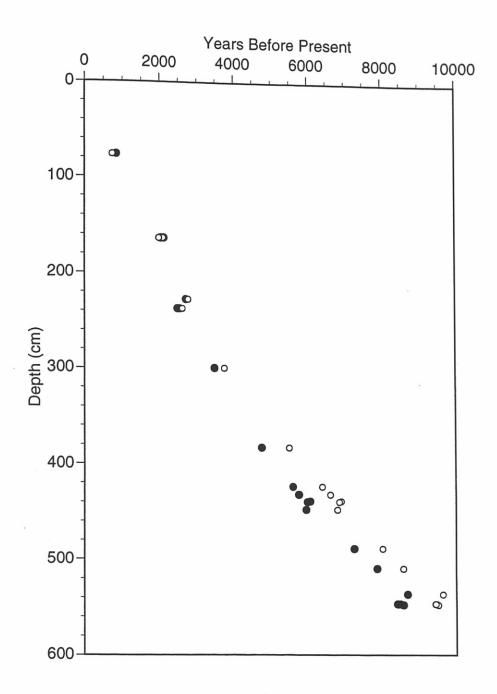


Figure 3.13 Radiocarbon and calibrated ages for Ritterbush Pond cores, correlated to depth in Core 2. Closed circles are uncalibrated radiocarbon ages; open circles are ages converted to calendar years using CALIB rev3.0.3A (Stuiver and Reimer, 1993).

relationship can be used to estimate that the age of sediment at the base of Core 2 (560 cm) is about 10,000 cal yr BP.

I use selected data sets (presented in Chapter 3) to investigate several aspects of inorganic layer deposition in Ritterbush Pond. In the following subsections I: 1) companies the different analytical methods used to determine the best tools for characterization of the inorganic layers, 2) correlate the cores to determine the spatial and temporal variability of the layers, 3) suggest emplacement mechanisms for the inorganic layers, and 4) estimate the age and frequency of inorganic layer deposition.

Comparison of Data Sets and Methods

visites strangraphy, loss-on-ignition, total organic carbon, magnetic susceptibility, x-radiography, and grayscale density were used to identify the location and type of material within the cores. Although the data sets are similar, each method measures a different physical or biochemical property of the sediment at varying resolutions and sensitivities, resulting in slightly different records of inorganic layer location and thickness within the gyttia (Figure 4.1). Visual methods (logs and pictures) rely on distinct color and textural changes for identification of varying lithology. Organic carbon content analysis (LOI and TOC) is a proxy for lithologic variation but detection of small-scale fluctuations is restricted by the sampling interval (1 cm). Magnetic susceptibility analysis is also limited by the resolution of the measurement (4 cm), decreasing the ability of the record to detect small changes in magnetic mineral content. X-radiographs, which depict variations in composition and density, have the highest resolution. The grayscale density data, based on gradation in the X-radiograph density, is also at measured high resolution (72 pixels per insh), and smoothed to 1 value per centimeter for comparison with other data sets.

# CHAPTER 4 - Interpretation of Results

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## 4.1 Comparison of Data Sets and Methods

Visual stratigraphy, loss-on-ignition, total organic carbon, magnetic susceptibility, x-radiography, and grayscale density were used to identify the location and type of material within the cores. Although the data sets are similar, each method measures a different physical or biochemical property of the sediment at varying resolutions and sensitivities, resulting in slightly different records of inorganic layer location and thickness within the gyttja (Figure 4.1). Visual methods (logs and pictures) rely on distinct color and textural changes for identification of varying lithology. Organic carbon content analysis (LOI and TOC) is a proxy for lithologic variation but detection of small-scale fluctuations is restricted by the sampling interval (1 cm). Magnetic susceptibility analysis is also limited by the resolution of the measurement (4 cm), decreasing the ability of the record to detect small changes in magnetic mineral content. X-radiographs, which depict variations in composition and density, have the highest resolution. The grayscale density data, based on gradation in the X-radiograph density, is also at measured high resolution (72 pixels per inch), and smoothed to 1 value per centimeter for comparison with other data sets.

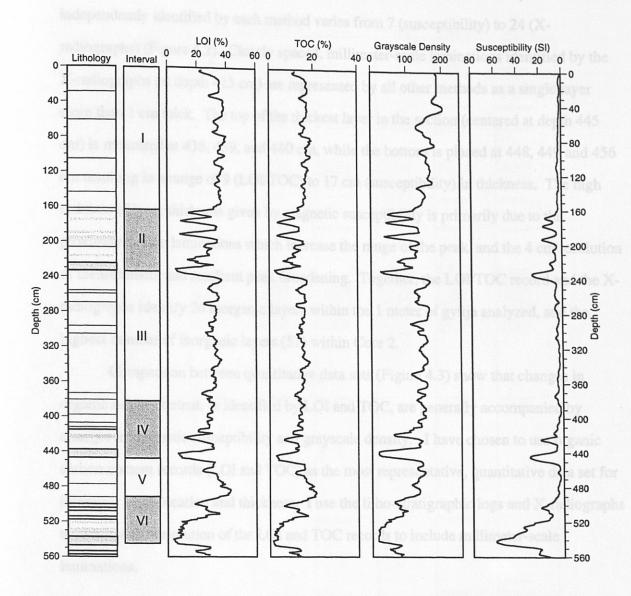


Figure 4.1 Comparison of high-resolution, whole-core data sets for Core 2. Shifts to the left indicate the location of inorganic layers.

Over a representative one meter section of Core 2, the number of layers independently identified by each method varies from 7 (susceptibility) to 24 (X-radiographs) (Figure 4.2). Closely spaced, millimeter-scale laminations identified by the X-radiographs (at depth 415 cm) are represented by all other methods as a single layer more than 1 cm thick. The top of the thickest layer in the section (centered at depth 445 cm) is measured at 438, 439, and 440 cm, while the bottom is placed at 448, 449 and 456 cm resulting in a range of 9 (LOI/TOC) to 17 cm (susceptibility) in thickness. The high estimate of layer thickness given by magnetic susceptibility is primarily due to the proximity of fine laminations which increase the range of the peak, and the 4 cm resolution of measurement and resultant peak broadening. Together, the LOI/TOC record and the X-radiographs identify 24 inorganic layers within the 1 meter of gyttja analyzed, and the highest number of inorganic layers (57) within Core 2.

Comparison between quantitative data sets (Figure 4.3) show that changes in organic matter content, as identified by LOI and TOC, are generally accompanied by changes in magnetic susceptibility and grayscale density. I have chosen to use organic carbon content records (LOI and TOC) as the most representative, quantitative data set for inorganic layer location and thickness. I use the litho-stratigraphic logs and X-radiographs to increase the resolution of the LOI and TOC records to include millimeter-scale laminations.

#### 4.2 Core Correlation

Correlation of the four cores for Ritterbush Pond permits the determination of the lateral extent and lithologic variability of the inorganic deposits. Correlating Cores 2, 3, and 4 with Core RT-2, augments my data set with the existing pollen chronology and 14 radiocarbon dates (Lin, 1996). Together, the core correlation and radiocarbon dates

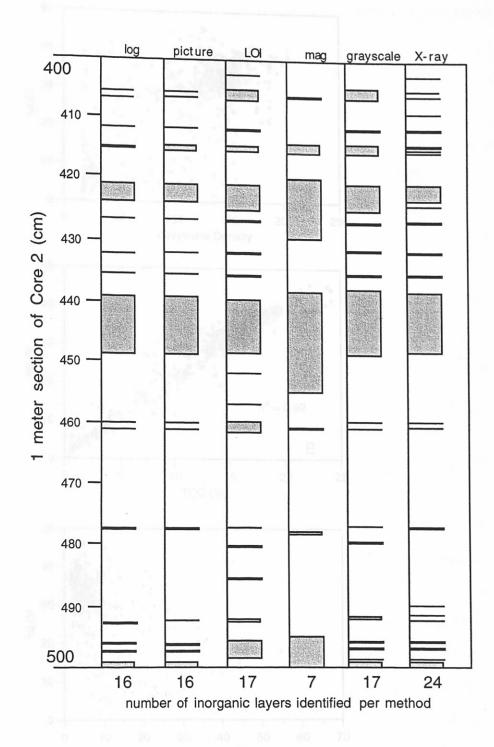


Figure 4.2 Identification of inorganic layer location and thickness by different analytical techniques.

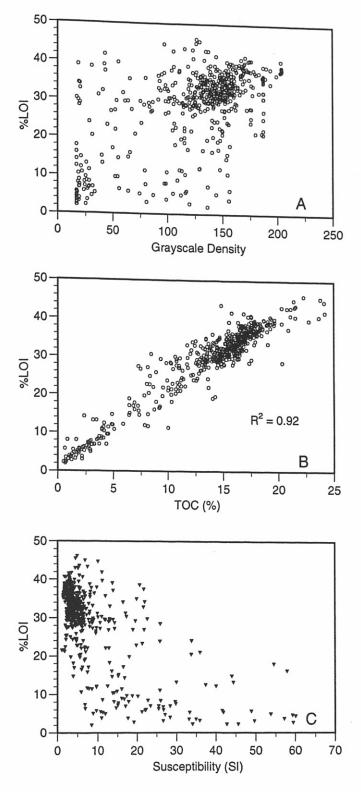


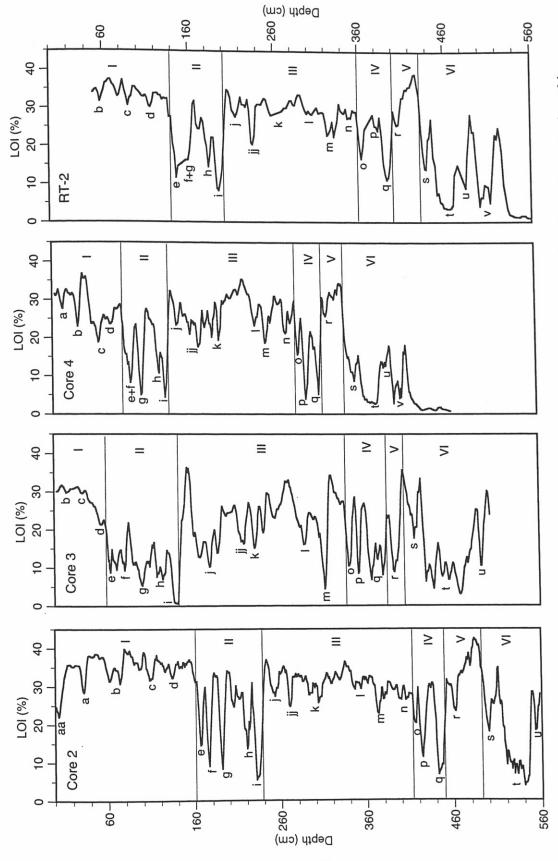
Figure 4.3 Comparison of LOI to A) grayscale density (low and high values appear linear), B) TOC (linear) and C) magnetic susceptibility (exponential).

allow me to investigate the spatial and temporal distribution of the inorganic layers throughout the lake.

# 4.2.1 Litho-Stratigraphic Correlation

The sensitivity of the LOI data to varying amounts of inorganic material make it an ideal record for correlating inorganic layers between cores. Using the 5-point running average record for Core 2, I assigned a lowercase letter to each significant low LOI value, or negative peak, or in some cases, a single letter to pairs of small peaks (Figure 4.4). The peaks (aa to u) vary in magnitude according to the thickness and number of inorganic layers they represent. I then made a peak-by-peak correlation of Cores 3, 4, and RT-2 using LOI records and litho-stratigraphic logs. The peaks identified in Core 2 account for all significant peaks in the other cores, although one large peak in Core 2, may be represented as two closely spaced, smaller peaks in another core. The best agreement in number, magnitude, and shape of peaks is between Cores 2 and RT-2, due to the proximity of the coring locations in the center of the lake. Cores 4 and RT-2, the only cores to bottom in till, contain an additional peak (v) at their base.

The number, thickness, and grain size of the layers comprising each peak (aa to v) for all four cores were tabulated to assess the lateral variability in layer frequency, size, and lithology (Table 4.1). Peaks I through o in the LOI record for Core RT-2 were not visually represented in the stratigraphic log. In all cores, layers in peaks as through d were visibly indistinct and contained brown (organic-rich) sand and silt, in contrast to the gray silt and gray/brown sand observed in the rest of the core. Thick graded beds (peaks f, g, i, p, and t) are present in all four cores and show thickness variations of up to 4 cm. The greatest variation of numbers of layers occurs in peak q, where four 1-cm sand layers are identified in Core 3. In Cores 2 and 4 and RT-2, all collected in deeper water, layer q is a single 8 to 9 cm layer.



correlation between cores. Roman numerals indicate the division of each core into six intervals. RT-2 LOI data from Lin Figure 4.4 Correlation of Ritterbush Pond cores using smoothed (5 pt) LOI data. Lettered peaks indicate stratigraphic

Table 4.1 Lateral Variation in Correlated Inorganic Lavers

Peak (layer)	RT-2	C2	C3	C4
aa	4 cm br silt	2 cm br sand		
a	2 mm br silt	2 mm br silt		Or comment of the A
b	2 mm br silt	2 mm br silt	man A stance of the se	1 cm br sand
С	2 mm br silt	2 mm br silt		1 cm silt^
d	2 mm br silt	1 cm br silt	shrupon for Anti-	: Name and the original of the
e n of a thick	5 mm silt 3 cm sand *	2 cm sand *	2 cm br sand 1 cm sand 2 cm sand *	1 cm sand ^
f s	5 cm sand *	3.5 cm sand*	7 cm sand * 2, 1 cm sand	4 cm sand *
g	4.5 cm sand	5 cm sand *	6 cm sand * 1 cm sand	6 cm sand *
h	couplet 4, <1cm silt 2, 1 cm sand *	couplet 4, <1cm silt	3, 1cm sand	8 mm silt 2 cm silt
i de	10 cm sand *	10 cm sand *	5 mm silt 9 cm sand *	6 cm sand *
i ma	5, <1 cm silt	2, 2mm silt	8, 1-2 cm sand^	
**	1 cm sand	5 mm silt	2, 1 cm sand	2, 1 cm sand^ 4 mm silt
k	5, <1 cm silt	3 mm silt 5 mm silt	1 cm sand^ 5 mm silt	2,1 cm sand ^ 5 mm silt
		2, <1mm silt	1 cm sand^	8 mm lam
m Table see a se		2, 2 mm silt 2.5 mm silt	5 cm sand^*	3 cm sand lam 5 mm silt
n		<1mm silt couplet	Trhe insupanie is	8 mm silt 1 mm silt
0		8 mm silt		1.5 cm silt^
р	2.5 cm sand *	2 cm sand *	2, 3 cm sand	5 cm sand * 2, 5 mm silt
q	8 cm sand *	9 cm sand *	4, 1 cm sand	3 cm sand *
r	2 mm couplet	2mm couplet	<1 cm sand 5 cm sand^	1 mm couplet
S	1 cm sand	2, 3mm silt 6 cm mix 2, 2mm silt 1 cm sand *	1 cm sand^ 2 cm sand^	3, 4mm silt
t es	6, <1 cm silt 9 cm sand *	7, 1-3 cm sand 9 cm sand *	*7,1-4 cm sand* 8 cm sand^	faint lam 8 cm sand *
u	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 cm sand 2 cm sand *	2, 1 cm sand 1 cm sand	1.5 cm sand
V	i see from sed	rest source and	bathymetry. T	1 cm silt 3 cm sand *

\* graded bed

^ abundant macrofossils

4, 1 cm silt = 4 layers of silt, each 1 cm thick

lam = lamination

mix = inorganic and organic material

br = brown

## 4.2.2 Time-Stratigraphic Correlation

Fourteen radiocarbon dates from four stratigraphic horizons (peaks e, i, q and t) confirm that the litho-stratigraphic correlation proposed above is a time-stratigraphic correlation (Table 4.2). These four horizons were chosen for dating because of the presence of a thick, graded bed at the base of each peak (i, q, t), and the coincidence of the peak with an interval boundary (e, i, q, t) (Figure 4.4). Two samples from Core 3 (layers q and t) were located significantly above the base of the peak and therefore provide minimum ages for event initiation. Core 2 was sampled 1 cm below the base of the peak t, and gives a maximum age for the event. All the samples for layer e are located above the lowest layer in the peak, and give a minimum estimate of peak initiation age. The best estimates of the peak ages are averages of values from the base or within the lowest layer contained in the peak. The standard deviation of the average values does not exceed the statistical variability associated with the dates.

#### 4.2.3 Summary of Spatial and Temporal Distribution

The variation in thickness and grain size of the inorganic layers within a single core is probably due to changes in sediment source location and availability, and velocity of subaqueous transport. Laminations (<5 mm thick) tend to be finer grained than thicker layers, suggesting lower transport velocity and a smaller magnitude transport event. In Core 2, layers composed of similar grain sizes range from 1 to 10 cm thick. The thicker layers may be due to a larger amount of sediment available for transport or a greater magnitude (duration and intensity) hydrologic event. The variation in layer grain size and thickness between cores, in addition to transport velocity and sediment availability, are also due to distance from sediment source and bathymetry. The deposition of layers in lake-marginal cores but not in the center cores may represent an event that did not

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Table 4.2 Calibrated Radiocarbon Dates for Ritterbush Core Correlation	
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e         44693         C3         63.5         wood         above first of 2 layers         2090         younger         2020±60           44693         C3         63.5         wood         above the only layer         1990         younger         2020±60           44694         C4         81         leaves         above the only layer         2610         same         2620±10           44695         C3         144         wood         base (in layer)         2630         same         2620±10           20194         RT-2         348         gyttja         base (in layer)         2630         same         2620±10           44696         C4         132         leaves         base (in layer)         6820         same         2620±10           44697         C2         439.7         twig         in the only layer         6820         same         6840±30           44698         C4         311         gyttja         base         econd of 4 layers         6630         younger (minimum)         9440*           32854         RT-2         426         gyttja         1 cm below base         9510         younger (minimum)         9440*           44699         C3         444	peak	peak CAMS#	Core	Depth	sample	position in peak	calendar age (yr BP)	age in relation to base of peak	best estimate of peak age (±1σ)
44693         C3         63.5         wood         above the only layer         1990         younger           44694         C4         81         leaves         above the only layer         1980         younger           44695         C3         144         wood         base (in layer)         2610         same           44696         C4         132         leaves         base (in layer)         2630         same           20194         RT-2         348         gyttja         base (in layer)         6820         same           40775         C2         439.7         twig         in the only layer         6820         same           44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         younger (minimum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)		33132	RT-2	96	gyttja	above first of 2 layers	2090	younger	
44694         C4         81         leaves         above the only layer         1980         younger           33352         RT-2         154         gyttja         base (in layer)         2610         same           44695         C3         144         wood         base (in layer)         2630         same           20194         RT-2         348         gyttja         base (in layer)         2630         same           40775         C2         439.7         twig         in the only layer         6820         same           44698         C4         311         gyttja         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         tm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44699         C3         444         bark         top of the third of 8 layers         9440         younger (minimum)	Ф	44693	8	63.5	poom	above second of 3 layers	1990	younger	2020±60
33352         RT-2         154         gyttja         base (in layer)         2610         same           44695         C3         144         wood         base (in layer)         2610         same           20194         RT-2         348         gyttja         base         6820         same           40775         C2         439.7         twig         in the only layer         6830         younger (minimum)           44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           32854         RT-2         426         gyttja         base         9510         older (maximum)           40776         C2         548         gyttja         top of the third of 8 layers         8580         younger (minimum)           44699         C3         444         bark         top of the third of 8 layers         9440         same		44694	2	81	leaves	above the only layer	1980	younger	
44695         C3         144         wood         base (in layer)         2610         same           20194         RT-2         348         gyttja         base (in layer)         6820         same           40775         C2         439.7         twig         in the only layer         6830         younger (minimum)           44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           32854         RT-2         426         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44700         C4         380         wood         base         9440         same		33352	RT-2	154	gyttja	base	2610	same	
44696         C4         132         leaves         base (in layer)         2630         same           20194         RT-2         348         gyttja         base         6820         same           40775         C2         439.7         twig         in the only layer         6870         same           44697         C3         375         wood         base of second of 4 layers         6820         same           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44700         C4         380         wood         base         9440         same	-	44695	8	144	poom	base (in layer)	2610	same	2620±10
20194         RT-2         348         gyttja         base         6820         same           40775         C2         439.7         twig         in the only layer         6870         same           44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44700         C4         380         wood         base         9440         same		44696	2	132	leaves	base (in layer)	2630	same	
40775         C2         439.7         twig         in the only layer         6630         younger (minimum)           44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44700         C4         380         wood         base         9440         same		20194	RT-2	348	gyttja	base	6820	same	
44697         C3         375         wood         base of second of 4 layers         6630         younger (minimum)           44698         C4         311         gyttja         base         9440         same           40776         C2         548         gyttja         1 cm below base         9510         older (maximum)           44699         C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           44700         C4         380         wood         base         9440         same	0	40775	22	439.7	twig	in the only layer	6870	same	6840±30
C4         311         gyttja         base         6820         same           RT-2         426         gyttja         base         9440         same           C2         548         gyttja         1 cm below base         9510         older (maximum)           C3         444         bark         top of the third of 8 layers         8580         younger (minimum)           C4         380         wood         base         9440         same		44697	8	375	poom	base of second of 4 layers	0899	younger (minimum)	
RT-2426gyttjabase9440sameC2548gyttja1 cm below base9510older (maximum)C3444barktop of the third of 8 layers8580younger (minimum)C4380woodbase9440same		44698	2	311	gyttja	base	6820	same	
C2 548 gyttja 1 cm below base 9510 older (maximum) C3 444 bark top of the third of 8 layers 8580 younger (minimum) C4 380 wood base 9440 same		32854	RT-2	426	gyttja	base	9440	same	
C3 444 bark top of the third of 8 layers 8580 C4 380 wood base 9440	+	40776	8	548	gyttja		9510	older (maximum)	9440*
C4 380 wood base 9440		44699	8	444		top of the third of 8 layers	8580	younger (minimum)	
		44700	2	380	poom	base	9440	same	

no variance

reach the center of the lake. The sediment in layers not identified in a lake-marginal core, but present in the other cores, may have originated on the opposite lake shore. The flat bottom of the lake, where Cores 2 and 4 were collected, is likely to receive more sediment and experience less net erosion than the site of Core 3, located on a steeper slope.

I subdivide Core 2 into six intervals, each noted by a Roman numeral (Figure 4.1), based on the location and clustering of the inorganic layers. These intervals are common to all cores and the depth of the intervals is determined for Cores 3, 4 and RT-2 by the stratigraphic correlation (see Figure 4.4). Even-numbered intervals (II, IV, VI) contain the lowest LOI values, and the thickest inorganic layers, while odd intervals (I, III, V) have higher average LOI values and fewer and thinner inorganic layers. The clustering of the inorganic layers into three, easily-identifiable intervals in each of the cores suggests that frequency of layer deposition is not constant throughout the core (Figure 4.5). The time between events in the even intervals is highly variable, whereas the time between events is shorter in odd intervals.

### 4.3 Inorganic Layer Emplacement

Layer i, in Core 2, is the interval of the core for which the most (nine) lab analyses have been performed (Figure 4.6). This layer was chosen as representative of the thickest graded beds in the core, and these data are used to constrain the interpretation of possible emplacement mechanisms for this and other inorganic layers.

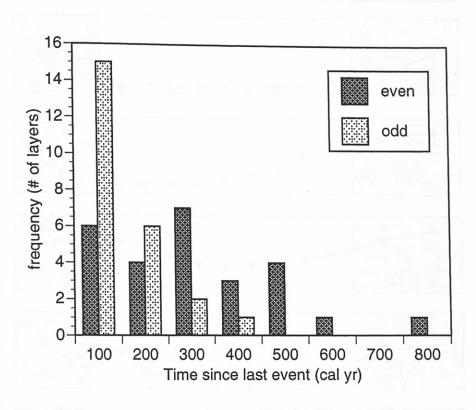
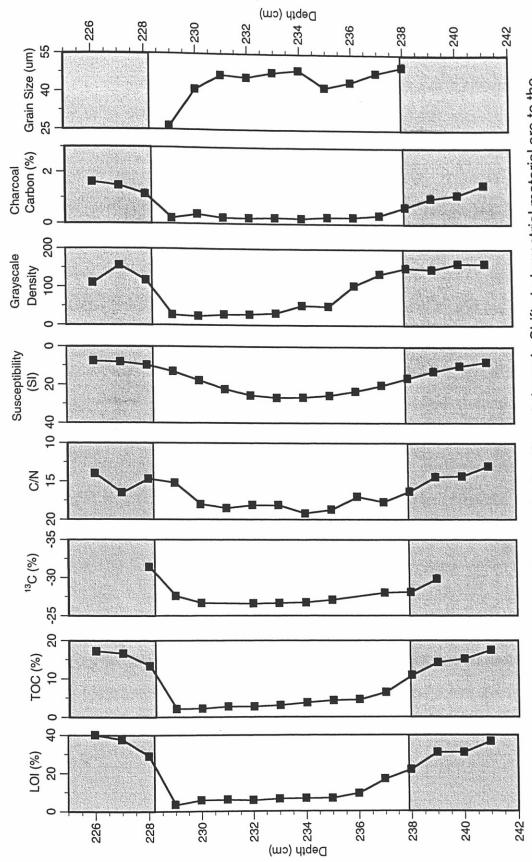


Figure 4.5 Layer frequency as a function of time since the last event. Even and odd intervals exhibit different trends.



gyttja above (2720 <sup>14</sup>C ybp) and below (2490 <sup>14</sup>C ybp) the inorganic layer exhibit an age inversion (Bierman et al., 1997). Figure 4.6 Summary data for layer emplacement using Core 2, layer i. Shifts to terrestrial material are to the left; shifts to the right indicate aquatic material (with the exception of the grain size data). Radiocarbon dated

#### 4.3.1 Physical Characteristics

Layer i was visually estimated to extend from depth 228 to 238 cm, with sharp upper and lower boundaries and internal grading. LOI and TOC data show a 2-cm transition from silt to gyttja at the base beginning at depth 238 cm, a well-mixed center 8 cm thick, and an abrupt change back to gyttja at depth 228 cm. This trend is also present in the grayscale density data, although the lower transition from gyttja to silt appears to begin 1 cm higher, and the well-mixed center spans only 7 cm. The magnetic susceptibility data, due to the lower resolution of this record, show a gradual transition at both the top and the bottom, and have a maximum value at depth 233 cm, the center of the layer identified by LOI and TOC. These data suggest that the deposition of inorganic layers involves initial mixing of gyttja and silt followed by deposition of relatively organic-free, homogenous sand and silt, and then a return to gyttja deposition with little to no mixing at the layer top.

Grain size in layer i generally increases with depth, confirming the visual identification of the layer as a graded bed ranging from coarse to fine silt. The upward decrease in grain size is interrupted at depth 234 cm by 3 cm of coarser sediment. The grading continues at depth 231 cm with significantly finer material in the top 1 centimeter. Graded beds are deposited by the suspension settling of particles, the grain size of which is determined by the available sediment and the energy of the water. Grain size in Core 3, taken close to the lake margin, is significantly coarser than in Cores 2 and 4, located closer to the lake center. This decrease in grain size with distance from shore suggests deposition by a decelerating current carrying sediment toward the center of the lake.

## 4.3.2 Organic Matter Source

Stable carbon isotope values ( $\delta^{13}$ C) shift to less negative values with the transition from gyttja to silt, indicating a change from aquatic organic material to terrestrial organic material. This observation is supported by the visual identification of leaves, wood, and other macrofossils within the inorganic layers. The upper transition from silt back to gyttja is sharper than the lower transition, supporting the hypothesis that the deposition of the inorganic layers involves mixing with gyttja at the base, and not at the top. The intermediate values between the average gyttja ( $\delta^{13}$ C = -31‰) values and the average terrestrial ( $\delta^{13}$ C = -27‰) values for Ritterbush Pond could also be due to a third source of organic material such as macrophytes, or previously mixed terrestrial and aquatic material that is incorporated into the base of the layer.

C/N ratios support a terrestrial origin of the organic material in the inorganic layers, with values increasing from 15 to 20 toward depth 234, 1 cm below the center of the layer. The C/N values show a 2 cm transition to higher values at the base, and a jump to lower values 1 cm below the visually-identified top of the layer. The change in source of organic material from aquatic to terrestrial in this layer suggests the delivery of material to the lake from the surrounding hillslopes or lake margins. The data available do not allow me to distinguish between terrestrial and lake marginal (emergent macrophytes) sources for organic material.

### 4.3.3 Timing of Layer Deposition

Samples previously analyzed (Bierman et al, 1997) in Core RT-2 for radiocarbon include gyttja samples above and below three inorganic layers (i, q and t) that have been correlated to Core 2. Each of the 3 pairs exhibits an inversion in age; the date above the layer is consistently older than the date below the layer. For layer i the offset is 180 cal yr, for layer q it is 100 cal yr, and for layer t the offset is 200 cal yr. As the offset is not

within the analytic uncertainty of the ages (1  $\sigma$ ), and is systematic for each of the thickest, graded inorganic layers in the core, it is probably a function of the depositional mechanism for the inorganic layers.

The inversion of ages suggests that there is both erosion and deposition associated with the mechanism emplacing the inorganic layer. Bierman et al. (1997) propose initial scouring of sediments by turbidity currents at the lake margins, followed by deposition of the graded bed and then redeposition of the disturbed sediments on top of the turbidite. At the lake center, where the inversion is observed, the scouring would erode less sediment than at the lake margins; the net movement of the disturbed sediments toward the center of the lake creates the measured offset in age. A similar inversion was observed by Bondevik et al. (1997) in the gyttja above tsunami deposits that was 300-500 <sup>14</sup>C yr older than the material below and within the tsunami deposit. The offset was interpreted to be the post-tsunami reworking of older material exposed by tsunami scouring at the edges of the coastal lake basin. Both interpretations of the age offset invoke relatively rapid transport and deposition of allochthonous material by a sedimentation event, which disrupts the slow accumulation of lake-produced gyttja.

### 4.3.4 Emplacement Mechanisms

Together, the lithologic, organic matter characterization, radiocarbon, and grain size data suggest sedimentation mechanisms for the inorganic layers in Ritterbush Pond. The following criteria must be met by the emplacement mechanism(s): 1) rapid deposition of terrestrial material from suspension, 2) possible gyttja scouring and mixing with inorganic material at the base of the deposit, 3) fining of the deposit toward the center of the lake, and 4) deposition of both fine laminations and thick (>1 cm) layers. Mechanisms associated with event sedimentation in lakes include, but are not limited to: turbidity currents (density currents with a high concentration of dispersed sediment), plumes of

sediment that undergo suspension settling or evolve into density-driven bottom currents, reworking of lake marginal sediment by storm (wind and wave) generated bottom currents, and slumping of lake marginal or hillslope sediments (Gorsline, 1984).

Of these mechanisms, suspension settling would fail to produce significant scouring or mixing at the base of the deposit and sediment slumping not accompanied by suspension sedimentation would be unlikely to produce grading. Density-driven bottom currents and high-concentration turbidity currents are most likely to result in the set of characteristics observed in the thickest inorganic layers. Inorganic, graded beds described in lake sediment studies are often simply called turbidites (Ludlam, 1974). Controversy exists over the common characterization of graded beds and associated sedimentary structures, such as planar laminations, as turbidites (Bouma, 1962), due to abundant evidence that turbidites may exhibit a wide variety of features or none at all (Kuenen and Migliorini, 1950; Kuenen and Menard, 1952; Piper, 1972; Walker, 1967). Deposits conforming to the sequence typical of turbidite deposits may be produced by a variety of mechanisms (Shanmugam, 1997; Nelson, 1982).

One test of turbidity current emplacement employs the linear relationship between coarsest 1% grain size in the layer to layer thickness (Mehrtens, 1988). Turbidite thickness is positively correlated to slope, flow depth, and the grain size distribution of the sediment, which determine the velocity of a turbidite (Sadler, 1982). The velocity of the turbidite at the moment of layer emplacement controls the coarsest grain size that can be deposited; the size of the turbidite at the moment of emplacement controls the thickness of the deposit. The five representative layers analyzed for grain size, however, do not exhibit a clear relationship between the coarsest 1% grain size and the thickness of the layer (Figure 4.7). Combined with the absence of sedimentary structures associated with turbidity current deposition (Bouma, 1962), this lack of a grain size to thickness correlation does not provide sufficient evidence to determine if the inorganic layers

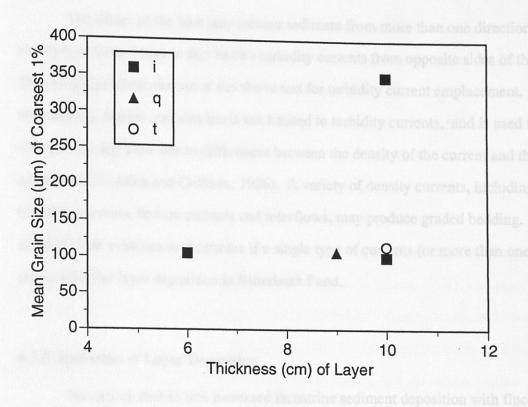


Figure 4.7 Test of emplacement mechanism for inorganic layers. The five thickest inorganic layers do not show a clear relationship between coarsest 1% of grains and layer thickness.

identified in Ritterbush Pond cores were emplaced by tubidity currents (Mehrtens, 1988; Sadler, 1982).

The center of the lake may receive sediment from more than one direction; the 10-cm layer in Core 2 may in fact be two turbidity currents from opposite sides of the lake. This would preclude the use of the above test for turbidity current emplacement. The term density current includes but is not limited to turbidity currents, and is used to characterize any flow due to differences between the density of the current and the ambient fluid (Allen and Collison, 1986). A variety of density currents, including turbidity currents, bottom currents and interflows, may produce graded bedding. There is not sufficient evidence to determine if a single type of currents (or more than one) is responsible for layer deposition in Ritterbush Pond.

### 4.3.5 Initiation of Layer Deposition

Numerous studies link increased lacustrine sediment deposition with fluctuations in the amount and intensity of rainfall. Recently, lake sediment research linked increased average grain size to storm occurrence (Campbell, 1998) and identified silt and clay layers within gyttja as products of individual storm events (Eden and Page, 1998). The sparse deposition of discontinuous sand layers (not-dated) in Mirror Lake has been attributed to storm-generated waves and currents at the lake margins redistributing sediment (Davis and Ford, 1984). Marshes and lakes in close proximity to the coast record hurricane generated sand layers (Liu and Fearn, 1993, Winkler, written comm., 1998). Nelson (1982) documented turbidite-mimicking sedimentary structures produced by post-storm-surge bottom currents on a marine shelf. Inorganic layer deposition in Ritterbush Pond is most likely initiated by hydrologic events, such as rainstorms and

spring snowmelt, which cause increased hillslope erosion and sediment transport to the lake.

The susceptibility of the hillslopes to erosion may also be increased by forest fires that strip the hillslopes of protective vegetation (Clark, 1988; Meyers et al., 1995).

Representative charcoal data for Core 2, layer i and the surrounding gyttja (Figure 4.6) show a decrease in charcoal abundance within the inorganic layer. Although this does not exclude the possibility that fires occurred in the surrounding watershed, or contributed to sediment availability for deposition, it does not support widespread, hillslope-clearing fires as a trigger for inorganic layer deposition.

Inorganic layers in sediment cores from the Puget Sound region (Adams, 1992), the Dead Sea (Ben-Menahem, 1976; Niemi and Ben-Avraham, 1994), and other areas, have been attributed to lake marginal slumps caused by seismic shocks, and used to document the paleoseismic activity of the region. Unlike these tectonically-active regions, Vermont is located in a relatively stable setting, and the largest historic earthquakes have not exceeded Richter magnitude 4.1. Vermont is proximal to several areas (the Adirondack Mountains, the White Mountains, and the Saint-Lawrence Valley) where larger earthquakes (up to magnitude 6.5) have been recorded (Ebel et al., 1995). A detailed study of lake sediment disturbance by earthquakes in the Charlevoix region of the Saint-Lawrence Valley, over 500 km from Ritterbush Pond, showed disturbance was limited to a radius of approximately 100 km from the seismic zone (Ouellet, 1997). Ritterbush Pond is also located more than 100 km away from other active seismic zones, minimizing the possibility that inorganic layer deposition is initiated by shaking associated with large earthquakes.

### 4.4 Age Control on Sedimentation

#### 4.4.1 Age Model

An average whole-core sedimentation rate (0.58 mm yr<sup>-1</sup>) can be estimated for Ritterbush Pond by dividing the depth of the oldest sample dated in Core 2 (548 cm) by its age (9440 cal yr BP). However, this rate (see Figure 3.13) does not account for the time discrepancy between the slow background sedimentation of gyttja, and the relatively rapid deposition of the inorganic layers that comprise 12% of the core. In order to portray more accurately changes in gyttja and inorganic layer sedimentation and model the age of individual inorganic layers, I constructed an age model based on the background accumulation of gyttja alone. Using the clustering of the inorganic layers to define six intervals, I systematically removed the inorganic layers from the stratigraphy and used calibrated radiocarbon dates at the top and bottom of each interval to calculate an age for each centimeter of gyttja within the interval (Figure 4.8). I then assigned an age to the location of each removed layer, creating a chronology of inorganic sedimentation events.

Inorganic layers are removed from the stratigraphy based on distinct changes in lithology identified at 1 cm intervals. Using the litho-stratigraphic logs, I noted the depth and thickness of each layer thicker than 5 mm. The model is insensitive to layers <5 mm, although the age of the thin layers can be calculated after age model construction. The TOC data were used to identify any additional 1-cm intervals containing inorganic material (TOC <5%) that was not identified visually. Each centimeter of material identified as containing significant inorganic matter, including centimeters containing several fine laminations, was then removed from the stratigraphy. The removal of the inorganic layers shortens the core by 67 cm. The percent inorganic material removed is calculated for each interval and is higher (18% to 49%) in the intervals where inorganic layers were clustered than in the intervals dominated by gyttja (<1%). Depth for each

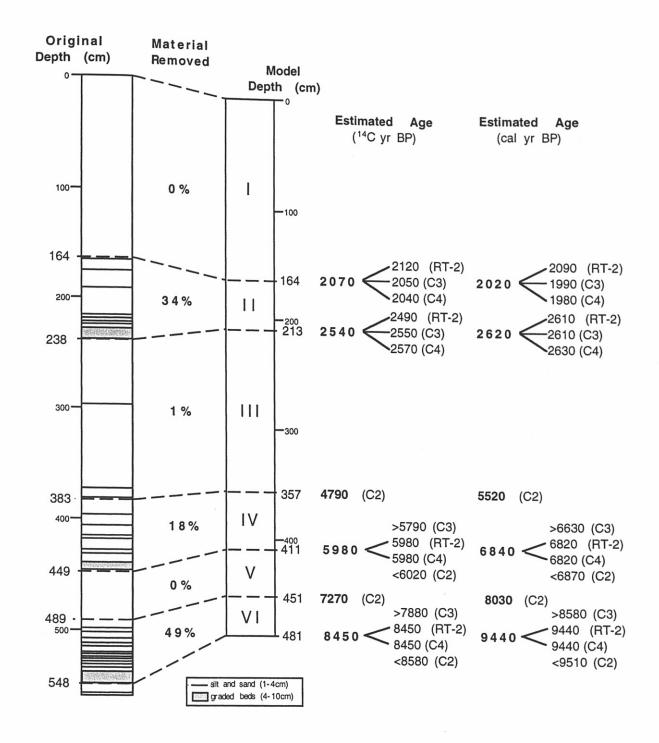


Figure 4.8 Compression of Core 2 for age modeling. Layers representing rapid deposition are removed (12% decrease in length) from the stratigraphy based on identification by logs, pictures, TOC and X-ray data. Ages (\frac{14}{C} and cal yr) bracketing each interval are estimates based on stratigraphically equivalent ages from all cores. Limiting ages (> or <) are not used in estimation.

centimeter of the core is recalculated as model depth to denote the removal of the inorganic horizons.

Dates (both <sup>14</sup>C and cal yr BP) from six depths in Core 2 used to construct the age model for Ritterbush Pond. Ages are derived from best estimates where stratigraphically equivalent samples from more than one core have been dated, and from depths dated only in Core 2 (Figure 4.8). A zero age is assigned to the top of the core (depth = 0 cm). Gyttja accumulation is modeled as linear between the upper and lower control points for each interval (Figure 4.9, Table 4.3).

### 4.4.2 Validity of the Age Model

Radiocarbon dated samples from the middle of intervals I, III and IV were used to check agreement with the modeled age (Figure 4.9). In interval IV, the age offset for model depth 395 cm (Core 2 depth 424 cm), is 80 years. A sample from interval III at model depth 275 cm (Core 2 depth 300 cm) also shows an offset of 80 years, which is within the analytic uncertainty for the dates. A sample was also dated for interval I at core depth 77 cm (730 cal yr BP), model depth 77 cm (947 cal yr BP) giving an offset of 220 years. Using all three ages for interval I, and modeling deposition as exponential (due to the lack of inorganic layers) does not significantly change the ages of the identified layers.

Continuous fine sediment (gyttja) resuspension and redeposition occurring due to seasonal lake turnover and lake marginal erosion, termed sediment focusing, can move sediment toward the lake center (Davis et al., 1984; Hilton, 1985; Lehman, 1975). Sediment focusing may result in the record in higher rates of gyttja accumulation in the lake center than at the lake margins, and thus a higher resolution sedimentation record. The age model I constructed is most likely an overestimation of basin-wide gyttja accumulation

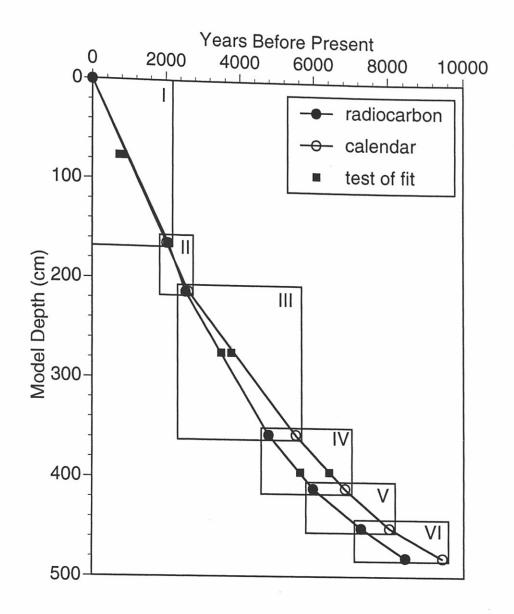


Figure 4.9 Age model for core 2. Accumulation rate is modeled as linear between age control points. Linear modeling was tested by independently dating samples from intervals I, III, and IV (squares).

Table 4.3 Age Model and Accumulation Rate Calculations for Core 2

A: Hadioc	A. naulocarbon year calculations	IdilOlis							
interval	14C yr BP	model depth (cm)	slope (yr cm <sup>-1</sup> )	linear intercept	sedimentation rate (cm yr <sup>-1</sup> )	bulk density (mg cm <sup>-2</sup> )	accumulation rate (mg cm <sup>-2</sup> yr <sup>-1</sup> )	average TOC (%) of interval	organic carbon (mg cm <sup>-2</sup> vr <sup>-1</sup> )
-	0- 2070	0-164	12.6	0.0	0.08	137	10.9	0.16	1.78
2	2070-2540	164-213	9.6	496.9	0.10	169	17.6	0.13	2.26
က	2540-4790	213-357	15.6	-788.1	90.0	225	14.4	0.15	2.23
4	4790-5980	357-411	22.0	-3077.2	0.05	196	8.9	0.14	1.20
2	5980-7270	411-451	32.3	-7274.8	0.03	250	7.8	0.17	1.34
9	7270-8450	451-481	39.3	-10469.3	0.03	222	5.6	0.14	0.77

		1113							
nterval	interval Calendar yr BP	model depth (cm)	slope (yr cm <sup>-1</sup> )	linear intercept	sedimentation rate (cm yr <sup>-1</sup> )	bulk density (mg cm <sup>-2</sup> )	accumulation rate (mg cm <sup>-2</sup> yr <sup>-1</sup> )	average TOC (%) of interval	average organic TOC (%) of carbon (mg interval cm <sup>-2</sup> yr <sup>-1</sup> )
1	0- 2020	0- 164	12.3	0.0	0.08	137	11.1	0.16	1.82
2	2020- 2620	164-213	12.2	11.8	0.08	169	13.8	0.13	1.77
ဗ	2620-5520	213-357	20.1	-1669.6	0.05	225	11.2	0.15	1.73
4	5520-6840	357-411	24.4	-3206.7	0.04	196	8.0	0.14	1.08
2	6840-8030	411-451	29.8	-5387.3	0.03	250	8.4	0.17	1.45
9	8030-9440	451-481	47.0	-13167.0	0.02	222	4.7	0.14	0.65
ote: The	note: The linear model is depth = slope *		age + linear intercept	intercept	vent. The magnitude fact observed between he is equivalent to 4				

rates, but if the rate of gyttja sediment focusing is steady, my model should portray accurately relative rate changes during the Holocene.

The deposition of inorganic layers in Ritterbush Pond is due to episodic sediment focusing events which are likely to disturb the temporal sequence of gyttja accumulation, as illustrated by the age inversion observed above the thickest graded layers (see section 4.3.3). Gyttja erosion and redeposition occurs during the emplacement of the thickest layers. Scouring at the base of the layer may decrease the estimated time since the preceding event; redeposition above the layer will increase the estimated time until the subsequent event. Since thick layers are more likely to generate greater erosion than thin layers, the amount of erosion and deposition will not be equal for each event. The close spacing of layers of varying thickness may result in both overestimates (thin on top of thick) and underestimates (thick on top of thin) of time since the last event. The magnitude of the disturbance of the gyttja stratigraphy can be estimated by the offset observed between the modeled and measured radiocarbon ages. The offset of 80 cal years is equivalent to 4 to 5 cm of gyttja, but within the analytic uncertainty of the dates. In addition, the removal of material visually identified as an inorganic layer during the creation of the age model, will also remove any gyttja mixed into the layer during transport from the lake margins. As I cannot quantify the sediment disturbance associated with each event, and because the age model has been demonstrated to be reasonably accurate, I use layer spacing as a proxy for time between events.

# 4.4.3 Gyttja Accumulation Rates

The average sedimentation rate calculated for each interval with the age model is used to estimate gyttja accumulation rates and changes in lake primary productivity. I use an average bulk density (Figure 4.10) for each interval to account for compaction and convert sedimentation rate (cm yr¹) to gyttja accumulation rate (mg cm² yr¹) (Figure 4.11, Table 4.3). I estimate the fraction of organic carbon in the gyttja by multiplying the accumulation rate by the average TOC (%) for the interval. The average TOC values were calculated after the removal of the inorganic layers from the stratigraphy, and represent the average organic carbon in the remaining sediment. Since the stable carbon isotope and C/N ratios indicate a primarily aquatic source for the organic carbon in the gyttja, I use the estimation of organic carbon accumulation rate as a proxy for changes in primary productivity in the lake. The calculated accumulation rate may also be influenced by down-core changes in decomposition of the organic material.

Gyttja accumulation rate, calculated for 1000 yr intervals, appears to generally increase from 9000 to 4000 cal yr BP, when the rate levels off at 11 mg cm<sup>-2</sup> yr<sup>-1</sup>. Superimposed on this trend are increases at 2000 to 3000 cal yr BP and 7000 to 8000 cal yr BP. These increased values coincide with clusters of inorganic layers and may be increased by episodic sediment focusing of gyttja due to event deposition, or increased primary productivity due to nutrient enrichment by the influx of terrestrial material (Figure 4.12).

Organic carbon shows an irregular increase in accumulation rate but also levels off (1.7 mg cm<sup>-2</sup> yr<sup>-1</sup>) at 4000 cal yr BP, with peaks at 5000 to 6000 cal yr BP and 7000 to 8000 cal yr BP. The coincidence of the increase in both gyttja and organic carbon accumulation from 7000 to 8000 cal yr BP suggests that inorganic layer deposition may have been accompanied by gyttja sediment focusing. The absence of an increase in

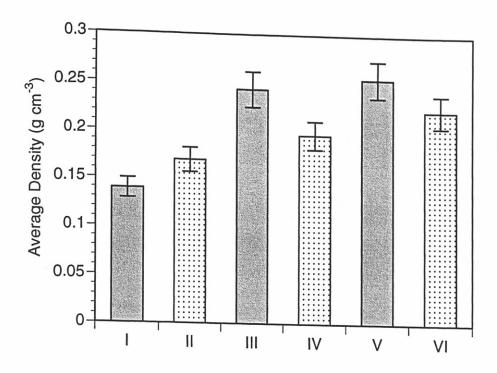


Figure 4.10 Average bulk density and standard deviation ( $1\sigma$ ) for each interval. Even intervals, dominated by inorganic layers, show less increase in density with depth.

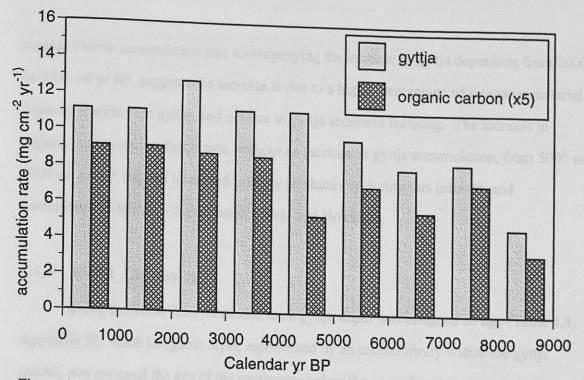


Figure 4.11 Gyttja and organic carbon accumulation rates for Core 2. Calendar year intervals (1000 yr) show increasing rates of gyttja and organic carbon accumulation prior to 4000 cal yr BP.

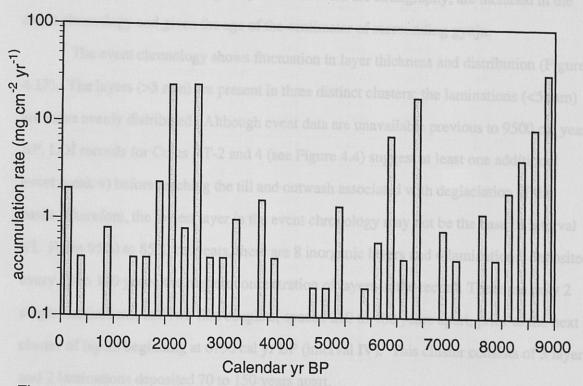


Figure 4.12 Inorganic layer accumulation rates for Core 2. Calendar year intervals (250 yr) show 3 clusters of layer deposition at 2000 to 3000, 6000 to 7000, and prior to 8500 cal yr BP.

organic carbon accumulation rate accompanying the increase in gyttja deposition from 2000 to 3000 cal yr BP, suggests the increase is due to a higher percentage of inorganic material deposition within the gyttja, and not due to gyttja sediment focusing. The increase in organic carbon accumulation rate, without an increase in gyttja accumulation, from 5000 to 6000 cal yr BP, implies increased primary productivity during this interval, and corresponds to the well-documented warm, mid Holocene.

# 4.4.4 Event Chronology

Using the linear interval model, each gyttja depth was assigned an age (Table 4.4, Appendix E). Each inorganic layer, represented by an unconformity within the gyttja model, was assigned the age of the centimeter below the unconformity, a maximum age for the depositional event. Millimeter-scale laminations identified by litho-stratigraphic logs and X-radiographs, but not originally removed from the stratigraphy, are included in the event chronology and given the age of the centimeter of surrounding gyttja.

The event chronology shows fluctuation in layer thickness and distribution (Figure 4.13). The layers (>5 mm) are present in three distinct clusters; the laminations (<5 mm) are more evenly distributed. Although event data are unavailable previous to 9500 cal years BP, LOI records for Cores RT-2 and 4 (see Figure 4.4) suggest at least one additional event (peak v) before reaching the till and outwash associated with deglaciation of the basin. Therefore, the lowest layer in the event chronology may not be the base of interval VI. From 9500 to 8500 cal years, there are 8 inorganic layers and 4 laminations, deposited every 50 to 190 years, the highest concentration of layers in the record. There are only 2 single laminations, and two fine couplets, spaced 210 to 480 years apart, prior to the next cluster of layers beginning at 6750 cal yr BP (interval IV). This cluster consists of 3 layers and 2 laminations deposited 70 to 150 years apart.

Table 4.4 Modeled Layer Age in Radiocarbon and Calendar Years for Core 2

Interval				thickness	equivalent	ars for Core 2		
mervar	peak'	layer <sup>2</sup>	depth (cm)	thickness (cm)	gyttja	model age	model age	time since last event
1	aa	1	4.5		depth	(14C yr BP)	(cal yr BP)	(cal yr)
	a	2	4-5	1	5	63	62	319
		3	30.8-31.0	0.2	31	391	381	382
	b	4	61.0-61.2	0.2	62	781	763	160
	c	5	74.6-74.8	0.2	75	945	923	356
	ŭ	6	103.8-104.0	0.2	104	1310	1279	259
	d	7	124.7-124.9	0.2	125	1575	1538	221
II	е	8	142-143	1	143	1802	1759	209
		9	159.0-159.2	0.2	160	2016	1968	57
	f		164-167	3	165	2081	2025	73
		10	173-177	4	171	2139	2098	134
	g h	11	188-193	5	182	2244	2232	122
	"	12	203-204	c (0.2)	192	2340	2354	159
		13	217-219	2	205	2465	2513	24
		14	221-222	1	207	2484	2537	25
		15	224.0-224.2	0.2	209	2503	2562	58
III	<u> </u>	16	228-237	9	213	2540	2620	333
	j	17	254.5-254.7	0.2	230	2800	2953	81
		18	258.5-258.7	0.2	234	2862	3034	241
	ij	19	270.5-271.0	0.5	246	3050	3275	523
	k	20	296.0-296.3	0.3	272	3455	3798	
		21	305.0-305.5	0.5	280	3502	3858	60
		22	309.4-309.5	0.1	284	3642	4039	181
		23	319.0-319.1	0.1	294	3798	4240	201
	1	24	355.0-355.1	0.1	330	4360	4963	723
		25	358.0-358.1	0.1	333	4407	5024	61
	m	26	371.8-372.0	0.2	346	4610	5285	261
		27	373.0-373.2	0.2	348	4641	5325	40
		28	380.0-380.3	0.3	355	4750		141
IV		29	397.8-397.9	0.1	372	5107	5466 5870	404
	n	30	406.2-406.7	c (0.1)	381	5305		220
		31	411.3-411.4	0.1	385	5393	6090	97
	0	32	415.2-416.0	0.8	391	5525	6187	147
	р	33	420-423	3	395	5613	6334	97
		34	426.5-426.6	0.1	398	5679	6431	74
		35	431.8-431.9	0.1	403		6505	122
	q	36	439.5-449.0	9.5	411	5789	6627	213
٧	r	37	461.1-461.8	c (0.2)	423	5980	6840	441
		38	477.5-477.7	0.2	439	6388	7281	414
VI	S	39	492-493	c (0.3)	454	6905	7695	476
		40	497.4-497.6	0.2		7373	8171	282
		41	501-502	1	460	7609	8453	141
		42	506-508	2	463	7727	8594	188
		43	511.5-511.6		467	7884	8782	141
		44	512.6-512.7	0.1	468	8002	8923	47
	t	45	513-514	0.1	471	8041	8970	47
		46	516.0-516.1	1	472	8080	9017	94
		47		0.1	473	8159	9111	47
			517.5-520.0	2.5	475	8198	9158	47
		48	521-522	1	476	8238	9205	47
		49	523-525	2	477	8277	9252	47
		50	526-532	c (1.5)	478	8316	9299	94
		51	533-535	2	479	8395	9393	47
	ed in Co	52	537-547	10	481	8434	9440	235 <sup>3</sup>

<sup>&</sup>lt;sup>1</sup> as identified in Core 2 <sup>2</sup> layers identified by litho-stratigraphic logs, X-radiographs and TOC

<sup>&</sup>lt;sup>3</sup> estimated from lithostratigraphic logs and accumulation rate of interval VI

c = couplet, layer thickness in ()

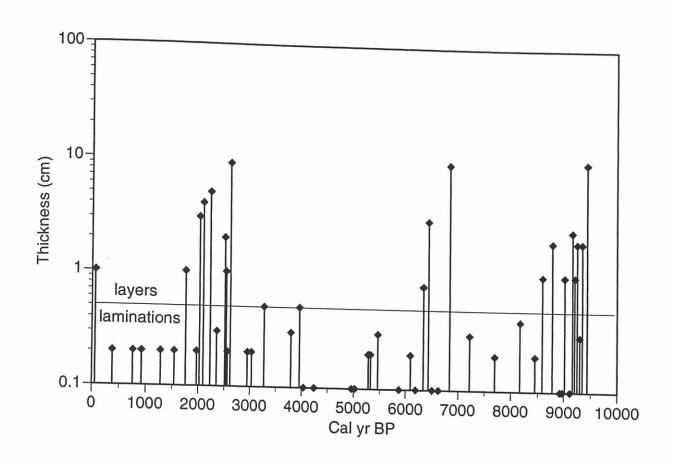


Figure 4.13 Layer thickness vs. calendar age. Solid line at 0.5 cm divides layers from laminations.

From 6250 to 2750 cal yr BP (interval III), 14 laminations and one couplet occur 40 to 720 years apart. The next cluster of layers, from 2750 to 2000 cal yr BP (interval II), contains 6 layers, 2 laminations, and 2 couplets that were deposited 20 to 160 years apart. The frequency of deposition decreases again in interval 1, where only one layer and 6 laminations were identified, ranging 160 - 380 years apart. The youngest individual layer identified, estimated at 62 cal yr BP, is a diffuse centimeter of macrofossil rich sand, and is the only evidence of event deposition in the last 300 years. In even intervals where the inorganic layers cluster, the thickest layer is consistently at the base of the interval. Subsequent layers decrease in thickness in each of the intervals.

## CHAPTER 5 - Discussion

The chronology of inorganic sediment layers in Ritterbush Pond is a record of both the frequency and magnitude of hydrologic events, and provides a detailed erosional history for the watershed. This chapter summarizes the geomorphic and hydrologic controls on sediment transport to Ritterbush Pond and investigates using the Ritterbush record as a proxy for storm frequency during the Holocene. I then use historic storm records to determine the types of events capable of depositing an inorganic layer in the lake, and compare the Ritterbush event chronology to other global climate records for the Holocene.

## 5.1 Event Sedimentation in Ritterbush Pond

# 5.1.1 Sedimentation Dynamics of the Ritterbush Watershed

The Ritterbush Pond cores provide a detailed record of discrete sedimentation events. The sand and silt layers are terrestrially-derived sediment, transported from the lake margins toward the lake center, probably by density currents. The transport of sediment to the lake is most likely caused by episodic increases in stream flow, which erode stream channels, stream banks, and lake margins (see section 4.3.5). However, similar inorganic layers have not been found in sediment cores from Sterling Pond (Bierman et al., 1997) or Richmond Pond, both located in Vermont's Green Mountains. Nor do other New England lakes, extensively cored for de-glacial and pollen research, exhibit recurrent episodes of terrestrial sediment deposition during the last 9000 <sup>14</sup>C years (Davis et al., 1984; Thompson et al., 1996).

The physical characteristics of the Ritterbush Pond watershed strongly influence the sensitivity of the hillslopes and stream channels to erosion. Similar to other Vermont

lakes, the watershed is forested, relatively small (<3 km²), and has significant bedrock outcrops. In contrast to the other cored ponds, Ritterbush Pond has steep hillslopes on all sides. Although the vegetation in the watershed limits hillslope erosion and mass movement during moderate hydrologic events, the steep slopes increase the velocity of runoff once the ground is saturated (Dunne and Leopold, 1978; Ritter et al., 1993). During severe hydrologic events, high-velocity saturation overland flow results in short periods of intense stream discharge, maximizing the potential for channel scouring and bank erosion. Streams draining watersheds with lower relief, such as Sterling Pond, are likely to have less-peaked hydrographs, decreasing runoff rates and thus sediment transport potential during intense precipitation events.

Once sediments reach Ritterbush Pond, their preservation potential is enhanced by lake bathymetry. Unlike the gentle, shallow bathymetry of Richmond Pond, Ritterbush Pond has a deeper, bowl-shaped basin. The movement of sediment stored at the shallow lake margins, where streams lose competence and build deltas, toward the deep flat center of the lake, is facilitated by steep inner lake slopes conducive to sediment resuspension and density-current transport. Additionally, the steep lake slopes minimize the removal of material from the lake center once it has been deposited. Shallower basins with lower outlets may experience resuspension and transport of fine-grained sediment from the lake during periods of high discharge.

### 5.1.2 Effect of Precipitation Events on Sedimentation

The deposition of terrestrial material in Ritterbush Pond occurred episodically throughout the Holocene, suggesting temporary changes in the erosion dynamics of the watershed. Increases in runoff and streamflow, the primary cause of layer deposition, are due to hydrologic events such as rainstorms and spring snowmelt. Very large and damaging floods have been generated by snowmelt alone, and rain on melting snow,

from March to May in New England (Ludlam, 1996). However, the Ritterbush watershed is less likely to experience such flooding, even if the entire snowpack were to melt rapidly, due to the small size of the drainage basin. Additionally, the range of hillslope gradient, elevation and aspect within the Ritterbush watershed, would result in varying rates of snowmelt, and stagger water release from the snowpack (Dunne and Leopold, 1978). Futhermore, hydrologic events occurring during the winter and early spring are probably less likely to result in layer deposition due thick ice cover on the lake.

Precipitation events cause sediment deposition in Ritterbush Pond due to increased sediment erosion from hillslopes and transport to the lake by streams.

Precipitation percolates through the thin, moderately well-drained soils, and moves as subsurface stormflow along the bedrock or impervious till substrate to stream channels (Babcock, 1979; Fetter, 1994). Once the soils are saturated, downslope transport of runoff occurs even more rapidly as saturation overland flow, which reaches the stream channels up to 100 times faster than subsurface stormflow (Dunne and Leopold, 1978). The resulting rise in stream discharge increases shear stress and flow velocity at the base and sides of the channel, resulting in a greater volume of material moved by bedload transport, and an increase in the grain size of the particles in the suspended load (Ritter et al., 1995). In the Ritterbush watershed, increased stream flow may result in the scouring of sediment from channel bottoms, and especially where streams run over bedrock or well-consolidated till, the erosion of channel banks by lateral channel migration. The volume and grain size of sediment transported to Ritterbush Pond should generally increase with increasing storm runoff and the resulting stream discharge.

Storm events may also influence sediment deposition in Ritterbush Pond by increasing wave and current activity at the lake margins. Although the basin is small, wind-generated waves may resuspend sediment stored at the lake margins; wind-generated currents, and increased inflow from streams, may alter lake circulation patterns

and transport lake marginal material toward the center of the lake (Horne and Goldman, 1994). Sediment-laden streamflow may cause oversteepening and failure of the delta slopes. Regardless of the exact source for sediment, or the specific mode of transport to the lake, the deposition of each inorganic layer is probably driven by a discrete hydrologic event.

# 5.1.3 The Ritterbush Event Chronology

If each inorganic layer in Ritterbush Pond represents a erosional event in the watershed, event frequency and magnitude, has fluctuated during the Holocene. Layer frequency, the time between depositional events as calculated by the age model, may be used to estimate the recurrence intervals of hydrologic events large enough to cause layer deposition (see section 4.4.2). The average event recurrence interval for odd intervals is  $270 \pm 170$  cal yr BP, and the average event recurrence for the even intervals is  $130 \pm 100$  cal yr BP. The more frequent event recurrence during the even-numbered intervals suggests periodic changes in the frequency of the largest hydrologic events during the Holocene.

Layer thickness, however, is an uncertain proxy for storm magnitude. In even intervals, layer thickness appears to increase with time since the preceding event, for all events > 2 cm thick (Figure 5.1). This correspondence suggests that layer thickness and/or storm magnitude may depend on the time elapsed between events. In odd intervals, where all layers are thin, and in parts of even intervals where layers are < 2 cm thick, layers exhibit a wide range of recurrence intervals, suggesting that for thin layers, thickness may better indicate the magnitude of the storm event. Accordingly, I conclude that 1) layers > 2 cm thick probably indicate storm events larger than layers < 2 cm thick, but are not necessarily correlative to storm magnitude, and 2) layers ranging from 0.1 to 2 cm thick may represent a range in storm magnitudes.

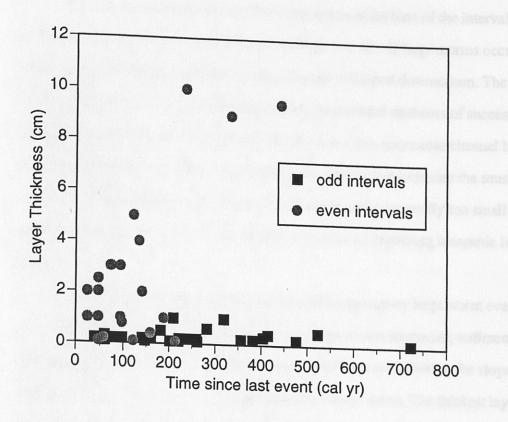


Figure 5.1 Layer thickness as a function of calendar years since the last event. In even intervals, layer thickness increases with time since last event for layers thicker than 1 cm. Thinner layers, occurring in both odd and even intervals, do not exhibit dependence on time since last event.

In the even intervals, the thickest layer occurs at the base of the interval, and subsequent layers decrease in thickness (see Figure 4.13). If large storms occur frequently, sediment stored in the stream channels is flushed downstream. The reduced availability of easily mobilized sediment limits the potential thickness of successive inorganic deposits in the lake. Conversely, the first storm may cause channel bank collapse or hillslope failure that exposes new surfaces to erosion, and increases the sensitivity of the watershed to subsequent storm events. Successive storms, normally too small to cause significant sediment transport, would then be capable of depositing inorganic layers in the lake.

The removal of easily eroded sediment from storage by large storm events seems more probable than the lingering effects of previous storms increasing sediment yield. The elapsed time between events is always greater than 50 years, allowing for slope stabilization and the regrowth of vegetation after a large storm. The thickest layer at the base of each even interval is thus an accurate reflection of the erosion and sedimentation potential of a larger-than-average storm, when abundant sediment is available. The second event in a pair of closely spaced events, may be of greater magnitude, but because less sediment is available, may deposit a thinner layer. Therefore, while the spacing of the layers may be used to estimate storm frequency (assuming negligible erosion and redeposition of gyttja during layer deposition) and the occurrence of thicker layers in even intervals suggests larger storm events, the relative thickness of layers within even intervals may not be an accurate proxy for magnitude of the storm event.

The magnitude of floods, large storm events, and the annual maximum series of 24-hour precipitation totals often fit an extreme-value probability distribution (Hershfield and Kohler, 1960; Dunne and Leopold, 1978). If the thickness of the inorganic layers corresponds to storm magnitude, and is not dependent on sediment availability, then the occurrence of such layers should conform to the extreme-value distribution. The

probability distribution of layers less than 0.5 cm thick fit an extreme value distribution, suggesting that thickness reflects storm magnitude (Figure 5.2). Thicker layers also show correspondence, but with a steeper linear fit that is discontinuous between layers less than 5 cm, and layers greater than 8 cm thick. The discontinuity of the linear fit implies dependence on a factor other than storm magnitude, such as sediment availability, for layers greater than 0.5 cm. Interestingly, the distinct break in slope between thin layers and thick layers corresponds well with the layer thickness occurring in odd and even intervals. Layers thicker than 1 cm occur only within even intervals, possibly indicating a change in factors controlling layer deposition (including storm magnitude, storm frequency and sediment availability) during even-numbered intervals.

# 5.2 New England Climate Records

The three even intervals (II, IV, VI), representing an increased frequency of large storm events in Ritterbush Pond, last 500 to 1,000 calendar years. The lack of large events during the thousands of years separating these intervals suggests that the frequency of layer deposition may be influenced by fluctuations in regional climate. In the northeastern United States, general trends in average precipitation, temperature, and vegetation since deglaciation have been reconstructed using specific pollen abundance as a climate proxy record (Jackson and Whitehead, 1991; Lin, 1996; Spear et al., 1994). Although the exact timing varies, all proxy records suggest a gradual rise in temperature following deglaciation, maximum warmth in the mid-Holocene (the hypsithermal), and cooling toward present climate conditions (Figure 5.3). The wettest period of the Holocene, as interpreted from lake-level curves (Webb, et al., 1993), occurred from 8000 to 6000 <sup>14</sup>C yr BP. The pollen chronology for Ritterbush Pond suggests warm, moist conditions

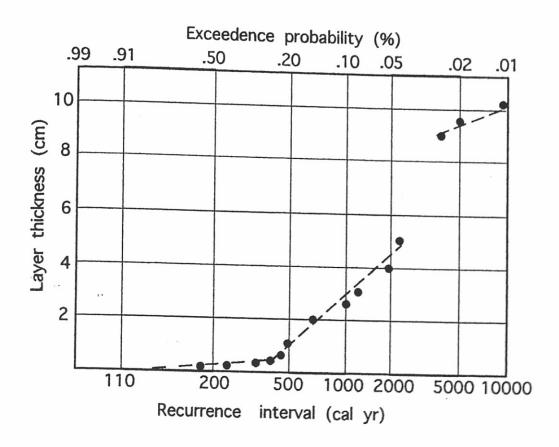


Figure 5.2 Extreme value probability distribution of inorganic layer thickness in Ritterbush Pond cores. When more than one layer of the same thickness occurs, the highest probability is graphed. Thin layers (<0.5 cm) conform to the extreme value distribution; thick layers fit a discontinuous linear distribution.

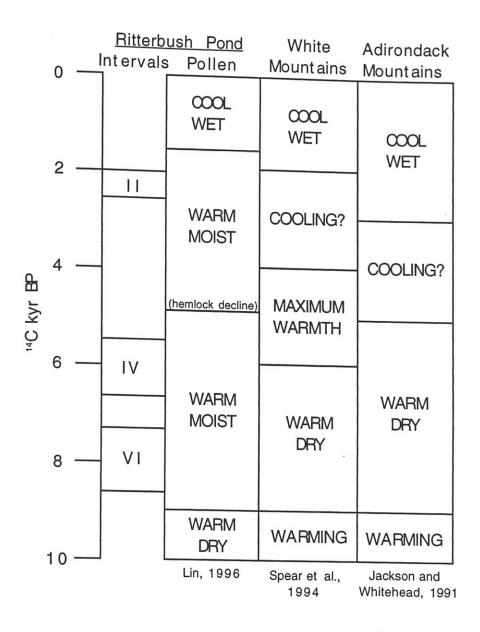


Figure 5.3 Summary of Holocene Climate Proxy (Pollen) Data for the northeastern United States in  $^{14}$ C yr BP.

from 9000 to  $1600\,^{14}$ C yr BP, spanning all three intervals of increased inorganic layer deposition.

The lack of correspondence between intervals of increased layer deposition with any particular regional climate regime suggests that the increase in storm activity is not necessarily caused, or accompanied, by changes in average climate conditions, primarily mean annual precipitation, that control watershed vegetation. If the increased frequency of layer deposition indicates a prolonged period (up to 1000 years) of increased precipitation, then this change should be, but is not, reflected by a shift in vegetation. A single storm event, however, is unlikely to impact the watershed sufficiently to cause vegetation changes significant enough to be detected by pollen analysis. Clusters of inorganic layers most likely represent clusters of extreme hydrologic events not detected by the pollen data.

# 5.3 Frequency and Magnitude of Vermont Storms

Extreme storms causing layer deposition in Ritterbush Pond, whether local or regional events, will remain undetected by climate proxy records that integrate over long time periods and wide areas. However, 200 years of written and anecdotal history provide a regional record of storm magnitude and frequency that is a potential analog for prehistoric and Holocene storm activity at Ritterbush Pond.

# 5.3.1 Historic Storms in Vermont and at Ritterbush Pond

Large or intense rain storms in Vermont fall into two basic categories: low-pressure, or frontal, storm systems that interact with tropical air, and localized thunderstorms (NOAA, 1982). These storms result in different duration, intensities, and distributions of precipitation. Thunderstorms tend to be of shorter duration and localized, while frontal systems last longer and cover wider areas (NOAA, 1982). In Vermont,

intense, shorter thunderstorms have a higher probability of occurring earlier in the summer than longer-lived but low-intensity frontal storms (Figure 5.4). Intensity-frequency-duration curves for Burlington and Northfield (located in central Vermont) quantify the higher intensity of shorter storms (Figure 5.5). Studies of regional and spatial distribution of storms suggest that it is not possible to determine the type of storm (frontal or thunderstorm) using only precipitation data from a single weather station (Hershfield and Wilson, 1960). The regional extent of any storm can only be determined by comparison with similar records from other locations. Although the type of storm event represented by an inorganic layer can not be determined, the Ritterbush Pond record has the potential to record both localized thunderstorms and regional frontal storm systems.

The largest rainstorm in Vermont's recorded history occurred in November 1927, due to the collision of a frontal system with tropical air. The entire state received between 5 and 9 inches of rain over two days (Ludlam, 1996). Isoheyetal maps for the storm estimate that the Ritterbush watershed received approximately 7 inches of rain over 2 days (Kinnison, 1930). The 1927 flood was preceded by 3 rainstorms, each just over a week apart, making average rainfall during October 150% higher than normal (Ludlam, 1996). The second largest state-wide storm occurred in 1938, when a what was a Class 3 hurricane tracked diagonally southeast to northwest across Vermont, dropping more than 3 inches of rain in the south in 24-hours, and resulting in five-day totals of 5 to 8 inches across the state (Coch, 1995; Ludlam, 1996). Saturation of the soils by heavy rains prior to the hurricane favored increased runoff and resulted in widespread flooding throughout the state (Ludlam, 1996).

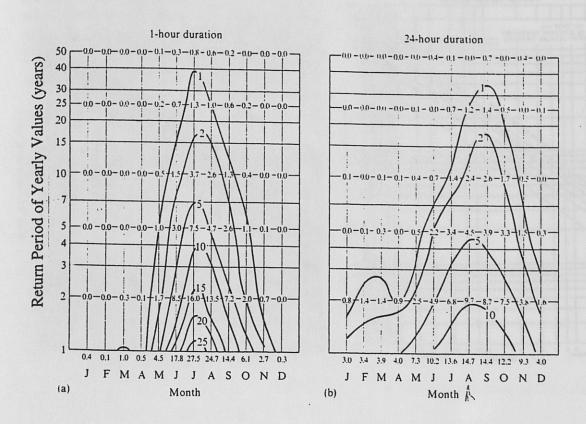


Figure 5.4 Seasonal probability of intense precipitation for the northeastern United States, from U.S. Weather Bureau (1959). Contours indicate the percent probability for each month of obtaining precipitation equal to or exceeding each return period value. Intense 1-hour storms are most likely to occur in July, while intense 24-hour rainfall has the highest probability of occurring in September.

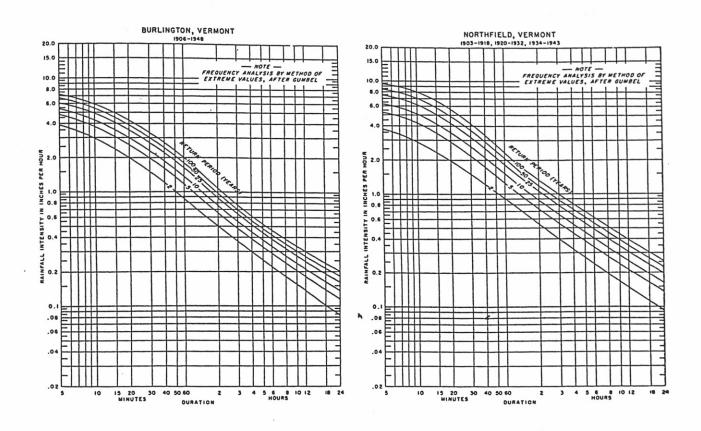


Figure 5.5 Rainfall intensity-duration-frequency curves for Burlington and Northfield, Vermont, from U.S. Weather Bureau (1955). For all return periods, short-duration rainfall events have higher rainfall intensity than long-duration events. Comparing rainfall intensity values for Burlington and Northfield (approx 1000 ft higher in elevation) suggests a dependence of rainfall amount on elevation.

In Ritterbush Pond, only one inorganic layer was deposited in the last 350 years. This layer consists of 1 cm of indistinct, disturbed, organic-rich sand. The age model suggests this layer was deposited about 1935 AD. I estimate that this diffuse sand layer, located in the liquid upper 10 cm of the core would probably correspond to less than 0.5 cm of sand if compressed, placing it among the events where magnitude does correlate to layer thickness in both even and odd intervals. Considering the uncertainty associated with this age, the deposition could represent either the 1927 or 1938 storm. If the largest statewide storms recorded in 200 years produced only 1 cm of sand, then the deposition of 10 cm of sand suggests a storm of much greater magnitude than witnessed historically.

# 5.3.3 The Potential Magnitude of Large Storm Events

Based on historic precipitation records and a combination of physical storm system modeling and estimation of meteorological parameters, the National Weather Service (NWS) has made regional estimates of the probable maximum precipitation (PMP) for a six hour period (US Weather Bureau, 1956). The PMP for all of northern Vermont is estimated between 18 and 20 inches (US Weather Bureau, 1961). These estimates are used to indicate the order of magnitude of extremely rare rainfalls. The PMP for Ritterbush Pond is estimated at 19 inches in 6 hours, almost three times the amount that resulted from the 1927 storm over 2 days (Table 5.1).

In 1969, Hurricane Camille hit central Virginia, causing massive hillslope failure, flooding, and general devastation (Williams and Guy, 1973). The PMP estimate for this region is 26 to 30 inches in 6 hours (US Weather Bureau, 1960). Camille delivered 24 inches in 8 hours (Williams and Guy, 1973), suggesting that the PMP is a reasonable estimate of extreme precipitation. Catastrophic rainfall events are required to produce significant debris-flows in the Appalachians (Kochel, 1990), but as the duration

Table 5.1 Rainfall Intensity Estimates for Extreme Events at Ritterbush Pond

Source (Rationale)	Kinnison, 1939 (isohyetal map)	*Burlington *1.35	U.S. Weather Bureau, 1961 (isohyetal map)	*Burlington *2
Normalized Intensity (cm hr -1)	0.4	0.7	8	10.7
Intensity	7 in / 48 hr	6.2 in / 24 hr	19 in / 6 hr	4.2 in / 1 hr
Return Period	107 yr	100 yr	N/A	100 yr
Estimate	1927	24-hour max	PMP	1-hour max

\* Burlington data (NWS, 1998) adjusted (section 5.3.3) for elevation (24-hour max) and intensity (1-hour max) according to Dunne and Leopold (1978). of a storm increases, the intensity of rainfall required decreases (Figure 5.6). Although there is little evidence of recent debris flows or mass movement in the Ritterbush basin, potentially the PMP storm would drop enough precipitation to destabilize steep slopes (Kochel, 1990).

The longest daily precipitation record for Vermont begins in 1893 and is from Burlington, located on Lake Champlain, approximately 50 km to the southwest of Ritterbush Pond. The 24-hour annual maximum data for Burlington have an extreme value probability distribution (Figure 5.7). The highest value, 4.49 inches, was recorded during the 1927 storm, and represents the 107-year storm event. The 1938 storm does not appear in this record. The second and third largest values are attributed to localized, intense thunderstorms in the Burlington area. The correspondence of the annual maximum series to the extreme value distribution implies that the 1927 storm is within the expected values given the current weather patterns; although a rare event, the 1927 storm is consistent with the past century of weather observations.

Using the isoheytal maps for the 1927 storm, an estimate can be made of the minimum magnitude storm needed to initiate sediment deposition in Ritterbush Pond. The precipitation estimate for Ritterbush Pond during the 2-day 1927 storm is 7 inches (Kinnison, 1939). Given the same antecedent soil conditions (saturated) and sediment availability, 7 inches of rain over 2 days on saturated ground is capable of depositing a thin inorganic layer in the lake. The 1927 storm is just sufficient to generate slope failure according to the data compiled by Kochel (1990) (Figure 5.6).

Precipitation data are not available for Ritterbush Pond, but Burlington data can be used to estimate precipitation for the Ritterbush watershed. Burlington data underestimate the magnitude of precipitation events at Ritterbush Pond. Mean annual precipitation

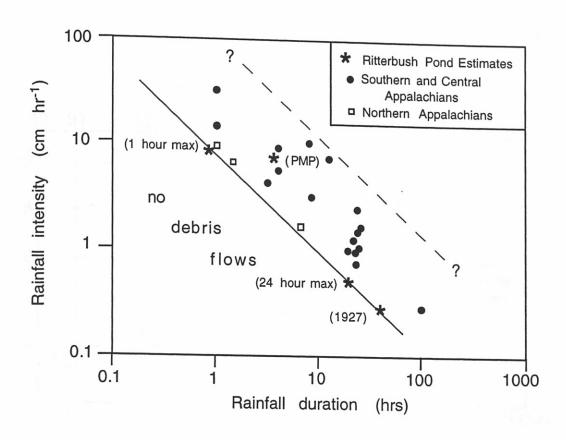


Figure 5.6 Intensity-duration relationship for major, debris-flow producing storms in the Appalachians, from Kochel (1990). Estimates of maximum intensity storms at Ritterbush Pond (Table 5.1) are plotted with asterisks and all estimates fall just within the envelope projected to generate slope failure on steep, forested hillsides.

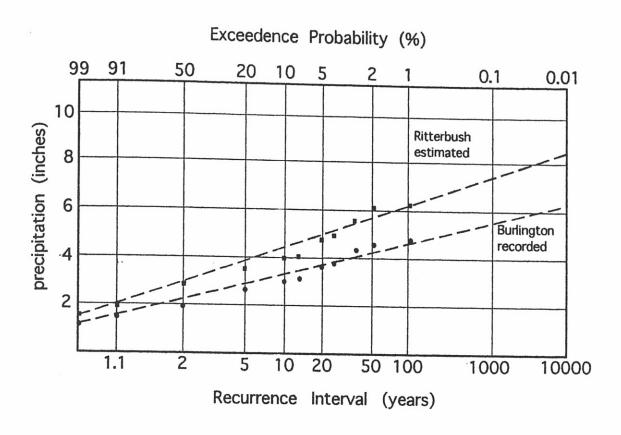


Figure 5.7 Extreme value distribution of 24-hour annual maximum precipitation data for Burlington (NWS, 1998). Burlington data are scaled by 35% to estimate Ritterbush Pond precipitation.

data from northeastern Vermont are positively correlated to elevation (Eq. 1) (NWS, 1998; Dunne and Leopold, 1978),

$$y = 0.0093x + 33.7$$
where y = precipitation (inches)
$$x = elevation (ft)$$
(1)

suggesting that Ritterbush Pond (1430 ft) receives 140% the precipitation of Burlington (320 ft). The isoheyetal maps from the 1927 storm show maximum values along the axis of the Green Mountains (Kinnison, 1930); and Ritterbush Pond (7 in) received 130% of Burlington rainfall (5.5 in) during the 1927 storm. Therefore, for regional precipitation events, Ritterbush Pond probably receives 30% to 40% more precipitation on average than Burlington. By scaling the Burlington data by 35%, the magnitude of the 100 year, 24-hour storm is estimated for Ritterbush Pond as 7.2 inches (Figure 5.7).

Since localized, intense storms may also cause layer deposition in Ritterbush Pond, it would be useful to estimate their potential magnitude as well. When short duration precipitation data are unavailable for a specific location, Dunne and Leopold (1978) suggest that an estimate of maximum event magnitude can be made by doubling the recorded value from a nearby station. For example, in a small (<20 mi²), forested watershed in Ohio, the rainfall resulting from a short duration thunderstorm was carefully quantified (McGuinness and Harrold, 1965). Several gauges within the watershed recorded almost 4.5 inches in one hour, but the storm was not even recorded by the regional long-term weather station. The US Weather Bureau estimates for the region that the 1-hour, 100-yr storm event would produce approximately 2 inches of rain, less than half the maximum recorded during the event. Following the method and using Burlington precipitation data, doubling the 1-hour, 100-year storm event maximum of 2.1 inches (NWS, 1998) results in an estimate of 4.2 inches for the 100-year, 1-hour precipitation event at Ritterbush Pond. Each of the four estimates (1-hour, 6-hour, 24-hour and 48-hour) of the 100-year precipitation event (Table 5.1) for Ritterbush Pond plot within the envelope suggesting slope failure (Figure 5.6).

It is interesting to note, that the PMP event, had it occurred even once during the last 10,000 years (thus making it the 24-hour, 10,000-year event) would be inconsistent with the extreme value distribution (Figure 5.7), which estimates the 10,000 year storm would drop only 8.7 inches of precipitation at Ritterbush Pond. This may indicate that the conditions needed to produce the PMP are independent of average weather patterns. Thus, the PMP may be used as a maximum estimate of potential storm magnitude (19 inches in six hours), and the 1927 storm a minimum magnitude (7 inches in 2 days), needed to trigger the deposition of inorganic sediment layers in Ritterbush Pond.

# 5.3.3 The Ritterbush Chronology and Holocene Storm Patterns

The distinct characteristics of the even and odd intervals of the Ritterbush chronology suggest fluctuation between two sets of conditions, or regimes, that control storm frequency in the watershed. The odd intervals record storms of magnitude similar to the largest in Vermont's history; the events are usually separated by more than 200 years. This quiet regime includes interval III, during the warm Holocene hypsithermal, and interval I, containing the historic storm record. The even intervals constitute the noisy regime and record more frequent storms, often separated by as little as 50 years. Although it is more difficult to determine relative storm magnitude for the noisy regime, each event probably represents a storm equal to or larger than the 1927 storm, and smaller than the PMP event.

In Vermont, storm generation is controlled by the patterns of weather systems that have been highly variable during historic times (NOAA, 1982). The Ritterbush record may represent large storms that impact extensive areas (Vermont or New England) or an increase in localized thunderstorms. If the increase in storm activity during the noisy (even) intervals is due to larger scale changes in weather patterns then, 1) similar stormgenerated erosion events might have occurred in other parts of New England, and 2) the

fluctuation in regime may represent shifting atmospheric or oceanic circulation that perturbs storm patterns over a wide area. Abrupt shifts in ocean circulation patterns are thought to have caused significant changes in climate, such as the Younger Dryas cooling event, at the close of the last glaciation (Broecker, 1997).

# 5.4 Comparison with Regional and Global Events

If the Ritterbush chronology reflects storm frequency and magnitude during the Holocene, two types of data can be used to assess the record in terms of changes in regional and global climate. First, individual layers in the chronology can be compared with other dated events linked to storms and/or climate change. Second, the fluctuation from noisy to quiet regime may be reflected by longer-term shifts in regional or global Holocene climate records. Acknowledging that the uncertainty of these comparisons increases with distance from the Ritterbush basin, I will evaluate the potential that the Ritterbush chronology reflects regional and global climatic events.

# 5.4.1 Regional Storm Events Communication of the Storm Events Communicatio

A possible geomorphic record of storm events exists for alluvial fan sedimentation in the Huntington Valley, Vermont, 60 km southwest of Ritterbush Pond. The basal ages of the fans represent initiation of aggradation at approximately 8530, 7835, 2500, and 1900 <sup>14</sup>C yr BP (Bierman et al., 1997; Zehfuss, 1996; Church, 1997). The oldest ages occur within Ritterbush interval IV(10 cm and 2 cm layers, respectively), and the 2500 <sup>14</sup>C yr date corresponds with the base of interval II (9 cm layer). Given the uncertainty of both the fan and inorganic layer ages, the 1900 <sup>14</sup>C yr date falls at the end of interval II (1 cm layer). These four alluvial fans record decreased rates of aggradation during intervals III and IV, and a strong increase in aggradation associated with historic settlement. The coincidence of

alluvial fan initiation and two of the thickest layers in Ritterbush Pond suggests that the fans may be responding to the same large storm events.

# 5.4.2 Global Climatic Events

Episodic, inorganic sediment deposition has recently received increased attention as a climate proxy. Changes in the frequency, grain size, and thickness of inorganic deposits in lake sediments have been used in Chile (Lamy et al., 1998), Ecuador (Rodbell, 1997), Switzerland (Moscariello et al., 1998), and Scotland (Cooper and Sullivan, 1998), to interpret changes in local sedimentation dynamics and for comparison with global climate records. Layers of inorganic sediment have been used to determine the frequency of monsoons in the South China Sea (Huang et al., 1997) and storms in Canada (Campbell, 1998) and New Zealand (Eden and Page, 1998). These records of storm frequency, with average recurrence intervals ranging from 6 to 1500 years, have all been explained by regional and global climate patterns, such as ENSO events, and changes in atmospheric and oceanic circulation.

A Holocene lake sediment core from coastal Alabama was interpreted to record Class 4 and 5 hurricane recurrence at 600 year intervals over the last 3200 <sup>14</sup>C yr (Liu and Fearn, 1993). The base of the 9-m sediment record was not dated, but the hurricane deposits were restricted to the upper 3.2 m of the core. Liu and Fearn (1993) suggest that tropical storm patterns different from today may have dominated during the mid-Holocene. In the Ritterbush Pond chronology, the mid-Holocene (interval III) also exhibits a lack of storm layers. A 7,000 cal yr flood frequency record from the upper Mississippi River also suggests a decrease in flood frequency and size during the mid-Holocene (Knox, 1993). The earlier portion of the record suggests that large floods may also have occurred prior to 6500 cal yr BP, correlative to interval IV of the Ritterbush Pond record.

Ice rafted debris (IRD) events, identified by Bond et al. (1997), are attributed to ocean surface cooling events in the North Atlantic and occur at 1400, 2800, 4200, 5900, 8100 and 9400 cal yr BP. Ritterbush Pond records individual layer deposition within  $\pm 70$  years for all but the earliest two events. The intervals of increased storm frequency, however, appear to fall between IRD events. The 8100 cal yr IRD event is hypothesized to correspond to a widespread drying event at 8200 cal yr identified in the GISP2 Greenland ice core (Alley et al., 1997). The layer deposited in Ritterbush Pond at 8170 cal yr BP is a couplet of 0.3 mm silt laminations, and is not a large event in the basin. The 8200 cal yr BP event is the most discrete Holocene event in the GISP2 core. Other smaller scale variations in the ice core record do not correspond to individual layers, or to the noisy intervals (Alley et al., 1997).

Other well documented Holocene climatic events, such as the Younger Dryas (approximately 12,000 cal yr BP), the Mediaeval Warm Period (810 to 750 cal yr BP) and the Little Ice Age (350 to 250 cal yr BP), fit models of climate fluctuation based on century-scale periodicity, although the origin of the apparent global cyclicity has not been identified (Campbell et al., 1998; Bond et al., 1997). The Younger Dryas may be represented at Ritterbush Pond by layer v, not included in the event chronology, but identified in Core RT-2 and Core 4. One layer was deposited during the Mediaeval Warm Period and one during the Little Ice Age, suggesting that storm frequency in Ritterbush probably has little correlation to these global climate events.

Regional and global-scale generalizations of climate change emphasize average conditions, such as temperature, rather than individual meteorologic events, such as storms and floods. The regional variation in hydrologic response to climate change makes it difficult to compare a single storm frequency record, where the relative magnitude of events is difficult to determine, to global trends. The compilation of a regional storm frequency record for the Holocene, that may be more easily compared to global records of climate

change, requires the development of additional storm-generated erosion records for the northeastern United States.

- I conclude the following regarding terrestrial sediment deposition in Ritterbust
  - 1. Inorganic layers (0.1 to 10 cm) of fine sand and silt represent rapid deposition of terrestrial material in Ritterbush Pond. The thickest of these layers cluster in three time intervals: prior to 8560 callyr BP, from 6840 to 6340 callyr BP, and from 2620 to 2023
  - 2. Layer deposition is probably due to density currents reworking lake marginal sediments and transporting sediment delivered by streams toward the center of the lake. Correlation and apparent continuity of the layers between four cores suggests that
  - 3. The event chronology estimates the ages of 52 depositional events in Rinerbush. Pond since 9440 callyr BP. The thickest layers occur at 9440 (8450), 6830 (5980) and 2620 (2540) calendar (14C) yr BP and probably represent the largest crosional events in the basin during the Holocene.
  - 4. Gyttja and organic carbon accumulation rates follow general regional climate trends.

    Accumulation rates increase as the climate warms until the mid-Holocene

    (hypsithermal), probably reflecting increasing primary productivity within the lake. As the climate becomes cooler and wetter toward the present, accumulation rates remain steady.
  - 5. The most likely mechanism for inorganic layer deposition is large hydrologic events. The thickness of the inorganic layers is controlled by event magnitude and addiment availability. The apparent temporal spacing of the inorganic layers is

# CHAPTER 6 - Conclusions

# 6.1 Summary of Findings

I conclude the following regarding terrestrial sediment deposition in Ritterbush Pond during the Holocene.

- 1. Inorganic layers (0.1 to 10 cm) of fine sand and silt represent rapid deposition of terrestrial material in Ritterbush Pond. The thickest of these layers cluster in three time intervals: prior to 8560 cal yr BP, from 6840 to 6340 cal yr BP, and from 2620 to 2025 cal yr BP.
- 2. Layer deposition is probably due to density currents reworking lake marginal sediments and transporting sediment delivered by streams toward the center of the lake. Correlation and apparent continuity of the layers between four cores suggests that transport events are large enough to deposit material throughout the basin.
- 3. The event chronology estimates the ages of 52 depositional events in Ritterbush Pond since 9440 cal yr BP. The thickest layers occur at 9440 (8450), 6830 (5980) and 2620 (2540) calendar (<sup>14</sup>C) yr BP and probably represent the largest erosional events in the basin during the Holocene.
- 4. Gyttja and organic carbon accumulation rates follow general regional climate trends. Accumulation rates increase as the climate warms until the mid-Holocene (hypsithermal), probably reflecting increasing primary productivity within the lake. As the climate becomes cooler and wetter toward the present, accumulation rates remain steady.
- 5. The most likely mechanism for inorganic layer deposition is large hydrologic events. The thickness of the inorganic layers is controlled by event magnitude and sediment availability. The apparent temporal spacing of the inorganic layers is

- influenced by event frequency and may also vary with the amount of gyttja erosion and redeposition associated with layer emplacement.
- 6. The storm size necessary to initiate layer deposition in Ritterbush Pond may be estimated using historical data. The minimum size event needed to trigger layer deposition is probably similar in size to the largest storm in Vermont's 100-yr precipitation record (1927). Seven inches of rain fell over a two-day period, and may be represented as the only <1 cm-layer in the last 350 years of the Ritterbush Pond record. The maximum probable rainfall (PMP) estimated for New England by the U.S. Weather Bureau is 19 inches of rain in 6 hours, which should destabilize the hillslopes at Ritterbush and result in significant terrestrial sediment deposition in the lake.
- 7. The Ritterbush watershed appears to have experienced two different hydrologic regimes during the Holocene. The predominant, quiet regime results in the deposition of inorganic layers ≤1 cm thick, such as the one apparently deposited by the 1927 storm. The noisy regime interrupts the quiet one with clusters of inorganic layers >1 cm thick, probably representing more frequent, larger storms prior to 8650 cal yr BP, from 6840 to 6430 cal yr BP, and from 2620 to 2024 cal yr BP.
- 8. Events extreme enough to deposit 10 cm of sand in Ritterbush Pond could be due to large, regional storm systems that initiate similar erosion in other watersheds, or intense localized thunderstorms that only affect the Ritterbush area. An alluvial fan in north-central Vermont records deposition correlative to the noisy regime (intervals II, VI) at Ritterbush Pond (Bierman et al., 1997), suggesting a regional increase in storms.
- 9. The change at Ritterbush Pond from a noisy to a quiet hydrologic regime, as represented by the clusters of inorganic layers, may indicate larger-scale fluctuations in oceanic and atmospheric circulation that shift regional storm patterns. A lack of similar high-resolution regional and global climate proxy records makes it difficult to assess the validity of this hypothesis.

# 6.2 Suggestions for Future Research

The data collected for this thesis were evaluated for use in answering specific questions regarding sediment deposition in Ritterbush Pond. The quality and applicability of the resulting data varied among analytical techniques. Basic analysis of some data sets provided sufficient information, but suggested that detailed investigation, beyond the scope of this thesis, would add more insight into sedimentation dynamics. I suggest the following methods or investigations for future research on Ritterbush Pond or lakes with similar inorganic layers:

- 1. Collecting surface cores that preserve the sediment / water interface and the upper, liquid half-meter of the sediment would increase the chance of preserving a detailed historic record. The upper meter of the core could also be used to investigate sedimentation dynamics. For example, recent sedimentation rates could be measured using <sup>210</sup>Pb and/or high-resolution (gamma-ray) density measurements.
- 2. Detailed measurement of the stable carbon and nitrogen isotope values, in the upper portion of the cores, may facilitate understanding the effects of the mixing of different types (aquatic and terrestrial) of organic matter, and subsequent decomposition and diagenesis, on the values measured for the gyttja and inorganic layers deeper in the core.
- 3. High-resolution paleomagnetic analysis may provide declination and inclination signals comparable to regional records for the Holocene. This would require removing oriented samples from the core at 1-cm intervals and performing extensive analyses, but has the potential to provide continuous age correlation for the cores. Paleomagnetic signals can also record the orientation of magnetic minerals, suggesting paleocurrent directions for inorganic layer deposition, and the amount and type of magnetic minerals present, providing a diagnostic test for source sediments with distinct magnetic signals.

- 4. Of the analytical techniques used, I would select the following to investigate cores with lithology similar to Ritterbush Pond cores.
  - a) For detecting layers prior to opening the core, I would use magnetic susceptibility for low-resolution field identification and/or X-radiographs for high-resolution lab identification.
  - b) To characterize lithology and sedimentology of the layers and the gyttja, I recommend graphically logging and sampling the core.
  - c) For quantification of changes in lithology and organic matter source, I would perform elemental analysis (TOC and C/N). LOI provides comparable information only on organic carbon content.
- 5. Additional techniques that may detect changes of interest, but were not tested in this thesis include a) gamma-ray density analysis to provide a high-resolution density record for use in calculating accumulation rates, and b) detailed grain size analysis of the inorganic fraction of the gyttja to detect periods of high-flow (larger grains) not recorded by inorganic layer deposition.
- 6. Modeling of the spatial distribution of the layers within the lake (requiring additional cores) would allow for quantification of the amount of sediment deposited in the lake by a single event. Using hydrologic parameters, a) the streamflow needed to transport the sediment and b) the rainfall needed to produce the streamflow, could be calculated to estimate the size of event needed to deposit each layer.
- 7. In order to determine the extent of the hydrologic events initiating deposition in Ritterbush Pond, similar event records for the northeastern US need to be developed. The regional correspondence of the intervals of event deposition would suggest large-scale storm systems, or a regional increase in localized storms. With additional records, an investigation of the relationship between regional storm frequency and global climate would be more feasible.

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# APPENDIX A: Field Procedures

#### \*SURVEYING\*

#### **Materials**

Pentax electronic total station tripod triple prism prism rod flags (for marking hole locations)

#### **Procedure**

1. Set up tripod and total station so that total station is centered and level over the benchmark. The benchmark is a steel post on the south shore of the lake 2 m to the east of a wooden dock and boat launch. This is the first access to the pond from the main trail.

2. Zero set North as far corner of cabin across the pond, set bench coordinates at (1000,

1000). This is a project North, not true North.

3. Survey desired locations, recording northing, easting, and hole or core number.

### \*BATHYMETRY and SEDIMENT PROBING\*

### **Materials**

hand auger (with extra blades, alan key and blade sharpener) 30 meter measuring tape with weight magnesium/zirconium rods probe point propane torch

#### **Procedure**

### Bathymetry

1. Auger hole in ice

2. Lower measuring tape slowly. When it stops, note depth to top of ice

3. Survey location of hole (or mark for later surveying).

#### Sediment Thickness

1. Attach probe point to the female end of a rod.

2. Lower lengths of rod, screwing each on securely. (Many need to use the propane torch to remove ice from threads; propane must be kept warm to work)

3. Keep track of how many rods are lowered (and their length)

4. Keep the rods as close to vertical as possible!

- 5. Once in the sediment, push rods using full body weight. Do not push too quickly or too hard; the rods will bow out in the water since they are not cased.
- 6. When there is no longer any net motion downward, measure down from the end of the last rod to the top of the ice and subtract from the rod length lowered to determine total rod length.

7. Record water depth and total rod length.

8. Pull rods back out, again counting each rod to check measurement.

9. Separate the rods as they come out. If the joints are iced over, use the propane torch.

10. Survey in location of hole (or mark for later surveying).

#### Materials

Reasoner Corer

1. Core barrel - attachment holes drilled, core catcher/piston installed

2. Core head - pull rope, bolts and wingnuts

3. Core driver (pig) - filled with sand or rocks, pull rope

Piston - wire cable, frummer clamps, vise grips, wrenches, wire cutters and deadman (with webbing and keeper string) (rod to set the piston if needed)

Pulley system - 6 carabeaners, 6 pulleys and 2 jumars and deadman (with webbing and keeper string)

Permanent marker, paper and cloth towels, end caps, duct tape, ice auger, gloves

# Preparation

Core barrel

1. Obtain desired length of PVC pipe with 3.5" (9 cm) outer diameter. The pistons are designed for an 8 cm inner diameter pipe. A ten foot length of 3" PVC potable with bell and flange ends has been used successfully. Schedule 40 PVC is thicker walled, with an ID of 7.5 cm, which makes setting the piston extremely difficult and is not recommended.

2. Fit core barrel into core head and drill 1/4" holes to attach with bolts in field; mark core

barrel where it meets the core head and opposite the black arrow.

3. Mark core barrel in 0.5 m intervals from the bottom up; draw a continuous line down the length of the barrel to allow for realignment once it has been cut. Add arrowheads pointing up (top up) to the continuous line.

## Core catcher installation

1. Trace the pattern onto sheet aluminum and cut out; do not use the pattern!

2. Bend the teeth slightly inward to check that they will close properly

3. Insert the catcher, teeth first, into the bottom of the barrel and fold back to the outside of the barrel (cutting with snips where necessary) to secure.

4. Drill 1/4" holes through both layers of sheeting and core barrel5. Place rivets in holes and pop rivet the core catcher in place

6. Wrap exposed sheeting thoroughly in duct tape

Setting the piston

1. Make sure piston cable is securely fastened to piston (with a frummer) and that all components of the piston are properly attached and tightened.

2. Grease the rubber stoppers lightly with silicon grease.

3. Loosen the nuts on either side of both of the stoppers (need two wrenches)

4. Tighten the lower stopper first, until it fits snugly (almost too tight)

5. Thread the piston cable through the barrel and repeat step 4 for the upper stopper

6. Set the piston such that the lower stopper is flush with the end of the core barrel.

note: if the core catcher is already installed, the piston will need to be pushed down from the top of the barrel.

## Coring Procedure

#### Preparation

1. Auger an oversized hole (three auger holes) for core. Measure and record water depth.

2. Auger two holes for deadmen: one close to core hole for piston, one 40 ft away for pulley. Deadmen should be set in these holes and tied off to sleds, toolboxes, etc.

3. Check that piston is set tightly and core catcher installed (if desired).

4. Attach the core head with bolts and wignuts.

5. From the bottom of the barrel, measure up the water depth and mark (with tape or marker) both the piston cable and core head rope (1st mark)

6. A second mark should be made on the core head rope to determine when to stop driving the core. This mark should be at most the water depth plus the length of the core barrel, minus 20cm for the length of the piston and the overlap of the head and barrel.

7. Using a hand pump or waterbottles, fill barrel at least half full with water to weigh

down the piston and keep it from being buoyed up.

8. Tape piston and rope together to check for slippage while setting the core barrel.

9. Survey in location of hole (or mark for later surveying).

### Setting and driving the core

- 1. Lower core barrel down hole several meters, but not so the lower end touches the lake bottom.
- 2. Feed piston cable and head rope through center of the driver. Put driver in hole and hold it just below ice.

3. Keep all lines separate!

4. Lower to the FIRST mark (sediment water interface). Check for slippage. If there was no slippage remove tape and proceed. If there was slippage, pull up core and start over.

5. Clamp off piston cable with vice grips to deadman.

6. Carefully lower driver and set core into the sediment with several gentle drops.

7. Drive core in short frequent drops until 2nd mark is reached, the core ceases to move, or a double bounce is consistently felt.

# Retrieving the core

1. Pull out driver and remove from piston cable and head rope.

2. Set up pulley system on head rope (see diagram), starting with 4 pulleys.

3. Loosen piston cable.

4. Pull on head rope. If there is a lot of resistance, add pulleys for mechanical advantage OR put tension on the rope wait 10-15 minutes until trying to pull.

5. When the first mark is reached, pull up quickly through water column.

6. Catch under core with hand and endcap. If there is a core catcher and the endcap will not fit, quickly wipe the end clean and wrap with duct tape.

7. Cut piston cable OR saw top of barrel containing piston and cap top.

8. Cut core into <1.5 m lengths using PVC saw. Have endcaps and towels ready.

9. Cap and tape each section, and label with core name and section number.

9. If cores are at risk for freezing, wrap with webbing to hang from deadman in water until ready to transport out.

#### Comments

This corer is designed for deep water; can be modified for shallow water by decreasing the length of the head, driver and barrel. A tripod would be very helpful with core retrieval. A reusable, metal core catcher, would be easier, and probably more efficient, than the corecatchers cut from aluminum sheeting. The 3 3/4" endcaps do not fit over the end with the core catcher, larger diameter endcaps would be useful if a corecatcher is used. The piston works well (if it is set tightly) even without a core catcher, although the lowest 10 cm of material may be lost.

# APPENDIX B: Lab Procedures

# \*CORE PROCESSING\* \*Splitting\*

#### Materials

spliting rack (2 x 4's on plywood with saw guide and shims) circular saw, blade set to 1/4" safety glasses, ear protection long (splitting) knife, exacto knife and duct tape meter stick or tape measure, permanent marker plastic wrap, roll plastic and heat sealer paper towels, DI water

#### Procedure

- 1. Mark the core for splitting by wrapping a 8.5" by 11" piece of paper (creased in half) around one end of the core and marking where the ends meet and at the crease. These two marks should be on a diameter of the core.
- 2. Make sure both halves of the core will be labeled after splitting
- Place core in splitter with one of the cutting marks facing up. Shim in place.
   Set the circular saw against the guard and be sure the mark lines up in the sight
- 5. Cut down one side of the core. Stop and readjust blade if it does not go all the way through the PVC or if it goes too deep.
- 6. Run a piece of duct tape over the cut to hold it together while cutting the other side
- 7. Remove the shims, flip the core over and line up the second mark. Cut down the side.
- 8. Take core out of splitter being careful to hold it together.9. Cut through endcaps and duct tape with the exacto kinfe.
- 10. Rotate the core so that the duct tape is on the bottom and the open cut on the top. Split the core by gently sliding the knife into the sediment.
- 11. Rotate the core so that the knife is horizontal and lift the knife (and half of the core) up and off of the lower half of the core.
- 12. Slice the duct tape holding the two halves together and clean an edge of the PVC.
- 13. Using the ruler, mark both halves of the core at 10 cm intervals.
- 14. Wrap one half of the core in 2 layers of plastic wrap.
- 15. Seal in a plastic bag, being sure the core name, section, up direction, depth and length are noted on the outside.
- 16. Refrigerate at 4°C.

# \*CORE PROCESSING\* \*Logging\*

#### Materials

spatulas (scraping and sampling), paper towels, DI water metersticks (at least 2) labels for core name, section and meter depth core rack (gray 2 x 4's on white pressboard) photo stand with daylight bulbs, Kodak color chart camera and 35mm film video camera and Hi8 film graph paper, colored pencils, small ruler grain size card, hand lens

## Procedure

Cleaning

- 1. Scrape the surface of the core clean with a spatula, being careful to scrape across the core and clean the spatula well with DI water to minimize contamination.
- 2. Remove any obvious pieces of shredded PVC.
- 3. Place the core in the core rack on the photo stand.

Photo and Video Log

- 1. Place camera on photo stand. Mark where the frame of the camera falls on the stand.
- 2. Starting from the top, line up a section of the core (about 25-30 cm) within the frame.
- 3. Place a ruler directly next to the core at the appropriate cm depth, and label the meter depth (1-6).
- 4. Make sure the ruler, color chart and label fit into the picture.

5. Turn on the daylight bulbs.

6. Adjust camera against a grayscale card.

7. Take a picture and slide the core 20-25 cm. Adjust the ruler and make sure there is overlap between pictures. Repeat for entire length.

8. Turn off the daylight bulbs, remove camera.

9. For video log, place the video camera on the stand and repeat the above steps, leaving the camera on while the core is moved.

Graphic Log

- 1. Set up graph paper with a stratigraphic column (1 inch = 10 cm), grain size column and leave plenty of room for notes. Note core name, section and date.
- 2. Make a general description of the dominant sediment facies (gyttja), including grain size, color, sediment type, and texture (density).

3. Working up or down the core, cm by cm, describe

a) general changes in, or characteristics of, gyttja.

b) distinct layers (gyttja or minerogenic), color, thickness and grain size. c) the boundary between changes in sediment type (sharp, gradational).

d) the presence of macrofossils or other particles.

# CORE PROCESSING\* \*Sampling\*

#### Materials

plastic or glass 20 ml bottles and caps permanent markers and/or labels sampling spatula, semi-circular knives kimwipes, napkins DI water meter sticks

#### **Procedure**

1. Prior to sampling, label bottles with core name and depth interval

- 2. Starting from the top and working down, insert semi-circular knives at 1 cm intervals.
- 3. Scoop out the sediment between each pair of knives into the prepared bottle and cap.
- 4. Wash knives and spatula in DI water between samples to avoid contamination.
- 5. Remove large macrofossils and place in separate, labeled bottle or wrap in aluminum foil and seal in a plastic bag.

6. At thick inorganic horizons, adjust the sampling interval to reflect the location of the boundary.

7. Note any observations, such as the exact location of macrofossils, on the graphic log.

8. Refrigerate all samples at 4°C.

# \*MAGNETIC SUSCEPTIBILITY\* \*Sapphire\*

#### Materials

Magnetic coil and power box IBM compatible computer, software disk core rack (2 X 4's with dowels, shims, bolts and nuts) permanent marker, measuring tape

### Procedure

1. Allow core to come to room temperature for best results. This apparatus works best for whole cores. If half cores are used they should be unwrapped.

2. Mark core at 3 cm intervals from top down - (3 cm is the width of the coil). If the core is longer than 150 cm, it must be logged in 2 separate runs.

3. Assemble rack, place coil in the center of the rack, shim to hold in place.

4. Load software. Set CMS logging mode to fast, input core segment name and info.

5. Position core on rack, with top of core closest to coil, but about 50 cm away.

6. Begin measurements with a FREE AIR measurement with the core out of the coil, by pressing the coil button.

7. The computer will beep when it has completed each measurement; slide the core through at the intervals marked and depress the button each time.

8. When the segment is complete, or 50 measurements have been taken, remove the core and take a second FREE AIR measurement. Then press 9 to end the segment.

9. Repeat as necessary

10. Run each segment at least twice to calculate statistical error.

11. Download data (text file) to spreadsheet or graphing program.

# \*MAGNETIC SUSCEPTIBILITY\* \*Bartington\*

## Materials

Automatic core logging system with coil and meter IBM compatible computer and software

#### Procedure

1. Allow core to come to room temperature for best results.

2. Turn on computer and meter, let warm up for 1 hour.

3. Keep metal or other magnetic things away from the coil during the run.

4. Input core length, resolution (0.01) and interval (1 cm). Make sure to give each file a unique name.

5. Place core in boat, top closest to coil.

6. Initiate run. The computer will move the core at the specified interval and take free air measurements before and after the run that can be used to correct for drift.

7. Download data (text file) to spreadsheet or graphing program.

## \*X-RADIOGRAPHS\*

#### **Materials**

X-ray machine - UVM Radiation Saftey Lab lead labels, film

#### **Procedure**

1. Place two core sections on the x-ray table.

2. Use lead to label top of core, core name and depth at 20 cm intervals

3. Set controls to machine to measure cores. Experiment with what will give best exposure. Initially set at kV=63, Mas =20, sec=0.16.

4. Load film into tray in darkroom5. Place film under table, take x-ray.

6. Reload film in darkroom, slide film into developer

7. Reposition core (move about 30 cm) being careful to keep labels in place

note: the x-rays are "stretched" slightly with no distortion at the center and greater distortion at the edges due to a point source of x-rays.

## Image Processing

1. Cut each x-ray at the center of the image.

2. Measure the distance between lead labels (usually 2 cm greater than actual distance).

3. If there is not an adequate scale (1 cm intervals) on the x-ray, tape a plastic, transparent ruler on one side of the x-ray.

4. Scan x-ray with a transparency scanner.

5. In *Photoshop 3.0*, compress each image by the measured difference, from the edge to the center using a linear stretch.

6. Import into canvas and match each image cut image at end. Clip edges to match between x-rays and group images to create 1 image per section of the core.

7. Import each section into *NIH Image* and snap a line down the center of the image, creating and saving XY coordinates on a grayscale graph.

8. Export data to speadsheet or graphing program.

### \*LOSS-ON-IGNITION\*

#### **Materials**

drying oven, burning oven balance (record to nearest milligram) numbered crucibles (in pencil on the bottom), trays DI water, spatula, napkins, kimwipes

### **Procedure**

1. Clean and dry each crucible. Organize crucibles on tray in numeric order.

2. Record crucible weight.

- 3. Homogenize each sample. If sample is dry, grind with a mortar and pestle. If sample is wet, mix well in sample bottle.
- 4. Transfer approximately 2 g of sample to crucible (less if dry), recording sample number and crucible number. Keep samples in numeric order to minimize confusion.

5. Clean and rinse spatula to avoid contamination between samples.

6. Repeat steps 2+3 as desired (usually 50-60 per batch).

7. Weigh each crucible/sample and record.

- 8. Place crucibles in drying oven at 80°C to dry overnight.
- 9. Remove from oven, let sit 1 hour, weigh. 10. Place in burning oven @450°C for 2 hours
- 11. Remove from oven, let sit 1 hour, weigh.

# \*TOTAL CARBON AND NITROGEN\*

#### Materials

Elemental Analyzer silver capsules, spatulas and tweezers microbalance drying oven, crucibles, mortar and pestle 1N HCl, pipet

#### **Procedure**

- 1. Dry samples in crucibles at <80°C. Grind and homogenize sample with mortar and pestle.
- 2. Using microbalance, weigh 3-40 mg into a silver capsule, recording weight in computer spreadsheet. For organic samples use <10 mg; for sands use 30-40 mg.

3. Place open capsule in culture tray.

4. Add three drops of HCl with a plastic pipet to remove secondary carbonate

5. Allow to sit for 2 hours. Dry overnight at 60°C.

6. Close sample capsule with tweezers and load into carousel.

7. Begin run with a blank and two standards (peach leaves, 5 mg). Run two standards every 20 samples.

## \*NITRIC ACID DIGESTION / CHARCOAL\*

#### **Materials**

centrifuge, centrifuge tubes (in sets of 9), test tube racks hot water bath concentrated nitric acid DI water Elemental Analyzer, tin capsules, tweezers, spatula etc balance, microbalance

#### **Procedure**

1. Dry samples overnight at <80°C. Grind and homogenize the sample with mortar and pestle.

2. Weigh approximately 2 grams into centrifuge tube.

3. Add 15 ml nitric acid and stir. Let sit in hot water bath for 1 hour, stirring after 30 min.

4. Remove from bath and let cool.

5. Centrifuge at 20 on speed dial for 10 min and decant.

6. Add DI and stir, centrifuge and decant

7. Repeat twice.

8. Place test tubes in drying oven overnight (60°C)

9. Transfer ALL of sample into tin capsule. Close the capsule, record weight.

10. Place sample in carousel.

11. Begin run with a blank and two standards (peach leaves, 5 mg). Run two standards every 20 samples.

# \*STABLE CARBON ISOTOPES\*

Materials

Vacuum line, liquid nitrogen, alcohol vials and tubes dilute HCl Cu, CuO, quartz wool, spatulas

DI water, mortar and pestle

#### Procedure

1. Add several ml of dilute HCl to each sample. Allow to react for several hours. Rinse several times with DI water.

Dry overnight at 80°C. Grind and homogenize sample.
 Label glass tubes with sample number (use white-out)

4. Weigh out 600 mg CuO, mix with 10-40 mg of sample and funnel into tube.

Add 500 mg Cu and plug with quartz wool.

6. Place on vacuum line and seal.

7. Burn 1 hour at 900°C. Allow to cool.

8. Wipe glass clean of white out and relabel with permanent marker.

9. Score glass with razor blade.

10 Set up vacuum line, prepare liquid nitrogen, alcohol mixtures for traps.

11. Break tube, isolate  $CO_2$  and water in liquid nitrogen trap, pump away remaining gases. 12. Isolate water (releasing  $CO_2$ ) in alcohol trap. Transfer  $CO_2$  into sample container using a liquid nitrogen trap.

13. Analyze sample on the mass spectrometer.

## \*GRAIN SIZE ANALYSIS PREPARATION\*

## Materials

15% HCl

concentrated H<sub>2</sub>O<sub>2</sub> (30%)

1M NaOH (40 g of NaOH dissolved in 1L DI water)

Dispersant (25g of sodium metaphosphate dissolved in 500 ml DI water)

Centrifuge and test tubes, test tube racks

hot water bath

glass stir rods, 5 ml pipette

# Procedure (all chemicals should be handled under hood)

1. dry samples at 50°C and remove any large pieces of organic matter.

2. place between 0.4-0.6 g of sample in a centrifuge tube (use more if sample lacks fines).

3. To remove secondary carbonate, add 20 ml of HCl, stir and rinse rod into tube with as little DI as possible.

4. Place sample in a hot water bath (50°C) for 2 hours

5. Stir well, centrifuge, decant. If necessary, repeat steps 3-5.

6. Fill tubes 3/4 with DI water, mix well, centrifuge and decant. Repeat twice.

7. To remove organic matter, add 5 ml H<sub>2</sub>O<sub>2</sub>, stir and rinse rod.

8. After intial reaction wanes, place sample in a hot water bath (50°C) for at least 2 hours. Let sample react overnight (but do not leave hot plate on).

9. Centrifuge decant and rinse as detailed above (steps 5+6).

10. To remove biogenic silica, add 10ml NaOH, stir and rinse rod. 11. Let samples sit in hot water bath at least 4 hours.

12. Centifuge, decant and rinse as detailed above (steps 5+6).

13. Add 5 ml of dispersant to samples; stir vigorously until all clods are broken up.

14. If possible, place on reciprocating shaker for 2 hours prior to analysis.

## \*BULK DENSITY\*

#### Materials

semicircular knives, spatula, sharp knife DI water, ruler 1.2 ml measuring spoon crucibles, balance

### Procedure

- 1. Insert two semicircular knives into core about 1.5 cm apart. Remove one knife.
- 2. Make two cuts with regular knife about 3 cm apart perpendicular to the first cuts.
- 3. Lift the resulting rectangular block of sediment out of the core by lightly pressing a spatula to the open side and lifting the spatula and the remaining semicircular knife.
- 4. Dissect the block using an exacto knife. Carve out two 1cm<sup>2</sup> cubes.
- 5. If sediment is to wet to keep its shape, scoop it out directly from the core using a measuring spoon, being sure to level the spoon and clean it well.
- 6. Place the samples in crucibles, weigh.
- 7. Dry overnight at 60°C.
- 8. Allow to sit 1 hour, weigh samples.

## **APPENDIX C: FIELD DATA**

FIELD DATA and NOTES for RITTERBUSH POND - Eden VT All data is in meters, as recorded by total station, tapes and rods.

## Field Crews

1/12 - 1/13/1997: Sarah Brown, Paul Bierman, Dave Shaw

1/19/97: Sarah, Paul, Dave and Tom Davis

1/26/97: Sarah, Paul, Dave, Mike Abbot, Christine Massey, Andrea Lini

3/4/97: Sarah, Paul, Char Mehrtens and Stephen Wright

3/7/98: Sarah, Paul, Christine, Barry and Sandy Doolan, Kris Bryan, Stephen and Rebecca Wright

## Benchmark

Total station tripod centered over a steel fence post 2m right of dock, 1-2m on shore. Set to coordinate (1000,1000) North set at left corner of cabin across pond to the northwest. Approximate coordinates (1240, 1000)

Bathymetry and Sediment Probe Data

DATE	LOCATION	NORTHING	EASTING	WATER DEPTH	ROD LENGTH	SEDIMENT THICKNESS	NOTES
1/12/97	Transect 1						line @ 27.59.50 across pond to snag.
	-101.113						15m intervals
	1	1013.65	1007.25	1.7	5.5	3.8	ea.
	2	1026.77	1014.45	6.4	9.7	3.3	top of hard layer?
	3	1040.25	1021.67	10.2	14.2	4	
	4	1053.38	1029.00	12.8	17.1	4.3	
1 1 1 1 1	5	1066.37	1036.00	13.5	18	4.5	
	6	1079.41	1042.92	13.5	18.6	5.1	
	7	1092.28	1049.86	13.5	17.7	4.2	
	8	1105.11	1056.76	12.7	16.4	3.7	100
	9	1118.31	1064.06		14.5	3.2	
	10	1131.31	1070.96	10.1	13.2	3.1	hard to push
	11	1144.48	1078.14	9	12.4	3.4	hard to push
	12	1158.01	1084.88	8.5	11.8	3.3	nara to past.
	13	1171.32	1092.30	8	11.2	3.2	
	14	1184.81	1099.46		10.4	3.1	hard layer @9.5
	15	1197.84	1106.31	5.3	8.3	3	hard layer @7.7
	16	1211.15	1113.42		6.1	3.6	4.75, pushed hard
	17	1224.54	1120.27			0	not taken - thin ice
	18	1238.04	1127.05			o	not taken
1/13/97	Transect 2				1		long axis from mid-delta to outlet.
							22.5m intervals
	1	1177.99	902.76			0	not taken
	2	1164.35	920.21	4.2	8.4	4.2	hard out
	3	1149.84		7.4	11.6	4.2	halfway from above
	4	1135.54		10.4	14.2	3.8	6m water
	5	1121.32		12.1	16	3.9	
	6	1107.56		12.6	16.7	4.1	
	7	1093.10			17.5	4.1	
	8	1079.36	1026.43	13.4	17.8	4.4	
	9	1064.26	1044.06	13.5	17.8	4.3	
	10	1050.60	1063.40	13.6	19.3	5.7	_ 2 × 2
	11	1036.30	1081.89	12.9	17.2	4.3	The second secon
	12	1022.76	1100.27	7.7	10.9	3.2	gravel bottom?
	13	1009.30	1119.22	2.2	5.6	3.4	gravel bottom?
	14	995.25	1137.33	1		0	not taken
	15	981.52	1155.87	'		0	not taken
	Perimeter						clockwise from benchmark estimation of shoreline
320, 50	1 .	1010 74	982.06				Community of Charles
	1	1019.74		1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	2	1025.79		1	1 - 29 /		3m from shore @ delta
9	3	1058.37	1	1	C. 10	Death B	Jill Holli Silote & delta
The state of	4	1083.40	1			20	The property of the contract o
	5	1108.26		1			With the Art and the Art 149,000
	6	1127.32		1		- 1	A 2 to 10 and the control of
	7	1163.20	1	1			
	8	1203.60					
	9	1226.32	958.51				

	T						
DATE	LOCATION	NORTHING	EASTING	WATER DEPTH	ROD LENGTH	SEDIMENT THICKNESS	NOTES
1/13/97	Perimeter						
	10	1220.68	997.10				
	11	1215.81	1053.39				
	12	1231.30	1098.80				
	13	1238.28	1126.92				
	14	1219.27	1139.04				
1 1	15	1151.88	1141.93				
	16	1104.76	1145.64				
	17	1070.42	1145.95				
	18	1010.09	1155.70				
	19	1000.13	1145.24				outlet
	20	971.07	1115.59			1	outlet
	21	970.33	1092.44				outlet
	22	958.85	1075.08				rods (snag)
	23	949.16	1056.71				lods (snag)
	24	967.86	1033.06			1	2m from shore
	25	988.90	1014.53				Ziii iioiii siiole
1	Additional						
	Points						
1	NW shore	1195.34	1004.52	7.8	10.8	3	easy out
	NW mid	1134.28	1022.11	12.9	16.6	3.7	leasy out
1	SE mid	999.18	1072.08	9.4	13.7	4.3	
1					1011		
1/19/97	Α	1030.34	1059.42	13.6	17.5	3.9	easy out
1	В	1067.33	1058.27	13.4	18.5	5.1	525, 521
	С	1063.61	1088.93	12.9	17.65	4.75	
	D	1105.02	1090.28	9	12.1	3.1	hard refusal
1	E	1134.34	1105.16	4.1	7.8	3.7	refusal
1	F	1172.68	1055.42	9.9	12.6	2.7	layer @ 11.4
1	G	1193.09	1075.60		10.25	2.55	layer @ 10 (10cm)
1	н	1192.86	981.35	8.1	11	2.9	layer @ 10.45
	1	1185.50	959.00	8.7	12.45	3.75	,
	J	1130.01	928.68	5.2	9.7	4.5	
	K	1074.08	961.71	6.5	11.05	4.55	
	L	1052.38	1047.79	13.4	18	4.6	
	М	1069.04	1046.49	13.5	18.65	5.15	
	1					1	
1/26/97	1	1073.71	1004.77	12.4	17.05	4.65	
	2	1174.60	959.61	9.55	13.95	4.4	
	3	1076.51	1115.77		10.4	3.85	refusal (rock)
	check zero	1239.84	1000.10	1			corner of cabin
3/4/97	Core RT-2	1059.84	1061.88	3			approx from pic.
	check zero	1239.78	1000.05	5			corner of cabin
3/7/98	check zero	1	1000.04	1			corner of cabin

Cores - Re	asoner Cor	ing Device			
DATE	CORE	NORTHING	EASTING	WATER DEPTH	NOTES
1/19/97	practice			8.7	10 ft practice core taken approx 40m along transect 1 from dock.
					Piston and corecatcher - easy to drive, difficult to retrieve
1/26/97	1	1056.25	1063.77	13.5	6m barrel with piston and corecatcher. Retrieval with 5 pulleys
					easy pull out, upper section sloshes water in barrel
	2	1057.34	1063.62	13.5	6m barrel with piston and corecatcher. Retrieval with 5 pulleys
					heavy - solid core!
3/4/97	3	1177.06	1096.73	7.8	6m barrel with piston and corecatcher. Retrieval with 6 pulleys
					bottom in gyttja, could have driven further
	4	1130.34	966.93	12	6m barrel with piston and corecatcher. Retrieval with 6 pulleys
		1			driven to refusal, gray sediment at bottom
3/7/98	5	1060.64	1061.58	13.5	6m barrel (sched 40) with piston (set tight!) no corecatcher.
					Pushed through first meter of sediment THEN set piston.
					Retrieval with 4 pulleys. Gray liquified sand at bottom.

## APPENDIX D: Lab Data

Data Set	Page
Magnetic Susceptibility	138
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Elemental Analysis (TOC, C/N)	148
Bulk Density	149
Stable Carbon Isotopes	149
Charcoal (Nitric Digestion)	149
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Grain Size	151

epth (cm)	Susceptibility	Data - COF Depth (cm)	E 2	Sapphire St	sceptibility	Data - COR		Sapphire Si	usceptibility	Data - COR	E 4
3	6.4E-06	303	1.7E-05	Depth (cm)	Suscept(SI) 2.6E-06		Suscept(SI)	Depth (cm)	Suscept(SI)	Depth (cm)	Suscept(SI)
6	9.6E-06	306	1.9E-05	6	5.4E-06	303	9.6E-06	3	3.1E-06	303	1.0E-05
9	1.1E-05	309	1.8E-05	9	7.0E-06	306	1.5E-05 2.3E-05	6 9	5.5E-06	306	1.6E-05
12	1.2E-05	312	1.5E-05	12	8.5E-06	312	3.8E-05	12	6.4E-06 6.7E-06	309 312	3.4E-05 2.7E-05
15	1.2E-05	315	1.3E-05	15	9.5E-06	315	4.9E-05	15	6.7E-06	315	9.0E-06
18	1.1E-05 1.1E-05	318	1.3E-05	18	9.5E-06	318	3.1E-05	18	7.1E-06	318	4.4E-06
24	1.1E-05	321	1.3E-05	21	9.6E-06	321	1.2E-05	21	6.9E-06	321	2.2E-06
27	1.1E-05	327	1.3E-05 1.1E-05	24	9.6E-06	324	7.6E-06	24	6.6E-06	324	3.2E-06
30	1.1E-05	330	1.1E-05	30	9.3E-06	327	6.6E-06	27	6.5E-06	327	5.3E-06
33	1.2E-05	333	1.2E-05	33	9.0E-06 8.5E-06	330	6.4E-06	30	6.5E-06	330	6.9E-06
36	1.2E-05	336	1.1E-05	36	8.0E-06	336	6.6E-06 8.8E-06	33	6.6E-06	333	8.0E-06
39	1.2E-05	339	1.1E-05	39	7.5E-06	339	1.9E-05	36	6.3E-06 5.8E-06	336	9.8E-06 1.8E-05
42	1.1E-05	342	1.1E-05	42	5.5E-06	342	2.5E-05	42	5.7E-06	342	2.9E-05
45	9.4E-06	345	1.2E-05		4.5E-06	345	1.9E-05	45	5.4E-06	345	4.1E-05
48 51	9.0E-06	348	1.3E-05	48	3.9E-06	348	1.8E-05	48	5.0E-06	348	5.1E-05
54	8.9E-06 9.1E-06	351 354	1.3E-05		4.9E-06		3.9E-05	51	5.0E-06	351	5.5E-05
57	9.3E-06	357	1.3E-05 1.3E-05		6.3E-06		5.2E-05	54	5.7E-06		5.1E-05
60	9.8E-06	360			7.5E-06 1.5E-05		2.5E-05		5.0E-06		5.0E-05
63	1.0E-05	363			2.6E-05		1.3E-05 1.9E-05				8.0E-05
66	1.1E-05	366			3.1E-05						
69	1.1E-05	369		69	3.5E-05						1.1E-04 1.1E-04
72	1.1E-05	372	1.3E-05		3.2E-05						
75	1.2E-05	375			2.7E-05	375					
78	1.3E-05	378			3.5E-05	378	3.1E-05	78			
81	1.3E-05 1.3E-05	381			4.6E-05				4.6E-06	381	7.7E-05
87	1.3E-05	384			2.8E-05						
90		390			1.9E-05						
93											
96	1.6E-05										
99	1.6E-05	399	1.2E-05	99							
102			1.3E-05	102	5.6E-05						
105						405	3.3E-0				
108							3.0E-0	108	1.2E-0	5 408	7.0E-05
111											
117											
120											
123											
126											
129	1.5E-05	429		129							
132		432									
135					1.2E-0	4 43	7.3E-0				
138								5 13			
141											
144											
150											
153											
156											
159											
162											
165					3.5E-0	5 46	5 7.9E-0	5 16	5 5.8E-0	6 46	5 0.00043
168											
171											
174											
177											
183											
186											0.00070
189											
192	3.4E-0	5 49	2 1.9E-0	5 19	1.0E-0	5 49	2 4.3E-0	05 19	2 5.8E-0	06	
195							5 5.5E-0	05 19			
198											-
20											-
204											
20											-
21											
21							7.02	21			
21								21	9 1.1E-		
22	2 2.4E-0	5 52	2 4.4E-0	05 22	2 1.4E-0	05		22	9.5E-	07	
22							-	22			
22							-	22			-
23							-	23			
23							+	23			-
23								24			
24							1		3.3E-		1
24									46 2.4E-		
24									49 2.4E-		
25				05 25	2 4.6E-	06			52 8.4E-		
25	5 1.5E-0	55 55	5 4.1E-	05 25					55 4.0E-		-
25									58 2.4E-		-
26							-		61 3.05E- 64 4.28E-		-
26							-		67 6.17E		
26			3.1E-						70 9.07E		
27			-	27					73 7.56E		
27			+	27					76 6.71E		
27				27					79 6.89E		
28				28				2	82 9.03E	-06	
28				28	1.3E-				85 1.4E		
28	8 1.6E-	05			1.5E-				88 1.46E		
	1 1.6E-	05	-		1 1.7E-				91 2.5E 94 4.59E		
29				1 29	1.3E	00			94 4.59E	-00	
29 29 29					7 1.0E-	ns		2	97 3.26E	-05	

	Sust	ept(SI)	Depth (cm)	Data - CORE 2 Suscept(SI)	Deoth (cm)	Suscept(SI)	Donth (am)	C		-	-	-
2	25	1.1	101	3.2	201		Depth (cm) 301	Suscept(SI)		Suscept(SI)		Suscept(SI)
3	31	1.5	102	3.4	202		302	4.2	401	3.8	501	15.2
4	-	1.8	103	3.6	203		303		402	3.6	502 503	16.8
5 6	20	2.0	104	3.9	204	6.7	304		404	4.0		19.8
7		2.1	105	4.0	205		305	5.8	405	4.6		18.0
8	100	2.4	106	4.1	206		306	6.3	406	5.1	506	15.2
9	18 1.	2.5	108	4.2	207		307	5.9		5.6		13.9
10	880	2.5	109	4.5	209		308		408	5.8		13.7
11		2.3	110	4.4	210					5.7	509	13.9
12	10%	2.3	111	4.2	211					5.5		13.0
13		2.0	112	3.9	212					5.4		11.0
14		1.8	113		213					5.7 6.3		
15		1.6	114	3.3	214					6.9		
16		1.5	115	3.3	215							
17		1.4	116		216	6.0						
18		1.4	117		217		317					
20		1.4	118		218			3.4				
21		1.4	119		219						519	17.
22		1.4	121		220							
23		1.5	122		221							
24		1.6	123		223							
25		1.7	124		224							
26		1.9	125		225							
27		2.3	126	2.6	226							
28		2.3	127	2.5	227							
29		2.3	128	2.4	228	9.8						
30		2.2	129		229		32	3.				
31		2.3	130		230			3.	2 43	5.0	530	33,
32		2.1	131		231							35.
34		1.9	133		232							2 37
35		1.7	135		233							
36		1.6			23							
37		1.7	13		23							
38		1.7	131		23							
39		1.7			23							
40	0	1.7	14		23							
41		1.7	14		24							
42		1.7		3.6	24	1 8.						
43		1.8			24	2 6.						
44		1.8			24	3 5.	6 34	3 3.	7 44	4 29.	7 54	
45		1.9			24				0 44	5 29.	8 54	4 59
46		2.0			24						4 54	5 57
47		2.1			24							
41		2.2			24							
51		2.1			24							
5		2.3			24							
5		2.4			25							
5		2.4			25							
5		2.4			25							
5	5	2.4			25						.6 55	
5	6	2.5			25							
5	7	2.0	15	7 3.4	25							
5		2.0			25	7 6.	8 35	7 4	.9 45	8 3	.1 55	
5		2.0			25				.9 45	9 3	.5 55	8 2
6		2.			25				.9 4,6		.1 55	
6		2.0			26				.9 46		.9 56	
6		2.1			26				.7 46		.3 56	11 11
6		2.			26				.4 46		.8	
6		2.							.2 46		.9	
6		2.							.0 46		.8	
6		2.							.9 46		1.7	
6		2.							.1 46		2.7	
6		2.	7 16		26			8 4			.8	
	0	2.							.9 47		3.0	
	1	2.							.5 47		3.2	
	2	2.	7 17	2 7.8	27	2 6	.9 3	71 6	.2 47		3.6	
	3	2.									3.9	
	4	3.									1.1	
	5	3.									1.1	
	6	3.									1.8	
	8	2.									5.1	
	9	2.									5.4	
	0	2.									5.5	
	1	2.									5.5	
	2	2.							1.7 4	82 5	5.4	
	3	3.			2	83 3	.8 3	82	4.5 4	83	4.9	
8	14	2.	9 18	5.0	2	84 3	1.5 3	83			4.5	
	15	2.	9 11	35 4.							4.4	
	6	2.		36 4.							4.5	-
	37	2.		37 5.							4.9	
	88	2		6.							5.2	
	19	2.		8.							5.6	
	0	3.		90 11.							6.2	
	1	3.		91 14.							7.5	
	2			92 17.							8.0	
	3			93 17.							8.4	
	14	3		94 15. 95 12.							8.8	
	95			96 9.							9.7	
	7			97 7.							1.2	
	8			98 5.					3.5 4	98 1	3.0	
	9			99 5.				98	3.8 4	99 1	4.3	
				00 4.				99	4.0 5	00 1	5.2	ELECTRIC PROPERTY OF THE PARTY

John (cin)		D	Data - COR	: 3						1	
2	Suscept(SI) -0.1	Depth (cm)	Suscept(SI)	Depth (cm)	Suscept(SI)	Depth (cm)	Suscept(SI)	Depth (cm)	Suscept(SI)	Depth (cm)	Suscept(SI)
3	-0.1		27.1	201	2.4	301	1.6	401	26.1	501	3.4
4	0.0	102	24.7	202	2.2	302	1.7	402	20.7	502	-1.1
5	-0.1	104	21.3 18.3	203	2.1	303	2,0	403	15.1	503	-3.5
6	0.0	105	16.2	205	2.0 1.8	304	2.4	404		504	-2.3
7	-0.1	106	15.3	206	1.6	305	3.0	405	7.1	505	2.9
8	0.0	107	15.5	207	1.6	307	4.6	406		506	6.2
9	0.0	108	16.9	208	1.7	308	5.2	408			
10	-0.1	109	18.5	209	1.8	309	5.7	409			-
12	-0.1 -0.1	110	19.8	210	2.1	310	6.4	410			
13	-0.1	111	19.8	211	2.5	311	8.0	411	5.7		
14	-0.1	112	18.9 17.8	212	2.9	312	10.7	412			
15	-0.1	114	17.6	213	3.4	313	15.1	413			
16		115	17.8	215	4.0	314	20.7	414			
17	-0.1	116	18.0	216		315	26.2	415	-		-
18		117	17.6	217	6.0	317	26.5	416			
19		118	17.0	218	6.2	318	21.0	418			-
20		119	16.5	219	6.1	319	14.6	419			
21	0.0			220		320		420			
22			18.1	221	5.1	321	5.9	421			
24				222	4.3	322		422			
25				223		323		423			
26		126		224		324		424			-
27				225		325		425			
28				226 227		326 327		426			+
29	0.2			228		328					+
30	0.1	130	22.7	229		329					
31		131	23.4	230		330					
32				231	7.7	331					
33				232		332	0.8				
34				233							
35				234							
36				235							-
38				236							-
39				237							-
40				239							+
41				240							+
42				241							+
43		2 143	74.7	242							
4.4											
4.5				244		34	9.	4 44	4 47.	5	
4.6											
47											
48				24							
50											+
51				24							
52											-
53											
54											+
55											
56		4 15	6 10.	25	6 1.7	35	5 30.	0 45	5 52.	.6	
57					7 1.5	35	6 24.	6 45	6 55.	.8	
58										.4	
59											
60											-
63											
63											+
64											1
6.5											
6.0											
6	7 16.		7 18.	26							
61	8 16.	8 16	8 18.	4 26	8 0.	36	7 16	.0 46	57 53	.8	
6 9				3 26					58 58		-
70											
7									70 65		
7:									71 66		-
7									72 65 73 61		+
7									74 55		
7									75 49		
7									76 44		
7									77 41		
7	9 22	.1 17	9 14.	2 27	9 0.	9 37	8 13	.3 4	78 39	1.8	
8									79 39		
8									80 39		-
8										3.0	-
							32 30			3.9	-
8		.6 18 .7 18					35 41			1.5	+
		.6 18					36 36			3.8	
8		.7 18								5.9	1
		.0 18					38 22			3.2	
	9 10						39 17			1.4	
	0 13						90 16			0.6	
	1 15			3 29	91 4	.6 3	1 18	.6 4	90 20	0.6	
	2 17		2 4	7 29	92 4	.5 3	92 22	.4 4		1.5	
	3 18	.4 19	3 3	5 29	3 3	.7 3	93 26			3.3	
9	4 19	.4 19	94 3	0 29	94 2					5.7	-
9	5 20	.2 19	95 2							7.2	-
	6 21	.2 19	96 2							6.4	-
	7 23				97 1					0.5	-
			101 2	.8 29	98 1	.3 3	98 30	0.5 4	97 2	U.31	1
9	8 25								98 1	6.6	

	Suscept(SI)	Depth (cm) S	Suscent/SI)	Dooth (am)	Comment				
	0.2	101	6.7	Depth (cm)			Suscept(SI)		Suscept(SI)
2		102	6.8		0.9	301	4.4	401	49.7
3	0.5	103	6.3	202	0.8	302	4.7	402	50.8
4	0.5	104	5.2	204	0.7	303	5.3	403	51.7
5	0.5	105	4.0	205	0.7	304	6.5	404	49.0
6	0.6	106	3.0	206	0.7	305	8.5	405	42.1
7	0.5	107	2.2	207	0.7	306	11.5	406	34.1
8		108	1.7	208	0.7	307	15.9	407	28.5
9		109	1.4	209	0.7	308	20.2	408	26.4
10	0.7	110	1.3	210	0.6	309	21.8	409	
11		111	1.3	211	0.6	310	18.9	410	
12	0.6	112	1.3	212		311	13.5	411	
13		113	1.5	213	0.6	312	8.7	412	
14	0.4	114	1.5	214	0.6	313	5.6	413	
15		115	1.6	215	0.6			414	
16		116	1.9	216	0.7	315	2.7	415	
17		117	2.3	217	0.6			416	
18		118	3.0	218	0.6			417	
19		119	3.7	219	0.6			418	
20		120	4.7	220				419	
21	0.4	121	5.7	221	0.6	320		420	
22	0.4	122	6.6	222			0.8	421	
23	0.4	123	7.3	223				422	
24		124	8.0	224		324			
25		125	9.3	225					
26		126	11.4	225	0.6				
27			13.7	226				426	
28			15.4						
29			16.0	228					
30			14.5	229					
31			11.3	230					
32			7.9	231					
33			5.3	232					
34				233					
35			3.6	234					
36			2.0	235					
37			1.4	236					
38			1.0	237					
39			0.8	238					
40			0.7	239					
41			0.7	240					
42			0.8	241					
43			1.0	242					
44			1.1	243					3 131.
45			1.1	244					
			1.0	245					5 123.
46			0.8	246				3 44	6 118.
47			0.6	247			25.9	44	7 113.
48			0.7	248			26.1	8 441	8 111.
4 9			0.6	249			26.	7 44	9 113.
50			0.7	250			1 26.	7 45	0 119.
51			0.8	251			26.4	4 45	1 126.
52			0.8	252		8 35	3 24.	9 45	
5:			0.9	253	0.	7 35	4 23.	0 45	3 142.
54			1.0	254		7 35	5 22.	9 45	4 151
5			1.1	255	0.	6 35	6 24.	8 45	5 161
5 (			1.1	256	0.	6 35	7 28.	7 45	6 170.
51			1.0	257		4 35	8 34.	8 45	
51			0.8	258	0.	5 35	9 41.	7 45	8 187
51		159	0.6	259	0.	4 36			
61	0.0	161	0.8	260	0.				
6			0.8	261					
6:			1.0	262					
6:			1.1	263					
6			1.3	264					
6			1.4	265					
6			1.5	266					
6			1.7	267					
6		100	1.7	268		4 36			
6			1.8		-				
7			1.5						
7			1.2						
7			1.0						
7			0.9						
7			1.0						
7			1.0						
7			1.0						- 302
7			1.0						
7			0.9						E Internation
7			0.9						
	0 3.		1.0						
	1 4.		1.2						
	2 4.		1.3						
	3 5.		1.4						
	4 5.		1.4						
	5 5.		1.7						T HOMES
			1.4						
			1.1			.9 38			
	7 6.								
	8 7		1.0			7 38			
	9 7		1.1			0 39			
	0 6.		1.2						
	1 5.		1.3						
	2 4.		1.5						
	3 3		1.5						
	4 3.		1.3						
	5 3		1.1						
9	6 3	6 197	1.0						
	7 4	1 198	1.0	29					
		.8 199	1.0		A A	.8 39	9 52	.61	Carl Mark College
9	8 4	100	1.0			.0 40			

33.44   -11.067   8.68E-07   151   220.08   (Internally Depth   decimaton inclination intensity   1.69   (Internally Depth   1.	Paleomag	netic Data . (	ORE 2													
9 33.44 - 13.007   5686.07   151   126.156   59.44   542.26   321   10.000   10.000   10.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   152   11.000   1				intensity	Denth	doalination	I									
2 3.093 9.216 1.16£06 150 1.216.22 68.40 341.50 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.405 170 18.											inclination	intensity	Depth	declination	inclination	intensity
4 1.388															60.104	1.91E-05
6 44.009 0.778 1.73E-06 157 218.774 25.19 4.74E-09 207 207.231 25.757 4.8E-05 207 4.8E-05 1.8E-05 1.8E	4	41.388	-4.422													1.52E-05
8 46.629 3.886 1.895-66 159 213.887 62.721 4.395-00 309 527.601 53.555 4.385-00 40.411 59.519 7.55-10 12.53.017 17.151 53.016 161 212.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 21.008 161 2	6	44.009														1.21E-05
10 5.9.017 12.161 20.1666 161 212.068	8	48.629	3.854													9.73E-06
12 98.695		53.917	12.161	2.01E-06												8.12E-06
140 3.5.864		59.695	24.53	2.32E-06												7.35E-06
16   3.4.01   52.029   3.356.00   17  206.442   60.559   3.976.00   17  201.202   3.5.109   3.6.503   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   101.202   42   42   42   42   42   42   42		53.684	40.848	2.63E-06												
18   4.671   52.677   4.936.00   1.99   205.005   60.009   3.916.00   1.99   201.465   64.535   3.425.00   4.69   1.41.1.6   6.892   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985   1.985		32.201	52.029	3.35E-06												8.57E-06
20 351-107 4-3,886 325-500 173 204.090 59.196 4.085-50 321 300.862 37.363 3.565-50 471 125.891 6.4431 8.255-50 173 204.090 59.196 4.085-50 323 301.416 58.68 2.955-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 2.855-50 479 100.931 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.470 1.099 67.47			52.877	4.63E-06												
22, 345,599, 35,686, 1045,000,173, 103,881, 59,424, 1465,000, 323, 300,881, 36,374, 30,850,00, 473, 113,949, 47,476, 20,850, 473, 113,949, 47,476, 20,850, 473, 473, 473, 473, 473, 473, 473, 473				6.36E-06												
24   34.5.92   38.4.66   1.046.09   175   206.381   39.4.24   4.186.09   31.95   31.01.416   59.68   2.95.06   475   106.081   68.097   2.4.55   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01.416   31.01			43.886	8.22E-06	173											
28   342,625   34,025   1485-05   177   209,209   50,112   4,275-05   327   302,632   5,896   2,675-05   477   104,468   64,20   2,755   32,805   34,711   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   34,731   3			38.496	1.04E-05												
28 341,680 30,486 1,416-05 [179] 212,478 61.22 4,916-05 329 395,324 59,992 2,875-05 479 106,378 62,719 5,145 5			34.023	1.25E-05	177											
34 4 54.71					179	212.478										
34 343-71			27.283	1.46E-05	181											
34 345.9					183						-					
36 350,747 28,391 1,196,09 187 218,08 62,902 4,096,08 377 313,881 62,347 2,266,05 487 110,378 80.58 4,826 348 325,09 35,118 9,776,09 19 13,186 61,084 4,182,08 39 312,084 62,991 1,246,06 60,553 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,07 60,055 4,786 40 1,150,055 4,786 40 1,150,055 4,786 40 1,150,055 4,786 40 1,150,055 4,786 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1,150,055 40 1			24.819	1.30E-05	185	217.032										
381 355.789   355.789   355.785   357.805   139 213.86   41.605   34.605   34.1   308.407   69.981   24.865   49.91   117.504   69.224   42.41   42.5782   59.018   9355.06   193 215.24   62.318   4.485.05   4.48   308.407   69.488   221.625   69.312   223.36   60.646   5.024   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485   4.485			28.391	1.13E-05	187											
40 1.667			35.113	9.77E-06	189											
42 5.792 55.018 5.955.08 193 215.24 52.318 4.92.05 342 301.966 55.976 225.65 453 122.356 80.666 5.047 123.656 81.946 11.16.05 192 214.457 82.14 4.996.05 447 123.741 86.654 2.605.05 497 129.484 80.92 5.325 456 80.666 5.47 123.656 81.26.05 197 121.973 56.036 5.18.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.973 56.026 51.05 197 121.05 197 197 197 197 197 197 197 197 197 197																
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46   0.66   64.7   1.51E-05   197   212,943   0.281   4.79E-05   34.7   287.741   66.54   2.60E-05   497   129.464   69.925   5.33E   48   0.066   64.7   1.51E-05   192   211,973   50.304   5.14E-05   51   242,915   63.168   3.29E-05   499   131,339   60.867   5.25E   50.35E-15   5				1.11E-05												
48   0.066   44.7   1.51E-05   199   211.973   59.034   5.14E-05   349.244   66.0458   4.05E-05   501   131.539   0.669   5.44E   52   349.344   60.955   1.79E-05   203   212.031   56.848   6.02E-05   351   22.215   63.156   2.05E-05   501   132.575   6.08E-05   5.08E-05   5			64.697													
50 394.759 6 63.285 1.97E-05 201 212.083 66.924 5.61E-05 351 282.915 63.28E-05 530 132.926 50 132.087 60.94 5.41E 52 349.944 60.955 1.79E-05 205 215.21 51 68.486 6.0265 533 283.99 61.557 38.8E-05 530 33.27.44 61.32 65.41E 53 44.507 54.421 2.005.05 205 215.41 67.285 6.21E-05 355 284.426 60.458 4.08E-05 505 132.099 62.003 5.38E 53 49.991 39.005 205 215.41 67.389 6.18E-05 357 285.675 60.096 44.650 507 131.532 62.993 5.31E 60.000 50 500 50 50 50 50 50 50 50 50 50 50	48	0.066	64.7	1.51E-05												
52 349.544 6 0.955 1.795-05 203 213.231 56.848 6.002-05 353 285.39 61.457 3.865-05 503 132.744 61.326 5.415 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345 61.345																
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58 349.017 5.4.21 2.005.05 207 217.374 57.839 5.185.05 357 285.975 295.975 50.056 4.455.05 507 131.322 82.893 5.185 83 349.045 51.289 2.035.05 209 218.678 57.897 6.155.05 359 27.621 59.421 4.73-05 559 131.078 68.381 0.000 60 339.515 49.391 1.985.05 211 218.383 57.897 6.155.05 359 27.621 59.421 4.73-05 559 131.078 68.207 51.000 60 339.515 49.391 1.985.05 211 218.383 58.676 1.055.05 359 29.581 57.892 5.155.05 511 131.424 64.66 5.145 66 347 29.207 57.208 571 58.687 6.335.05 339 29.294 58.18 57.050.05 531 132.490 65.27 5.175 66 32.15 65.999 1.755.05 215 218.3934 54.681 6.355.05 383 29.294 58.18 57.692 5.155.05 511 132.490 65.27 5.175 66 32.05 57.209 1.755.05 217 220.871 54.67 6.485.05 537 29.756 5.155.05 517 134.711 67.752 5.365 66 327.0572 7.755.05 5.0572 7.7572 5.365 68 320.755 7.72.19 1.985.05 219 225.774 57.498 6.625.05 387 29.758 5.055.05 519 134.712 69.654 5.525 7.0 337.072 75.458 2.345.05 52.245.05 22.23 254.529 69.234 6.225.05 373 29.834 57.55 5.055.05 519 134.712 69.654 5.525 72 354.054 59.20 21.207 7.207 57.452 5.208.71 17.236 5.3755 5.055.05 57.0 39.50 5.05 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 5.0 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.00 57.0 39.			57.788	1.90E-05												
58   340,945   51,299   2,035-05   209   218,678   57.49   18.15-05   351   39.94   1.98-05   31.178   83.818   0.000     60   339.515   43.991   1.98-05   211   218.48   57.19   6.15-05   351   20.938   57.26   5.15-05   511   31.124   46.6   5.146     61   321.5   65.999   1.78-05   217   220.871   54.891   6.84-05   331   220.994   58.18   5.075-05   513   132.549   68.27   5.176     62   320.75   72.779   1.98-05   217   220.871   54.87   6.84-05   337   298.708   57.003   5.155-05   517   134.711   67.792   5.385     63   320.755   72.779   1.98-05   212   225.774   54.87   6.84-05   397   298.708   57.003   5.155-05   517   134.711   67.792   5.385     70   337.072   75.469   2.386-05   221   225.56   62.916   6.865-05   399   27.384   57.505-05   517   134.712   67.692   5.855     71   337.072   75.469   2.386-05   222   225.56   62.916   6.865-05   397   297.384   57.505-05   521   132.049   70.846   5.715     71   3.821   71.791   3.285-05   222   225.56   62.916   6.485-05   371   297.253   58.079   4.885-05   521   122.049   70.846   5.715     71   3.821   71.791   3.285-05   222   303.855   71.818   5.015-05   375   295.644   59.202   4.555-05   525   107.427   65.486   6.355   6.898   70.093   5.875   79.986   59.202   4.555-05   525   107.427   65.486   6.355   78.812   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   79.814   7	56	343.017	54.421	2.00E-05												
60 339.515	58	340.945	51.299	2.03E-05	209											
64 339.189 1.93 57.285 1.73E-09 219 219.2819.89 55.867 6.33E-05 363 292.994 55.175 5.73E-05 513 132.549 65.267 5.17E 64 329.185 57.285 1.73E-09 1.73E-05 217 220.871 54.87 6.84E-05 367 296.706 57.603 5.15E-05 517 134.711 67.732 5.38E 66 320.755 72.719 1.96E-05 217 220.871 54.87 6.84E-05 367 296.706 57.603 5.15E-05 517 134.711 67.732 5.38E 67 0.337.072 75.463 2.34E-05 221 225.56 62.916 6.86E-05 367 297.384 57.505-05 517 134.711 67.732 5.38E 67 0.337.072 75.463 2.34E-05 221 225.56 62.916 6.86E-05 371 297.384 57.505-05 517 134.712 67.632 5.38E 77 33.821 71.781 3.28E-05 222 255.56 62.916 6.86E-05 371 297.384 58.05E-05 521 132.049 70.846 5.71E 77 35.469 67.742 6.86E 5.745 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 5.785 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.06 70.	60	338.515	49.391	1.98E-05												
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66   320.755   72.719   1.966-05   219   225.774   57.496   6.622-05   369   297.384   57.55   50.65-05   519   194.712   69.654   58.52   70.3772   75.463   2.342-05   2.211   225.56   62.216   6.462-05   371   297.525   3697   4885-05   521   322.756   70.108   48.7172   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718   77.718	66	321.5														
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72 394,846 74.159 2.80C-05 223 284.529 69.234 6.22E-05 373 295.6394 59.725 523 122.756 70.108 5.93E 74 3.82E-05 70.049 3.60E-05 225 280.11 72.366 5.97E-05 375 295.646 59.222 4.5E-05 527 80.96E 50.76 6.93E 76 9.865 70.049 3.60E-05 227 303.855 71.818 5.6TE-05 377 295.666 59.322 4.4TE-05 527 99.861 56.076 6.93E 76 12.759 69.714 4.00E-05 229 318.358 70.032 5.24E-05 379 295.666 59.322 4.4TE-05 527 99.861 56.076 6.93E 80 14.234 70.593 4.44E-05 231 327.372 69.12 4.88E-05 381 286.284 59.327 3.6SE-05 531 80.009 29.981 9.6EE 62 13.407 71.553 4.6SE-05 233 332.204 68.713 4.7EE-05 383 2.96E.68 59.99 4.4EE-05 537 99.489 19.62E 0.000 86 1.721 70.628 5.39E-05 233 332.204 68.713 4.7EE-05 383 2.96E.68 59.99 4.4EE-05 533 79.489 19.62E 0.000 86 6.721 70.628 5.39E-05 239 288.422 72.25E 4.11E-05 387 295.729 65.145 2.62E-05 537 81.275 6.979 0.000 86 1.594 70.157 5.05E-05 239 288.422 72.25E 4.11E-05 387 295.729 65.145 2.82E-05 537 81.275 6.979 0.000 90 357.364 70.407 4.89E-05 241 248.634 66.177 4.56E-05 391 293.824 68.63 2.93E-05 543 80.355 2.86E 50 9.94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 68.63 2.93E-05 543 80.355 2.86E 50 9.94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 56.85E 50 543 80.3559 2.89E 0.000 94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 56.85E 50 543 80.3559 2.89E 0.000 94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 56.85E 50 543 80.3559 2.89E 0.000 94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 56.85E 50 543 80.3559 2.89E 0.000 94 356.587 74.263 4.39E-05 243 230.227 56.85E 5.53E-05 391 293.824 56.85E 50 543 80.3559 2.89E 0.000 94 356.587 74.263 4.39E-05 243 230.277 56.85E 5.53E-05 391 293.824 56.85E 50 544 8.85E 50 544			75.463			-										
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Tell   12.759   69.742   4.09E-05   229   318.356   70.022   5.24E-05   379   295.957   59.25   4.20E-05   529   65.152   43.207   8.06E   60   14.234   70.593   4.44E-05   231   327.372   69.12   4.98E-05   381   299.244   59.327   3.85E-05   531   60.609   29.961   9.86E   62   13.407   71.353   4.69E-05   233   332.204   68.713   4.76E-05   383   296.86   59.99   3.48E-05   533   79.499   19.626   0.000   64   10.952   71.263   4.98E-05   237   332.206   80.713   4.76E-05   385   296.85   59.99   3.48E-05   535   80.139   19.626   0.000   68   6.721   70.626   5.03E-05   237   332.206   70.538   4.17E-05   387   295.729   65.145   2.62E-05   535   80.139   19.626   0.000   68   6.721   70.626   5.03E-05   237   32.206   70.538   4.17E-05   387   295.729   65.145   2.62E-05   535   80.139   12.75   6.6979   0.000   68   6.721   70.626   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.000   70.757   70.0000   70.757   70.0000   70.757   70.0000   70.757   70.0000   7																
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88   1.594   70.157   5.05E-05   239   288.842   72.256   4.11E-05   389   294.481   67.28   2.57E-05   539   82.123   4.381   0.000   90   357.364   70.407   4.89E-05   241   248.634   66.177   4.56E-05   391   293.624   68.63   2.39E-05   541   82.737   3.521   0.000   94   356.587   74.263   4.33E-05   245   224.018   50.913   6.63E-05   395   286.577   71.921   2.35E-05   543   83.559   2.895   0.000   96   9.821   75.61   4.19E-05   247   224.118   48.141   7.67E-05   397   279.102   72.249   2.44E-05   547   88.541   3.774   8.55E   98   27.373   73.564   4.19E-05   247   224.134   48.141   7.67E-05   397   279.102   72.249   2.44E-05   547   88.641   3.774   8.55E   98   27.373   73.564   4.19E-05   247   224.134   48.141   7.67E-05   397   279.102   72.249   2.44E-05   547   88.641   3.774   8.55E   98   27.373   73.564   4.19E-05   247   224.434   47.377   8.57E-05   399   275.295   71.216   2.60E-05   549   95.583   11.678   6.52E   100   39.871   68.556   4.22E-05   251   224.459   47.815   9.18E-05   401   275.23   68.612   2.87E-05   551   109.175   30.117   4.341   102   47.79   63.06   4.22E-05   255   228.624   48.795   9.37E-05   403   276.627   66.49   3.19E-05   553   311.686   53.321   3.631   104   54.204   58.793   4.27E-05   255   228.030   50.13   9.13E-05   405   278.627   63.754   3.49E-05   555   153.31   67.762   3.51   106   60.227   56.599   4.46E-05   257   229.703   51.922   8.55E-05   407   20.446   60.406   3.79E-05   557   157.497   75.634   3.322   108   65.124   55.764   4.76E-05   259   230.678   53.886   7.74E-05   409   283.035   57.394   4.14E-05   559   139.378   79.694   3.03   110   65.999   55.493   5.01E-05   263   234.638   57.992   5.72E-05   413   286.605   4.71E-05   563   389.504   77.768   2.29   114   63.31   63.532   5.23E-05   263   296.862   72.003   2.45E-05   417   226.704   78.579   4.58E-05   4.77E-05   4.77E-05																
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98 27.373 73.564 4.19E-05 249 223.047 47.377 8.57E-05 399 275.295 71.216 2.60E-05 549 95.583 11.678 6.21 100 39.871 68.558 4.22E-05 251 224.459 47.815 9.18E-05 401 275.23 68.612 2.67E-05 551 109.175 30.117 4.341 102 47.79 63.06 4.22E-05 253 226.242 48.795 9.37E-05 403 276.627 66.49 3.19E-05 553 131.658 63.321 3.631 104 54.204 58.793 4.27E-05 255 228.203 50.13 9.13E-05 403 276.627 66.49 3.19E-05 553 131.658 63.321 3.631 106 60.227 56.596 4.46E-05 257 229.703 51.922 8.55E-05 407 280.448 60.406 3.79E-05 557 157.497 75.634 3.321 108 65.124 55.764 4.76E-05 259 230.678 53.868 7.74E-05 409 283.035 57.394 4.14E-05 559 139.378 79.694 3.301 110 66.999 55.493 5.01E-05 261 231.403 55.651 6.79E-05 411 284.608 55.96 0.000.45 561 110.208 79.971 2.681 111 65.31 56.332 5.23E-05 263 232.438 57.992 5.72E-05 413 283.462 56.965 4.71E-05 563 89.504 77.763 2.291 114 63.31 56.332 5.23E-05 263 236.682 72.003 2.45E-05 415 279.301 61.125 4.66E-05 110.208 79.971 2.681 118 69.219 59.532 5.22E-05 265 302.459 65.427 3.34E-05 417 227.2593 68.632 4.52E-05 124 50.762 59.68 4.76E-05 271 307.731 56.592 5.79E-05 412 272.593 68.692 4.52E-05 124 50.762 59.68 4.76E-05 273 309.375 55.215 6.11E-05 4.71E-05 50.404 4.71E-05 59.68 4.76E-05 273 309.375 55.215 6.11E-05 4.71E-05 50.404 4.71E-05 59.68 4.71E-05 59.69 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.642 50.6																
100   39.871   68.558   4.22E-05   251   224.459   47.815   9.18E-05   401   275.23   68.612   2.87E-05   551   109.175   30.117   4.341     102   47.79   63.06   4.22E-05   253   226.242   48.795   9.37E-05   403   276.627   66.49   3.19E-05   553   131.568   53.321   3.631     104   54.204   58.793   4.27E-05   255   228.203   50.13   9.13E-05   405   278.207   63.754   3.49E-05   555   153.31   67.762   3.631     106   60.227   56.596   4.46E-05   257   229.703   51.922   8.55E-05   407   280.448   60.406   3.79E-05   555   153.31   67.762   3.321     108   65.124   55.764   4.76E-05   259   230.678   53.888   7.74E-05   409   283.035   57.394   4.14E-05   559   139.378   79.694   3.031     110   66.999   55.493   5.01E-05   261   231.403   55.651   6.79E-05   411   284.608   55.96   0.000045   561   110.208   79.971   2.281     112   65.752   55.565   5.16E-05   263   232.438   57.992   5.72E-05   413   283.462   56.965   4.71E-05   563   89.504   77.763   2.291     114   63.31   56.332   5.23E-05   265   302.495   65.427   3.34E-05   417   276.2704   78.579   4.59E-05     118   59.219   59.532   5.22E-05   267   304.621   61.092   4.17E-05   417   262.704   78.579   4.59E-05     120   57.112   60.023   5.18E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05     124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05     128   49.929   66.645   4.46E-05   277   312.816   52.595   5.89E-05   429   110.693   56.86   5.99E-05     130   55.022   75.322   4.19E-05   281   314.187   52.929   5.89E-05   429   110.693   56.86   5.99E-05     131   84.769   85.264   4.49E-05   281   314.187   52.929   5.89E-05   429   110.693   56.86   5.99E-05     131   84.769   85.264   4.49E-05   283   314.187   52.929   5.89E-05   429   110.693   56.86   5.99E-05     133   220.286   67.303   5.35E-05   287   310.46   59.114   4.10E-05   433   104.174   55.075   4.93E-05     134   220.443   56.336   6.68E-05   293   306.136   60.288   3.99E-05   441   98.249																
102   47.79   63.06   4.22E-05   253   226.242   48.795   9.37E-05   403   276.627   66.49   3.19E-05   553   131.568   53.321   3.631     104   54.204   58.793   4.27E-05   255   228.203   50.13   9.13E-05   405   278.207   63.754   3.49E-05   555   153.31   67.62   3.531     106   60.227   56.596   4.46E-05   257   229.703   51.922   8.55E-05   407   280.448   60.406   3.79E-05   557   157.497   75.634   3.321     108   65.124   55.764   4.76E-05   259   230.678   53.888   7.74E-05   409   283.035   57.394   4.14E-05   559   139.378   79.694   3.031     110   66.999   55.493   5.01E-05   261   231.403   55.651   6.79E-05   411   284.608   55.96   0.000045   561   110.208   79.971   2.681     112   65.752   55.565   5.16E-05   263   232.438   57.992   5.72E-05   413   283.462   56.965   4.71E-05   563   89.504   77.763   2.291     114   63.31   56.332   5.23E-05   263   296.862   72.003   2.45E-05   415   279.301   61.125   4.66E-05     118   59.219   59.532   5.22E-05   267   304.621   61.092   4.17E-05   4.17   262.704   78.579   4.59E-05     120   57.112   60.023   5.18E-05   269   306.428   58.505   4.90E-05   419   220.34   86.96   4.87E-05   8.94E-05     124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05   4.99E-05   124   4.9.368   61.331   4.76E-05   273   307.731   56.592   5.59E-05   427   108.79   61.361   5.33E-05   5.03E-05   131   84.769   85.254   4.19E-05   283   314.187   52.929   5.44E-05   431   110.326   54.844   5.59E-05   133   201.724   82.646   4.96E-05   283   314.187   52.929   5.44E-05   433   101.734   56.275   4.93E-05   133   220.286   67.303   5.35E-05   291   301.737   60.664   3.62E-05   441   98.249   57.125   3.99E-05   441   220.443   5.67E-05   429   4.90E-05   441   4.90E-05   4.93E-05   4.93E-0																
104   54.204   58.793   4.27E-05   255   228.203   50.13   9.13E-05   405   278.267   63.754   3.49E-05   555   153.31   67.762   3.51																
106   60.227   56.596   4.46E-05   257   229.703   51.922   8.55E-05   407   280.448   60.406   3.79E-05   557   157.497   75.634   3.32     108   65.124   55.764   4.76E-05   259   230.678   53.888   7.74E-05   409   283.035   57.394   4.14E-05   559   139.378   79.694   3.03     110   66.999   55.493   5.01E-05   261   231.403   55.651   6.79E-05   411   284.608   55.96   0.000045   561   110.208   79.971   2.681     112   65.752   55.565   5.16E-05   263   232.438   57.992   57.72E-05   413   283.462   56.965   4.71E-05   563   89.504   77.763   2.29     114   63.31   56.332   5.23E-05   263   296.862   72.003   2.45E-05   415   279.301   61.125   4.66E-05     118   69.219   59.532   5.22E-05   267   304.621   61.092   4.17E-05   417   272.593   68.632   4.52E-05     120   57.112   60.023   5.18E-05   269   306.428   58.505   4.90E-05   419   220.34   86.96   4.87E-05     122   53.993   59.692   5.10E-05   271   307.731   56.592   5.59E-05   423   104.935   76.186   5.03E-05     124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05     128   49.929   68.645   4.46E-05   277   312.816   52.508   6.31E-05   423   104.935   76.186   5.03E-05     130   55.022   75.322   4.19E-05   281   311.187   52.929   5.44E-05   431   110.326   54.844   5.59E-05     131   84.769   85.254   4.19E-05   281   311.187   52.929   5.44E-05   431   110.326   54.844   5.39E-05     133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05     133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05     134   220.286   67.303   5.35E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05     145   220.199   56.342   6.67E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05     145   220.199   56.342   6.67E-05   295   294.033   61.333   3.89E-05   445   88.916   57.298   3.29E-05     147   220.581   56.976   6.69E-05   297   291.688   60.397   4.02E																
108																
110   66.999   55.493   5.01E-05   261   231.403   55.651   6.79E-05   411   284.608   55.96   0.000045   561   110.208   79.971   2.681   112   65.752   55.565   51.6E-05   263   232.438   57.992   57.2E-05   413   283.462   56.965   4.71E-05   563   89.504   77.763   2.29   114   63.31   56.332   5.23E-05   263   296.862   72.003   2.45E-05   415   297.301   61.125   4.66E-05   563   89.504   77.763   2.29   116   61.01   58.036   5.24E-05   265   302.459   65.427   3.34E-05   417   272.593   68.632   4.52E-05   118   59.219   59.532   5.22E-05   267   304.621   61.092   4.17E-05   417   262.704   78.579   4.59E-05   120   57.112   60.023   5.18E-05   279   306.428   58.505   4.90E-05   417   262.704   78.579   4.59E-05   122   53.993   59.692   5.10E-05   271   307.731   56.592   5.59E-05   421   113.866   83.656   5.04E-05   124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05   128   49.929   66.645   4.46E-05   277   312.816   52.508   6.31E-05   427   108.79   61.361   5.33E-05   128   49.929   66.645   4.49E-05   279   313.925   52.023   5.98E-05   429   110.693   56.86   5.99E-05   131   84.769   85.254   4.19E-05   283   314.175   52.529   5.44E-05   433   107.628   54.414   5.33E-05   133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05   133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05   133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05   141   221.17   58.399   6.37E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05   141   221.17   58.399   6.37E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05   141   220.443   56.738   6.76E-05   297   291.688   60.397   4.02E-05   447   82.499   57.589   2.85E-05   147   20.581   56.966   6.69E-05   297   291.688   60.397   4.02E-05   447   82.499   57.589   2.85E-05   147   20.581   56.966   6.69E-																
112   65.752   55.565   5.16E-05   263   232.438   57.992   5.72E-05   413   283.462   56.965   4.71E-05   563   89.504   77.763   2.29     114   63.31   56.332   5.23E-05   263   296.862   72.003   2.45E-05   415   279.301   61.125   4.66E-05     116   61.01   58.036   5.24E-05   265   302.459   65.427   3.34E-05   417   272.593   68.632   4.52E-05     118   59.219   59.532   5.22E-05   267   304.621   61.092   4.17E-05   417   262.704   78.579   4.59E-05     120   57.112   60.023   5.16E-05   269   306.428   58.505   4.90E-05   419   220.34   86.96   4.87E-05     122   53.993   59.692   5.10E-05   271   307.731   56.592   5.59E-05   421   113.866   83.656   5.04E-05     124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05     126   49.368   61.381   4.76E-05   275   311.215   53.787   6.36E-05   425   106.047   68.406   5.07E-05     128   49.929   66.645   4.46E-05   277   312.816   52.508   6.31E-05   427   108.79   61.361   5.33E-05     130   55.022   75.322   4.19E-05   281   314.187   52.923   5.48E-05   431   110.326   54.844   5.59E-05     131   84.769   85.254   4.19E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05     133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05     137   220.286   67.303   5.35E-05   287   310.46   59.114   4.10E-05   437   107.34   56.213   4.57E-05     141   221.17   58.399   6.37E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05     141   220.443   56.738   6.78E-05   295   294.033   61.333   3.89E-05   4447   82.499   57.589   2.85E-05																
114         63.31         56.332         5.23E-05         263         296.862         72.003         2.45E-05         415         279.301         61.125         4.66E-05           116         61.01         58.036         5.24E-05         265         302.459         65.427         3.34E-05         417         272.593         68.632         4.52E-05         6           118         59.219         59.532         5.2EE-05         267         304.621         61.092         4.17E-05         417         222.593         68.632         4.52E-05         6           120         57.112         60.023         5.18E-05         269         306.428         58.505         4.90E-05         419         220.34         86.96         4.87E-05           122         53.993         59.692         5.10E-05         271         307.731         56.592         5.59E-05         421         113.866         83.656         5.04E-05           124         50.76         59.68         4.97E-05         273         309.375         55.215         6.11E-05         423         104.935         76.186         5.09E-05         126         49.368         6.0840         5.07E-05         128         128         49.929         66.645																
116         61.01         58.036         5.24E-05         265         302.459         65.427         3.34E-05         417         272.593         68.632         4.52E-05         118         59.219         59.532         5.22E-05         267         304.621         61.092         4.17E-05         417         262.704         78.579         4.59E-05         120         57.112         60.023         5.18E-05         269         306.428         58.505         4.90E-05         419         220.34         86.96         4.87E-05         122         53.993         59.692         5.10E-05         271         307.731         56.592         5.59E-05         421         113.866         83.656         5.04E-05         126         49.368         4.97E-05         273         309.375         55.215         6.11E-05         423         104.935         76.186         5.03E-05         126         49.368         61.381         4.76E-05         275         311.215         53.787         6.36E-05         425         106.047         68.406         5.07E-05         128         49.929         68.645         4.46E-05         277         312.816         52.508         6.31E-05         427         108.79         61.361         5.32E-05         108.79         61.361														09.30	17.76	2.29E-0
118         59.219         59.532         5.22E-05         267         304.621         61.092         4.17E-05         417         262.704         78.579         4.59E-05           120         57.112         60.023         5.18E-05         269         306.428         58.505         4.90E-05         419         220.34         88.96         4.87E-05         125         53.993         59.692         5.99E-05         421         113.866         83.656         5.04E-05         5         128         4.90E-05         273         309.375         55.215         6.11E-05         423         104.935         76.186         5.04E-05         5         128         49.929         66.645         4.46E-05         275         311.215         53.787         6.36E-05         425         106.047         68.406         5.07E-05         128         49.929         66.645         4.46E-05         277         312.816         52.508         6.31E-05         427         108.79         61.361         5.33E-05         98         130         55.022         75.322         4.19E-05         279         313.925         52.023         5.98E-05         429         110.693         56.86         5.59E-05         131         84.769         85.254         4.19E-05														+	+	-
120   57.112   60.023   5.18E-05   269   306.428   58.505   4.90E-05   419   220.34   86.96   4.87E-05     122   53.993   59.692   5.10E-05   271   307.731   56.592   5.59E-05   421   113.866   83.656   5.04E-05     124   50.76   59.68   4.97E-05   273   309.375   55.215   6.11E-05   423   104.935   76.186   5.03E-05     126   49.368   61.381   4.76E-05   275   311.215   53.787   63.36E-05   425   106.047   68.406   5.07E-05     128   49.929   66.645   4.46E-05   277   312.816   52.508   6.31E-05   427   108.79   61.361   5.33E-05     130   55.022   75.322   4.19E-05   279   313.925   52.023   5.98E-05   429   110.693   56.86   5.59E-05     131   84.769   85.254   4.19E-05   281   314.187   52.929   5.44E-05   431   110.326   54.844   5.59E-05     133   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   4.33   107.628   54.413   5.33E-05     137   220.286   67.303   5.35E-05   287   310.46   59.114   4.10E-05   437   101.734   56.213   4.57E-05     139   221.246   61.949   5.84E-05   289   306.134   60.238   3.90E-05   439   100.253   56.903   4.28E-05     141   221.17   58.399   6.37E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05     145   220.488   56.976   6.69E-05   297   291.688   60.397   4.02E-05   447   82.499   57.589   2.85E-05														+	+	
122       53.993       59.692       5.10E-05       271       307.731       56.592       5.59E-05       421       113.866       83.656       5.04E-05       124       50.76       59.68       4.97E-05       273       309.375       55.215       6.11E-05       423       104.935       76.186       5.03E-05       126       49.368       61.381       4.76E-05       275       311.215       53.787       6.36E-05       425       106.047       68.406       5.07E-05       108.79       61.361       5.33E-05       131       130       55.022       75.322       4.19E-05       279       313.925       52.023       5.98E-05       429       110.693       56.86       5.59E-05       131       84.769       85.254       4.19E-05       281       314.187       52.929       5.44E-05       431       110.326       54.844       5.59E-05       110.326       54.844       5.59E-05       133       201.724       82.642       4.49E-05       283       314.175       54.752       4.90E-05       433       107.628       54.413       5.33E-05       135       215.906       74.443       4.92E-05       285       312.969       57.052       4.44E-05       435       104.174       55.075       4.93E-05       137													_	-	+	-
124         50.76         59.68         4.97E-05         273         309.375         55.215         6.11E-05         423         104.935         76.186         5.03E-05           126         49.368         61.381         4.76E-05         275         311.215         53.787         6.36E-05         425         106.047         68.406         5.07E-05           128         49.929         66.645         4.46E-05         279         312.816         52.508         6.31E-05         427         108.79         61.361         5.33E-05           130         55.022         75.322         4.19E-05         279         313.925         52.023         5.98E-05         429         110.693         56.86         5.59E-05           131         84.769         85.254         4.19E-05         281         314.187         54.752         4.90E-05         431         110.326         54.443         5.98E-05           133         201.724         482.642         4.49E-05         283         314.175         54.752         4.90E-05         433         107.628         54.413         5.38E-05           135         215.906         74.443         4.92E-05         285         312.969         57.052         4.44E-05         <														-	+	
126         49.368         61.381         4.76E-05         275         311.215         53.787         6.36E-05         425         106.047         68.406         5.07E-05           128         49.929         66.645         4.46E-05         277         312.816         52.508         6.31E-05         427         108.79         61.361         5.33E-05           130         55.022         75.322         4.19E-05         279         313.925         52.023         5.98E-05         429         110.693         56.86         5.99E-05           131         84.769         85.254         4.19E-05         281         314.187         52.929         5.44E-05         431         110.326         54.844         5.59E-05           133         201.724         82.642         4.49E-05         283         314.175         54.752         4.90E-05         433         107.628         54.413         5.33E-05           135         215.906         74.443         4.92E-05         285         312.969         57.052         4.44E-05         435         104.174         55.075         4.93E-05           139         221.246         61.949         5.84E-05         289         306.134         60.238         3.90E-05														+	-	-
128         49.929         66.645         4.46E-05         277         312.816         52.508         6.31E-05         427         108.79         61.361         5.33E-05           130         55.022         75.322         4.19E-05         279         313.925         52.023         5.98E-05         429         110.693         56.86         5.59E-05           131         84.769         85.254         4.19E-05         281         314.187         52.929         5.44E-05         431         110.326         54.844         5.59E-05         54.844         5.59E-05         54.844         5.59E-05         54.844         5.59E-05         54.844         5.33E-05         283         314.175         54.752         4.90E-05         433         107.628         54.413         5.33E-05         285         312.969         57.052         4.44E-05         435         104.174         55.075         4.93E-05         54.93E-05         137         220.286         67.303         5.35E-06         287         310.46         59.114         4.10E-05         437         101.734         56.213         4.57E-05         137         221.246         61.949         5.84E-05         289         306.134         60.238         3.90E-05         437         101.734														+	+	-
130   55.022   75.322   4.19E-05   279   313.925   52.023   5.98E-05   429   110.693   56.86   5.59E-05     131   84.769   85.254   4.19E-05   281   314.187   52.929   5.44E-05   431   110.326   54.844   5.59E-05     132   201.724   82.642   4.49E-05   283   314.175   54.752   4.90E-05   433   107.628   54.413   5.33E-05     135   215.906   74.443   4.92E-05   285   312.969   57.052   4.44E-05   435   104.174   55.075   4.93E-05     137   220.286   67.303   5.35E-05   287   310.46   59.114   4.10E-05   437   101.734   56.213   4.57E-05     139   221.246   61.949   5.84E-05   289   306.134   60.238   3.90E-05   439   100.253   56.903   4.28E-05     141   221.17   58.399   6.37E-05   291   301.757   60.664   3.82E-05   441   98.249   57.125   3.99E-05     143   220.443   56.738   6.76E-05   293   297.724   61.037   3.83E-05   443   94.37   57.197   3.67E-05     145   220.199   56.342   6.87E-05   295   294.033   61.333   3.89E-05   445   88.916   57.298   3.29E-05     147   220.581   56.976   6.69E-05   297   291.688   60.397   4.02E-05   447   82.499   57.589   2.85E-05														+	-	-
131															-	
133     201.724     82.642     4.49E-05     283     314.175     54.752     4.90E-05     4.33     107.628     54.413     5.33E-05       135     215,906     74.443     4.92E-05     285     312,969     57.052     4.44E-05     435     104.174     55.075     4.93E-05       137     220.286     67.303     5.35E-05     287     310.46     59.114     4.10E-05     437     101.734     56.213     4.57E-05       139     221.246     61.949     5.84E-05     289     306.134     60.238     3.90E-05     439     100.253     56.903     4.28E-05       141     221.17     58.399     6.37E-05     291     301.757     60.664     3.82E-05     441     98.249     57.125     3.99E-05       143     220.443     56.738     6.78E-05     293     297.724     61.037     3.83E-05     443     94.37     57.197     3.67E-05       145     220.198     56.342     6.87E-05     295     294.033     61.333     3.89E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.88E-05														+	+	
135     215.906     74.443     4.92E-05     285     312.969     57.052     4.44E-05     435     104.174     55.075     4.93E-05       137     220.286     67.303     5.55E-05     287     310.46     59.114     4.10E-05     437     101.734     56.213     4.57E-05       139     221.246     61.949     5.84E-05     289     306.134     60.238     3.90E-05     439     100.253     56.903     4.28E-05       141     221.17     58.399     6.37E-05     291     301.757     60.664     3.82E-05     441     98.249     57.125     3.99E-05       143     220.443     56.738     6.76E-05     293     297.724     61.037     3.83E-05     443     94.37     57.127     3.67E-05       145     220.199     56.342     6.87E-05     295     294.033     61.333     3.89E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.85E-05														-	-	+
137     220.286     67.303     5.35E-05     287     310.46     59.114     4.10E-05     437     101.734     56.213     4.57E-05       139     221.246     61.949     5.84E-05     289     306.134     60.238     3.90E-05     439     100.253     56.903     4.28E-05       141     221.17     58.399     6.37E-05     291     301.757     60.664     3.82E-05     441     82.49     57.125     3.99E-05       143     220.443     56.738     6.76E-05     293     297.724     61.037     3.83E-05     443     94.37     57.197     3.67E-05       145     220.199     56.342     6.67E-05     295     294.033     61.333     3.89E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.85E-05																
139     221.246     61.949     5.84E-05     289     306.134     60.238     3.90E-05     439     100.253     56.903     4.28E-05       141     221.17     58.399     6.37E-05     291     301.757     60.664     3.82E-05     441     98.249     57.125     3.99E-05       143     220.443     56.738     6.76E-05     293     297.724     61.037     3.83E-05     443     94.37     57.197     3.67E-05       145     220.199     56.342     6.87E-05     295     294.033     61.333     3.89E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.85E-05															-	-
141     221.17     58.399     6.37E-05     291     301.757     60.664     3.82E-05     441     98.249     57.125     3.99E-05       143     220.443     56.738     6.76E-05     293     297.724     61.037     3.83E-05     443     94.37     57.197     3.67E-05       145     220.199     56.342     6.87E-05     295     294.033     61.333     3.99E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.85E-05														-	-	-
143     220.443     56.738     6.76E-05     293     297.724     61.037     3.83E-05     443     94.37     57.197     3.67E-05       145     220.199     56.342     6.87E-05     295     294.033     61.333     3.89E-05     445     88.916     57.298     3.29E-05       147     220.581     56.976     6.69E-05     297     291.688     60.397     4.02E-05     447     82.499     57.589     2.85E-05														-		
145 220.199 56.342 6.87E-05 295 294.033 61.333 3.89E-05 445 88.916 57.298 3.29E-05 147 220.581 56.976 6.69E-05 297 291.688 60.397 4.02E-05 447 82.499 57.589 2.85E-05														-	+	
147 220.581 56.976 6.69E-05 297 291.688 60.397 4.02E-05 447 82.499 57.589 2.85E-05																-
														-		
149 220.458 58.281 6.32E-05 299 292.129 58.935 4.20E-05 449 74.731 58.407 2.37E-05														-	-	-
	149	220.45	58.28	1 6.32E-0	5 29	9 292.12	9 58.93	5 4.20E-0	5 44	9 74.7	31 58.40	7 2.37E-	05			

Paleoman	netic Data - C	OPE 2													
	declination i		intensity	Dooth	d!!!!										
0		4.588			declination			Depth	declination	inclination	ntensity	Depth	declination	inclination	intensity
2	356.875	4.765		150	16.966	52.198	1.26E-05	301	96.479	64	4.22E-07	450	38.911	59.449	2.73E-05
4	0.246	8.527		152	350.758	65.551	7.81E-06	303	105.336	64.377	4.12E-07	452	36.587	59.723	2.57E-05
6	4.371			154	288.099	68.742	5.62E-06	305	147.019	48.29	5.5E-07	454	35.495	62.262	2.39E-05
8		14.981 23.083		156	254.625	61.37	4.54E-06	307	161.209	29.942	1.05E-06	456	32.895	65.781	
10	9.285			158	241.156	56.477	3.78E-06	309	163.246	26.337	1.71E-06	458	32.107	70.557	
12	15.454 24.813	34.12		160	233.225	56.317	3.28E-06	311	161.563	30.269	2.23E-06	460	35.534	75.917	
14	40.222	47.877		162	227.933	59.498	3E-06	313	158.342	36.68	2.56E-06	462	46.995	79.015	
16		60.079		164	226.992	64.989		315	155.655	40.874	2.71E-06	464	53.569	78.059	
	59.92	67.366		166	224.686	75.114	2.64E-06	317	154.316	41.551	2.67E-06	466		74.667	3.34E-05
18	75.532	70.133		168	249.653	82.787	2.65E-06	319	154.148	42.132	2.58E-06	468		71.455	
20	85.298	71.119		170	333.387	84.074	2.85E-06	321	154.045	45.573	2.51E-06	470		69.077	
22	94.909	61.792		172	21.359	76.361	3.26E-06	323	152.349	51.546	2.31E-06	472		67.758	
24	106.542	62.189		174	21.986	70.005	3.81E-06	325	144.4	61.224	1.83E-06	474		67.071	
26	116.928	61.177		176	21.131	66.341	4.28E-06	327	81.985	75.835	1.28E-06	476		66.85	
28	123.417	60.133		178	20.788	63.841	4.54E-06	329	7.289	51.624	1.15E-06	478		66.067	
30	128.028	60.083		180	22.042	60.894	4.76E-06	331	353.328	33.014	1.28E-06			63.843	
32	132.147	61.086		182	28.004	56.52	5.19E-06	333	345.71	25.781	1.4E-06			60.602	
34	136.574	62.333		184	29.287	53.824	5.6E-06	335	340.789	23.973	1.6E-06			58.756	
36		64.635		186	29.718	51.958	5.61E-06	337	338.136	24.739	1.95E-06			58.951	
38	146.54	69.22		188	29.077	50.174	5.23E-06	339	330.122	28.755	2.34E-06				
40	152.829	77.45		190	27.76	49.832		341	319.345	43.836	2.27E-06				
42	199.881	86.781		192		52.303		343	228.082	66.386	2.53E-06				
44	293.163	81.489		194	29.293	55.174		345	174.359	39.82	5.63E-06				
46	288.638	77.145		196	30.561	55.24		347	163.145	32.851	1.06E-05				
48	254.035	76.838		198		54.459		349	154.056	35.363	1.54E-05				
50		71.983		200	25.712	57.238	2.64E-06	351	148.037	40.907	1.86E-05				
52		66.042			22.596	64.341		353	143.859	44.888					
54	171.369	65.19			22.272	70.894	1.96E-06	355	141.827	45.107	2.05E-05				
56		66.433				74.358	1.79E-06	357	143.657	43.257	2.08E-05				
58		66.284				76.618	1.73E-06	359	145.834	42.255	2.18E-05				
60		64.513			44.764	76.454	1.79E-06	361	147.133	42.38					
62		64.982				73.577	1.96E-06	363	146.189						
64		64.901	6.82E-06	214	34.152	69.546	2.18E-06	365	143.876		1.66E-05				
66		64.813	7.92E-06	216	31.043				142.401	54.147					
68	133.183	62.367	8.93E-06	218	30.181				148.338						
70		61.621	9.82E-06	220					161.773						
72		63.012	1.08E-05	222	28.529				167.381						
74	119.097	66.182	1.16E-05	224					168.43						
76		68.086	1.16E-05	226					167.349						
78	101.602	68.719	1.07E-05	228					164.878						
80	97.44	69.592	9.66E-06	230					162.034						
82	98.087	71.209	9.12E-06	232					160.42						
84	100.891	73.571	8.7E-06						160.131						
86	97.705	73.769	7.94E-06						159.536						
88	88.818	75.851							156.587						
90	72.944	73.577							148.235						
92	85.033	75.08							118.455						
94	105.028	75.226	5.96E-0	244					46.47						
96	117.49	74.059							20.954						
98		72.757													
100		72.468													
102		73.673													
104		75.019													
106		74.63													
108		71.87													
110		69.08													
112		68.19													
114		69.20													
116		69.69													
118															
120							1 2.13E-0				4.66E-C				
122							2 2.14E-0				5.99E-0				
124															
126															
128											7 1.14E-0				
130															
132											3 1.61E-0				
134															
136															
138			4 4.67E-0								2 0.00002				
140							6 5.66E-0				6 2.69E-				
142											1 2.82E-				
144															
146											9 2.94E-				
148											2 2.87E-				
140	27.255	45.09	2.022-0				9 4.62E-0		71.01	00.00					
		1		29	9 114.2	41 00.17	9.02E-U	-	-						

Paleomagn	etic Data - C	ORF 4													
	eclination i		intensity	Depth	declination	inclination	laterate.			-					
0	9.235	-54.293		150	256.617	40.067				inclination			declination		
2	32.074	-55.04		152	251.193	49.471	2.52E-06 1.8E-06	301	233.248	56.609	2.73E-05	451	55.679	56.678	0.000128
4	47.802	-50.792	4.13E-07	154	252.534	59.387	1.41E-06	305	236.577 242.295	58.441 64.291	2.59E-05 2.29E-05	453 455	59.11 62.787	54.534 52.215	
6	56.216	-45.501		156	253.23	77.879	1.1E-06	307	249.513	68.211	2.02E-05	457	67.183	50.393	9.21E-05
8	61.328	-38.979		158	297.419	84.839		309	243.591	70.551	1.76E-05	459	72.708	48.641	7.94E-05
10	65.12	-31.623		159	350.509	81.51	7.78E-07	311	230.742	69.079	1.59E-05	461	77.339	47.578	6.68E-05
12	66.631	-24.752		159	191.006	55.817	4.84E-07	313	223.494		1.53E-05	463	78.517	46.555	5.31E-05
14	59.147	-18.684 -13.589		161	187.692	53.735		315	224.903	67.656	1.47E-05	465	72.856	45.434	3.69E-05
18	52.48	-9.963		163	185.588	55.923		317	234.484		1.25E-05	467	53.838	42.684	
20	45.161	-7.802		165	184.738	58.898		319	262.851		9.03E-06	469	7.579	26.405	
22	38.69	-6.578		169	184.928 185.215	60.976		321	322.487		6.01E-06	471		-7.657	1.07E-05
24	34.759	-6.139		171	184.802	61.735 62.68		321	187.36		4.48E-07	473		-25.711	
26	32.319	-6.464		173	184.194	63.642		323	191.563		5.62E-07	475		-33.499	
28	30.329	-6.958		175		64.408		327	208.662		7.04E-07 8.6E-07	477	271.937	-34.537	1.69E-03
30	28.361	-6.625	5.19E-07	177	182.439	64.695		329	200.992		1.05E-06	965	776	7 7 7 7	
32	26.631	-5.647		179		64.414		331	187.303		1.3E-06	734	9.5		
34	25.563	-4.721			179.06	62.923		333	175.94				7.4	6.35	
36	25.069	-2.744				58.171	1.56E-06	335	166.443						
38	24.428	1.585				52.457	1.8E-06	337	156.071						
40	23.357	7.412				50.327		339	142.296	80.487	3.4E-06	Till		1 - 1	
42	21.802	12.342				52.548		341	127.859						-
46	19.362	15.655 17.826				55.238		343	116.148					20.00	
48	15.242	18.415				56.447		345							-
50	14.835	17.155				57.219 59.221		347	122.185					-	-
52	14.812	15.719				62.276		349					-		-
54	14.783	15.263						351 353					-	70	-
56	15.094	14.954						355					-		1
58	15.81	7.411							122.82						1
60	15.366	6.549	8.94E-07					359					1 12	111	
62	14.475	7.036											1.7	17 341	
64	13.161	8.841				81.064							1.0	12.501	
66	11.1	11.375							43.38			5	1. 1.1.1	2.001	
68	8.549	15.541											31131	1.0.1631	
70	7.271	23.457												1 - 202	
72	11.026	36.586												1 11	
74	23.982	50.582												1	-
76 78	42.055 52.926	56.444											-	1	
80	59.508	50.24											-	-	+
82	61.331	47.60											-	+	-
84	60.827	47.90											1.48	46.50	1
86	62.428	47.02											7.5.5.	19.00	1
88	62.706	48.39											1.87	1.4	
90	62.777	50.5	3 5.52E-0	6 237	179.82									1 1 1	
92	62.172	53.01	5 5.81E-0	6 239	180.49	59.05	3 6.43E-0	7 391	119.34	1 71.429	4.54E-0	5	153	The Late	
94	60.378	54.46		6 24	1 183.52	58.47	4 7.28E-0	393	119.4	9 72.15	5.34E-0	5	1000	160 101	
96	57.008	55.05											6.44	1 711	
9.8	52.88	56.10												11111	-
100	44.777	59.94												10 39	-
102	30.787	64.											-	-	-
104	16.954	65.71											-	+	+
106	354.583 336.053	63.49 57.72											-	+	
110	336.053	57.72											+	1	
112	300.561	56.69												1	
114	254.434	67.65													
116	185.064	64.0													
118	156.317														
120			8 2.39E-0				2 8.75E-0			79 77.41	7 4.93E-				
122			1 3.37E-0	05 26	9 36.78						9 5.95E-			-	
124			6 4.2E-0	05 27										-	
126													-	-	
128															
130											2 0.0001			+	+
132											1 0.0001			-	
134											4 0.0001		-	-	-
136											6 0.0001			-	
138															
140											7 0.0001			1	
142											6 0.0001				
144											0.0001				
148											0.0001				
140	200.000	1 00.7	0.272	29							0.0001				
	<b></b>				9 234.71		17 2.68E-0				-091	3			
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	N-IGNIT	TON COR	E2		-							
Depth	(cm)	LOI %	Depth (cm)	LOI%	Depth (cm)	LOI%	Depth (cm)	LOI%	Depth (cm)	LOI %	Depth (cm)	LOI%
	2	31.52 21.18	101	39.44	201	34.07	301	30.47	401	30.62	501	19.44
	3	21.18	102	38.30	202	31.74	302	27.82	402	29.75	502	7.47
	4	20.90	104	36.36 32.77	203	21.64	303	27.69	403	28.61	503	29.24
	5	21.98	105	27.36	204	11.16 31.36	304	32.04	404	29.07	504	38.73
	6	24.93	106	37.50	206	30.41	305	10.34 32.87	405	31.89	505	36.86
	7	26.89	107	33.89	207	28.88	307	32.05	406	22.64	506	17.91 3.57
	8	30.34	108	32.45	208	30.63	308	29.10	408	29.02	508	29.78
	10	30.34	109	27.51	209	29.47	309	32.12	409	31.89	509	44.37
	11	31.90 32.02	110	27.75	210	26.09	310	27.47	410	30.58	510	41.57
	12	35.86	111	39.58	211	21.64	311	33.24	411	29.17	511	29.08
	13	34.64	113	33.24 38.76	212	28.57	312	35.48	412	18.85	512	26.49
	14	35.80	114	37.77	214	27.95 29.33	313	31.23	413	29.23	513	32.65
	15	35.77	115	37.28	215	28.57	315	34.59 32.94	414	31.96 28.53	514 515	7.77 29.95
	16	36.18	116	38.36	216	27.78	316	31.64	415.5	1.69	516	33.89
	17	35.51	117	38.76	217	28.38	317	29.91	416	11.36	517.5	23.51
	18	35.63	118	32.35	218	5.37	318	32.99	417	30.60	518	2.78
	20	35.12 34.76	119	37.99	219	5.15		30.25	418	29.15	519	4.41
	21	35.37	121	35.25 38.10	220	26.83		28.49	419	28.66	520	12.90
	22	35.14	122	36.33	222	26.17 4.74		32.12	420	30.79	521	23.67
	23	36.04	123	33.82	223	11.07	322	33.91 34.38	421	28.86	522 523	2.91
	24	36.36	124	34.12	224	35.09		34.04	423	8.59		1.98
	25	35.69	125	35.16		16.74		34.29	424	11.86		3.25
	26	34.63	126	31.81	226	36.46	326	30.39	425	11.62		20.14
	27	35.25	127	34.47	227	37.61	327	32.02	426	21.74	527	3.19
	28	36.02 35.98	128	36.76		28.98		31.10	427	16.73	528	12.15
	30	31.91	129	35.88		3.43		33.02		19.27		11.83
	31	25.09	131	35.75		5.78		31.56		28.86		5.49
	32	23.98	132			5.65		31.62 35.61		29.18 32.12		1.96
	33	27.71	133			6.45		36.62		27.15		12.89
	34	33.69	134	31.42	234	6.65		35.61		31.85		1.96
	35	35.47	135			6.67	335	36.20		31.96		2.76
	36	37.10			236	9.26	336	38.35	435	26.90	536	17.6
	37	40.34	137			16.80		33.22		29.20	5 537	15.80
	39	37.80 38.60				21.79		32.16		33.7		2.40
	40	36.64	140			30.75		35.3		32.5		4.0
	41	37.50				36.59		36.63		3.6		3.4
	42	38.42				37.38		31.0		7.7		4.5
	43	38.19				39.11		32.7		7.2		5.3
	44	37.86				37.66		24.2		6.6		5.1
	45	37.64				34.0	1 345	31.8		8.0		4.9
	46	38.66				33.2		30.0		8.0		10.7
	47	40.31				33.5		29.1				5.1
	48	38.16				33.9		30.6		10.1		34.6
	50	37.25				27.8		33.6				38.2
	51	36.39				30.8		32.1 28.7				37.1 26.5
	52	37.58						28.5				5.5
	53	39.12										29.3
	54	37.88						29.6				22.9
	55	37.86		34.0				28.0				7.7
	56	35.90										28.3
	57	34.98										
	58	34.08										
	59 60	32.82										38.7
	61	31.58						34.5				
	62	29.09										
	63	30.53										
	64	33.8	16	4 28.2	4 264	38.6	8 364	32.6	9 463	27.2	.5	
	65	36.5								31.7	7	
	66	35.1										
	67	34.1										-
	69	34.4							6 467			<del>                                     </del>
	70	33.8										1
	71	34.3										
	72	34.2	0 17	2 27.3	7 271	30.8	34 372	15.4	5 47	37.0	05	
	73	31.5	3 17	3 25.6	4 272	32.5	373	20.7	8 472	30.3	32	
	74	28.9	8 17									-
	75	24.6										+
-	76	39.2										1
	77	40.5										+
	79	40.3										1
	80	38.1										
						28.4	40 381	16.	58 48	0 34.	53	
		36.6				1 33.7	72 382	30.	31 48	1 32.	17	
	81 82		4 18				49 383			2 42.	65	
	81 82 83	36.6 39.3 39.6	4 18 7 18	3 32.5	6 282							
	81 82 83 84	36.6 39.3 39.6 39.0	4 18 7 18 9 18	3 32.5 4 33.5	6 282 5 283	3 33.5	58 384					+
	81 82 83 84 85	36.6 39.3 39.6 39.0 40.2	4 18 7 18 9 18 3 18	3 32.5 4 33.5 5 31.7	66 282 55 283 78 284	3 33.5	58 384 92 385	30.	99 48	4 45.	78	-
	81 82 83 84 85 86	36.6 39.3 39.6 39.0 40.2 38.8	4 18 7 18 9 18 3 18 0 18	3 32.5 4 33.5 5 31.7 6 32.1	66 282 55 283 78 284 4 285	3 33.5 4 31.9 5 30.2	58 384 92 385 23 386	30.5 31.	99 48 86 48	4 45. 5 42.	78 77	
	81 82 83 84 85 86	36.6 39.3 39.6 39.0 40.2 38.8 34.2	4 18 7 18 9 18 3 18 0 18 9 18	3 32.5 4 33.5 5 31.7 6 32.1 7 34.4	66 283 55 283 78 284 4 285 15 286	3 33.5 4 31.9 5 30.2 6 31.5	58 384 92 385 23 386 52 387	30. 31. 7 31.	99 48 86 48 06 48	4 45. 5 42. 6 36.	78 77 09	
	81 82 83 84 85 86 87 88	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0	4 18 7 18 9 18 3 18 0 18 9 18 5 18	3 32.5 4 33.5 5 31.7 6 32.1 7 34.4 8 29.1	66 283 55 283 78 284 4 285 15 286	3 33.5 4 31.9 5 30.2 6 31.5 7 29.	58 384 92 385 23 386 52 387 13 388	30.5 6 31. 7 31. 8 30.	99 48 86 48 06 48 51 48	4 45. 5 42. 6 36. 7 40.	78 77 09 32	
	81 82 83 84 85 86 87 88	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0 38.7	4 18 7 18 9 18 3 18 0 18 9 18 1 18	3 32.5 4 33.5 5 31.7 6 32.7 7 34.4 8 29.	66 282 55 283 78 284 4 285 15 280 11 28	3 33.5 4 31.5 5 30.2 6 31.5 7 29.3 8 33.4	58 384 92 385 23 386 52 387 13 388 46 389	30.5 31.7 31.8 30.9	99 48 86 48 06 48 51 48 65 48	4 45. 5 42. 6 36. 7 40. 8 44.	78 77 09 32 66	
	81 82 83 84 85 86 87 88 89	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0 38.7	4 18 7 18 9 18 3 18 0 18 9 18 5 18 1 18 8 19	3 32.5 4 33.5 5 31.7 6 32.1 7 34.4 8 29.1 9 4.5	66 282 55 283 78 284 44 283 15 286 11 285 16 286	3 33.5 4 31.5 5 30.2 6 31.5 7 29.8 8 33.4 9 34.	58 384 92 385 23 386 52 387 13 386 46 389 18 396	5 30. 6 31. 7 31. 8 30. 9 29. 0 27.	99 48 86 48 06 48 51 48 65 48 27 48	4 45. 5 42. 6 36. 7 40. 8 44. 9 42.	78 77 09 32 66 96	
	81 82 83 84 85 86 87 88 89 90	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0 38.7 35.4	4 18 7 18 9 18 3 18 0 18 0 18 5 18 1 18 1 18 8 19	3 32.5 4 33.5 5 31.7 6 32.1 7 34.4 8 29.1 9 4.5 10 6.1	66 283 55 283 68 284 4 283 15 286 11 28 10 28 10 28 17 29	3 33.5 4 31.5 5 30.2 6 31.5 7 29.3 8 33.4 9 34.0	58 384 92 385 23 366 52 385 13 386 46 385 18 396 70 39	5 30. 6 31. 7 31. 8 30. 9 29. 0 27. 1 28. 2 29.	99 48 86 48 96 48 51 48 65 48 27 48 91 49	4 45. 5 42. 6 36. 7 40. 8 44. 9 42. 0 38. 1 37.	78 77 09 32 66 96 46	
	81 82 83 84 85 86 87 88 89	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0 38.7 35.4 33.8	4 18 7 18 9 18 3 18 0 18 9 18 5 18 1 18 8 19 9 19	3 32.5 4 33.5 5 31.7 6 32.7 7 34.4 18 29.1 19 4.5 10 6.1 11 6.5	66 282 55 283 68 284 64 283 65 286 61 28 66 28 67 29 68 29 68 29	33 33.5 4 31.5 5 30.2 6 31.5 7 29. 8 33.4 9 34. 0 33.1 1 32.1 2 22.	58 384 92 385 23 366 52 367 13 386 46 389 18 399 70 39 87 393 45 395	30. 31. 7 31. 8 30. 9 29. 0 27. 1 28. 2 29. 3 29.	99 48 86 48 06 48 51 48 65 48 91 49 90 49	4 45. 5 42. 6 36. 7 40. 8 44. 9 42. 0 38. 1 37. 2 29.	78 77 09 32 66 66 96 46 50	
	81 82 83 84 85 86 87 88 89 90	36.6 39.3 39.6 39.0 40.2 38.8 34.2 37.0 38.7 35.4	4 18 7 18 9 18 9 18 3 18 0 18 9 18 5 18 1 18 8 19 9 19	3 32.5 4 33.5 5 31.7 6 32.7 7 34.4 8 29. 9 4.5 0 6. 11 6. 2 9. 3 14.	66 287 55 288 8 284 4 288 55 281 11 28 15 281 6 281 6 281 67 291 100 291 100 291 101 291 102 291 103 291 104 291 105 291 106 291 107 291	33 33.5 4 31.5 5 30.6 6 31.5 7 29. 33.4 9 34. 0 33.1 1 32.1 2 22.3 3 30.5	58 384 92 385 23 386 52 38 113 381 46 389 18 399 70 39 87 399 45 39	5 30. 6 31. 7 31. 8 30. 9 29. 11 28. 22 29. 33 29. 4 29.	99 48 86 48 06 48 51 48 65 48 27 48 91 49 90 49 69 49	4 45. 5 42. 6 36. 7 40. 8 44. 9 42. 0 38. 1 37. 2 29. 3 27.	78 77 09 32 66 96 46 50 55	
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		RE 3									
epth (cm)	%LOI 30.52	Depth (cm)	%LOI	Depth (cm)	%LOI						
2	30.12	101.5	4.95 9.53	201	25.62	301	21.21	401	18.42	501	31.3059
3	29.03	102	11.84	202	24.06	302	23.96	402	37.18	502	30.06993
4	30.34	103	10.94	204	24.26	303	26.94 22.66	403	34.28	503	31.13924
5	30.29	104	10.53	205	24.41	305	18.28	404	35.78 36.49	504 505	18.9729
7	30.53		10.68	206	26.12	306	16.16	406	34.36	506	12.5498
8	30.72	106	13.26	207	25.00	307	18.05	407	31.23		
9	32.93	108	13.63 8.07	208	28.20 27.83	308	14.98	408	30.33		
10	32.00		13.38	210	24.92	309	27.38	409	27.30		
11	31.94	110	3.19	211	21.21	311	3.87 2.85	410.5	29,46 28,57		
12	29.50		26.64	212	17.87	312	3.66	411.5	20.67		
14	29.95 29.82		21.70	213	16.44	313	4.33	412.5	27.52		
15	29.29		15.05	214	18.23	314	7.38	413	25.89		
16	29.96		10.17	216	21.75	315	8.26	414	25.05		
17	30.29	116	8.03	217	9.00	317	22.89	415	19.61		
18	30.45		4.82	218	16.74	318	34.39	417	25.08		
20	30.17		5.11	219	19.90	319	36.28	418	10.93		
21	31.27		15.56	220	17.09	320	35.65	419	10.25		
22	30.48		11.03	221	20.79	321	33.67	420	32.72		
23	30.29		7.52	223	27.82 26.35	322	31.53	421	24.27		
24	30.53	122	11.19	224	27.84	324	30.68	422	24.82 35.01		-
25	31.65		11.16	225	26,20	325	29.72	424	32.73		
26	32.00		3.17	226	27.15		27.12	425	31.54		
27	31.47		1.76	227	24.13	327	30.00	426	34.47		
29	30.83		12.93	228	20.65		30.94	427	33.60		
30	29.74		14.21	229	19.96		26.00		3.54		-
31	29.15		18.50	231	11.94		27.27 26.24	429	9.61	-	-
32	29.15	130	15.15	232	9.90		26.46		11.62		
33	29.37		9.70	233	18.13	333	27.36		4.22		
34	30.43		12.03	234	23.73	334	27.98	432	8.39		
36	31.40		12.30	235	25.82		28.73		8.67		
37	29.73		12.28	236	24.04		27.09		12.66		-
38	27.89		0.93	237	28.29		25.17 16.51		10.80		-
39	26.91		0.70		24.11		8.03		13.29		-
40	26.77		1.39		20.82		6.58		3.2		-
41	27.78		0.45		15.27		13.28		3.9		
42	27.69		0.67	242	11.76		7.67				
44	26.58		0.48		24.32		17.73		4.8		-
45	26.52		0.65		28.77						-
46	25.28		3.81		33.99						1
47	25.55	144	23.16		30.00						1
48	26.75		24.67		24.69						
49	23.46		21.67		26.9		25.17	446.5			
50 51	21.10		22.22		30.29						
52	23.60		20.00		24.29						-
53	20.5		25.82 33.33		22.7						-
54			31.88		20.9						+
55	21.2				28.0						1
56	24.3				24.0						
57	23.8				21.9	3 356	23.3	4 454	12.6	2	
58	22.7				25.1						
59 60	16.5				27.9						-
61	13.1				27.4						-
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62											
63	18.4	9 160	23.7	264	28.9	6 363	15.8	8 461	9.4	3	
64						4 364	9.0	2 462	7.9	3	
65											-
66											+
68											+
69											-
70	4.6										
71	19.8	6 168	11.4	1 272	31.3	5 371	16.9	6 46	4.3	2	
72											-
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79	3.6	2 17€	13.4	5 280	24.8	0 37	16.2	6 47	7 6.	70	
80.5											+
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87	13.1	7 184	16.9	5 288	16.3	38	6 24.7	2 48	5 16.	23	-
88											+
89		186									-
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95				8 297	7 23.8	30 39	4 9.3	36 49	3 2.	58	
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97					21.6						-
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	NITION COI	Depth (cm)	%LOI	Depth (cm)	9/101	D. II			
1	33.33	101	5.83	201	%LOI 32.14	Depth (cm)	%LOI	Depth (cm)	%LOI
2	32.61	102	3.52	202	31.33	301.5	10.45	401	7.95
3	30.82	103	8.37	203	30.79	303	23.74	402	5.93 4.83
5	29.91 31.17	104	23.21	204	29.74	304	10.83	404	0.96
6	30.61	105	30.79	205	30.69	305	23.43	405	0.86
7	32.95	107	27.51 26.59	206	30.43	306.5	10.53	406	21.11
8	34.35	108	24.93	207	30.28	307	2.92	407	20.95
9.5	34.29	109	27.82	209	31.00	308	3.55	408	20.82
10.5	25.41	110	28.72	210	33.22	310	3.49 5.44	410	24.26
11	21.46	111	24.74	211	33.44	311	32.49	411	18.54
12	28.65 31.55	112	19.38	212	33.19	312	32.42	412	5.4
14	31.03	113	23.81	213	31.60	313	27.88	413	7.6
15	32.88		25.98 25.77	214	31.99	314	31.33	414	6.7
16	32.83		22.04	216	30.89	315	29.17	415	4.50
17	32.71	117	20.27	217	34.28	316	27.43 17.39	416	4.9
18	33.69		19.08	218	36.47	318	26.32	417	3.6
20	30.80		8.61	219	36.33	319	28.37	419	3.2
21	29.21 31.56	120.5	14.61	220	35.36	320	33.03	420	2.7
22	31.90		7.59	221	34.28	321	32.14	421	2.3
23	32.11	123	16.20	222	34.69	322	31.48		2.3
24	31.52		26.24	224	33.82	323	30.74	423	2.7
25	31.48		23.47	225	32.00	324	33.05		2.4
26	28.92	126	2.91	226	30.67	326	29.25 31.33		1.4
27	29.38	127	3.84	227	30.71	327	29.57		1.2
28	24.41	128	2.62	228	31.83	328	30.40		1.2
30	17.52		5.89	229	32.51	329	30.15	429	0.8
31	22.94		7.15	230	28.82		35.71	430	0.8
32	39.18		14.89	231	24.83		37.66		0.9
33	40.24		31.74	232	23.40		28.75		1.2
34	36,77	134	31.97	234	26.79		42.19		1.2
35	33.33	135	33.45	235	22.04		38.55		1.1
36	34.52		32.14	236	20,45	336	35.12		1.2
37	34.11		32.33	237	29.13		30.61	437	1.7
39	37.23		29.90		29.07		20.64		1.7
40	35.39		26.98 28.57	239	27.09		15.52		1.5
41	28.29		27.46	240	28.12		20.31		0.9
42	25.84	142	24.13		28.57		19.91		0.9
43	25.76		18.97		27.21		12.92		0.9
44	27.7		17.33	244	25.67		8.95		0.8
45	23.5		30.56		16.60		13.47		0.9
46	16.42		29.12		15.93		15.90		0.9
48	27.70		31.48 26.28		12.85		11.72		1.0
49	26.48		28.57		28.04		5.97		2.9
50	20.65		28.21		26.20		7.68		1.2
51	14.23		20.35		23.4		9.1		1.3
52	16.1	152	24.94		25.78		6.4		0.9
53	22.2		27.32	253	25.64		15.0	2 453	1.5
54	20.7		30.11		18.9		20.7	7 454	1.0
55	23.3		28.33		29.63		15.4	7 455	1.0
56 57	25.4		16.67		32.2		10.3		1.0
58	25.3		17.91 27.56		32.3		15.3		1.1
59	24.8		22.42		29.8		6.8		0.8
60	27.7		20.31		29.4		4.7		0.6
61	23.5		24.19		26.6		3.1		0.6
62	22.9	162	28.88	262	29.1		5.2		0.4
63	25.1		23.76		29.0	363	3.0		0.9
64	27.3		24.60		30.7		2.9		
65	25.8		15.83		30.7		4.6		
66	18.7		26.33		29.6		3.8		
68	24.7		12.95	267	30.6 25.1		1.5 3.0		
69	28.5		8.68		3.6		2.7		
70	27.6	6 170	12.39	270	20.8		3.5		
71	27.6	8 171	29.0	271	27.9		4.1		95 200
72	27.8		29.46		28.4		2.6	5	81 1118
73	27.3		27.30		27.3		1.8	3	25 (1)
74			24.24		25.6		2.2		
75 76			13.64		25.6		2.8		
77			23.0		18.6		3.1		
78			30.0		30.3		2.7		
79			29.4		29.6		5.9		84,
80			29.3		30.3		13.9		21
81			23.3		30.1	2 381	21.4	0	110000
82			19.0		27.8	1 382	13.5	2	19444170
83			17.9		8.9		9.4	7	
84			28.4		8.3		10.6		
85 86			12.6		13.0		12.4		Malayana (II)
87			27.8		31.2		15.4		
88			31.9		29.9		14.5		
89			30.5		24.9	3 389	5.8		200000
			29.3	3 290	19.7	4 390	22.2		2 2 2 2 2
90	20.5	1 190	26,9	5 291	3.1	6 391	19.1	8	Til meriligi
	18.2	2 191	25.0	8 292	4.1	1 392			
90 91 92	04 2		23.1		3.8				
90 91 92 93			7.6	7 294	3.4		1.1	1	
90 91 92 93	24.6					A		00	
90 91 92 93 94	24.6 25.1	3 193	14.4	9 295	5.1				-
90 91 92 93 94 95	24.6 25.1 22.7	3 193 3 194	14.4 30.3	9 295 7 296	13.8	7 396	4.3	32	
90 91 92 93 94 95 96	24.6 25.1 22.7 20.5	3 193 3 194 8 195	14.4 30.3 31.7	9 295 7 296 3 297	13.8	7 396 1 397	4.3	32 36	
90 91 92 93 94 95 96 97	24.6 25.1 22.7 20.5 5.6	3 193 3 194 8 195 0 196	14.4 30.3	9 295 7 296 3 297 6 298	13.8	7 396 1 397 0 398	4.3 4.3 1.3	32 36 33	
90 91 92 93 94 95 96	24.6 25.1 22.7 20.5 5.6 5.5	3 193 3 194 8 195 0 196 4 197	14.4 30.3 31.7 30.1	9 295 7 296 3 297 6 298 7 299	13.8 14.0 21.8	7 396 1 397 10 398 15 399	4.3 4.3 1.3 12.3	32 36 33 32	

-		ogen Data -	CORE 2														
	% nitrogen	% carbon	Depth (cm)	% nitrogen 9	6 carbon	Depth (cm)	% nitrogen	9/ norther	Death ( )								
1 2	1.26 0.66	16.75	101	1.44	18.69	201	1.11	16.47	301	% nitrogen	% carbon 14.88	Depth (cm)	% nitrogen 1.08			% nitrogen	% carbon 7.8
3			102	1.29	17.99	202	1.10	14.96	302	1.00	13.36	401	1.03		501 502	0.54	2.9
4	0.55	10.00	104	1.12	16.23	203	0.65	9.54	303	1.01	14.51	403	1.20	14.50	503	1.01	14.4
5			105	1.04	14.87	204	0.99	4.11	304	0.20	15.68	404	1.28		504	1.42	20.3
7	0.81		106	1.28	17.88	206	1.01	14.15	306	1.13	16.27	405	1.29 0.85		505 506	0.69	18.2
8			107	0.91	15.40	207	1.03	14.78	307	1.17	15.75	407	0.78		507		1.0
9			109	0.87	12.81	208	0.87	15.12	308	1.04	14.63	408	1.08		508	0.78	10.6
10			110	1.10	15.86	210	0.77	11.30		0.74	14.43	409	1.31		509	1.64	24.1
11			111	1.34	18.68	211	0.64	10.04	311	1.11	15.63	410	1.29		510 511		17.5
13	1.20	16.57	113	1.27	16.31	212	0.75	10.76		1.17	16.69	412	1.31	14.05	512	0.56	7.5
14			114	1.11	17.24	214	0.81	10.28		1.04	14.67 16.45	413	1.26		513		12.9
15			115	1.23	17.50	215	0.95	12.78	315		16.36	414			514 515		15.4
17			116	1.35	18.36	216	1.06	13.10	316	1.07	14.63	415.5	0.08		516		12.
18	1.14	15.66	118	0.99	14.47	217	0.97	13.12			14.92	416	0.67		517	0.73	9.
19			119	1.26	18.43	219	0.22	2.91			16.05 13.25	417					1.
20			120	1.07	16.43	220	0.84	10.95	320		14.53	419	1.11				3.
22			122	1.20	16.66 17.21	221	0.22	12.94			14.79	420	1.33	15.95	521	0.75	12.
23	1.24		123	1.12	16.99	222	0.83	10.01				421					
24			124		16.56	224	1.49	16.95									10.
25 26			125 126		16.34	225	0.60	7.23	325	1.19	17.00	424		5.88	525		1.
27	1.25	16.93	127		16.62	226	1.23	17.19							526	0.65	
28	1.39		128	1.23	18.02	228	0.91	16.57 13.27									
29 30			129		17.67	229	0.14	2.15	329	1.03	15.92	428					
31			130		18.22	230	0.12	2.20	330	0.90	14.67	429	1.33	15.02	530	0.11	0.
32	0.88	13.63	132		14.42	231	0.15 0.15	2.78							531	0.09	
33	1.01		133	1.00	13.46	233	0.17	3.05									
34 35					15.35	234	0.19	3.70	334	1.21	18.47	433	1.33	15.57	534		
36					15.26 17.61	235	0.23	4.35	335	1.18	17.84	434	0.96	13.36	535	0.11	0
37	1.13	17.54	137		16.04	236	0.27	4.54 6.44									
38			138	1.34	17.01	238	0.67	10.89									
39 40					17.01	239	0.98	14.21	339	1.15	17.11	438					
41			140		15.76 16.69	240	1.06	15.17							540	0.08	
42	1.25		142		15.54	241	1.51										
43			143		14.44	243	1.56	17.80	343								
44					17.10 17.55	244						443	0.18	8 3.22	2 544	4 0.11	2
46					17.11	245	1.27	15.70									
47	1.24		147		16.51	247	1.25										
48					16.30	248	1.27	17.91	1 34								
49 50					16.64	249						448	0.2	5 4.9	2 54	9 1.18	19
51					13.15	250 251	0.54										
52	1.2		152		16.79	252	0.96										
53					17.02	253			0 35	3 1.04	15.6	1 452					
54 55					15.49	254									1 55	4 0.8	
56					16.35	255 256											
57			157	1.07	15.42	257											
58					14.50	258			1 35	8 1.18		7 45	7 1.2	6 15.8	2 55		
59 60					11.73 8.44	259										0 1.2	16
61					14.62	260										+	-
62	0.6	10.7	6 162	1.19	16.54	262						7 46				+	-
63				1.15	17.18	263			3 36	3 0.9	6 14.1	7 46	2 0.7	8 9.4	6		
6.4					10.24	264											-
66					4.14	265										-	+
67	1.0	15.6	167	0.27	5.06	267	1.32	17.0	9 36	7 0.9	5 14.5	6 46	6 1.3	16.3			
68					8.73	268	1.18		1 36	8 0.8	2 12.5	1 46	7 1.2	16.5	5		
69 70					13.78	269.5										+	+
71	0.9	15.8	2 171	0.93	13.66	270	0.13	2.3									+
72			3 172	0.74	11.00	271	1.14	16.4	8 37	2 0.4	9 7.3	0 47	1 1.3	18.3	13		
73					8.91	272										-	-
75						273										-	+-
76	1.3	3 19.0	5 176	0.24	3.93	275	1.17	16.1	4 37	6 1.1	1 15.1	9 47	5 1.4	17 20.8	30		
77					4.52							1 47	6 1.4			-	-
78 79					13.37											-	-
80					14.05												+
8.1	1.4		8 18	0.96	14.22	280	1.04	15.9	38	1 0.6	5 9.2	6 48	0 1.1	17 16.3	39		
82					12.43											-	-
83					13.90						5 16.2 4 15.5					-	+
8.5	1.4	2 19.2	7 18	5 0.85	13.35	28	1.09	15.2	8 38	5 1.0	6 15.9	0 48	4 1.6	61 22.2			
86	1.4	0 19.5	2 18	6 0.84	13.81	28	5 1.12	16.2	25 38	1.0	0 16.1	3 48	5 1.4	44 20.3	30		
87					13.44												-
88			_													-	-
90																-	1
91	1 1.1	3 15.9	5 19	1 0.17	3.25	29	1.20	16.6	31 39	1 0.9	4 14.5	68 49	0 1.3	39 19.	03		
92																_	-
93														86 11. 96 13.		-	+
94													-			-	+
96		2 12.6	7 19				5 1.0	16.6	37 39	1.0	15.	19 49	1.	09 14.	97		
97	7 1.3	5 17.8	0 19	7 0.86	12.03	29	6 1.2		38 39	7 1.1		30 49	0.				+
9.6														53 8. 20 2.		-	+-
	1.4															-	+
100	0 1.4	9 19.3	4 20	0 1.10		29											

epth (cr	(cc)	wet density	% water	original %water (LOI)	dry density	average dry density	Depth (cm) D	
	5 1.2		73.33	83.6	0.327	0.327	188	-30.43
	5 1.2		89.25	89.2	0.111	0.114	189	-26.82
	5 1.2		89.16	89.2	0.117		190	-26.56
	3 1.2		88.02	88.6	0.138	0.126	191	-26.61
	3 1.2		89.01	88.6	0.113		194	-27.85
14		and the second second second	86.58	87.4	0.170	0.170	195	-31.72
19		The state of the s	85.11	85.4	0.166	0.169	228	-31.39
19		the state of the s	86.02	85.4	0.171		229	-27.58
27			83.54	83.0	0.239	0.241	230	-26.65
27			83.55	83.0	0.242		232	-26.58
30			84.01	83.3	0.209		233	-26.64
30			83.73	83.3	0.178		234	-26.73
34		1.453	77.91	75.2	0.321	0.295	235	-27.09
34		1.274	78.89	75.2	0.269		237	-28.0
39		1.136	83.27	81.2	0.190		238	-28.10
39		1.258	82.75	81.2	0.217		239	-29.80
39	1.0	1.183	82.33	81.2	0.209			
4:	28 1.0	1.217	84.22	86.0	0.192	0.187		
4:	28 1.0	1.167	84.40	86.0	0.182			
4	7 1.0	1.486	81.36	80.8	0.277	0.277		
41	33 1.0	1.284	82.87	82.9	0.220			
4	33 1.0	1.161	80.53	82.9	0.226			
5	1.0	1.214	81.71	82.4	0.222	0.222		
5	51 1.2	1.128	80.95	80.8	0.215			
5	58 1.0	1.012	82.41	82.5	0.178			

Depth (cm)	% carbon	Depth (cm)	% carbon	Depth (cm)	% carbon	Depth (cm)	% carbon	Depth (cm)	% carbon
40	1.23	179	1.25	232	0.22	290	2.06	445	0.31
41	1.40	180	1.29	233	0.24	335	2.39	446	0.32
42	1.48	181	1.32	234	0.21	336	2.16	447	0.34
43	1.86	182	1.37	235	0.26	337	1.36	448	0.36
44	1.48	183	1.48	236	0.26	338	1.33	449	0.26
45	1.81	184	1.42	237	0.34	339	1.31	450	2.15
46	1.98	185	1.12	238	0.67	340	1.45	451	2.14
47	1.82	186	1.24	239	1.02	341	1.33	452	2.04
48	1.93	187	1.17	240	1.15	342	0.73	536	0.90
49	1.45	188	0.81	241	1.55	343	1.23	537	0.96
50	1.75	189	0.29	275	2.12	344	0.70	538	0.04
51	1.08	190	0.20	276	1.90	345	0.77	539	0.16
52	1.45	191	0.20	277	2.08	346	0.74	540	0.1
53	1.29	192	0.26	278	2.01	347	1.04	541	0.1
54	0.99	193	0.31	279	1.81	348	0.91	542	0.10
55	1.13	194	0.46	280	1.68	349	0.75	543	0.1
56	1.18	195	1.88	281	1.91	350	0.88	544	0.1
171	1.03	196	1.69	282	1.84	437	1.87	545	0.1
172	0.83	197	1.06	283	1.77	438	1.77	546	0.2
173	0.65	226	1.61	284	1.65	439	1.05	547	0.1
174	0.29	227	1.47	285	1.88	440	0.30	548	2.2
175	0.25	228	1.14	286	1.20	441	0.29	549	2.8
176	0.28	229	0.21	287		(2) 中国国际电子工业中的公司公司	0.24	550	3.2
177	0.28	230	0.37	288	2.25	443	0.27	7	
178	0.37	231	0.23	289	2.03	444	0.26	6	

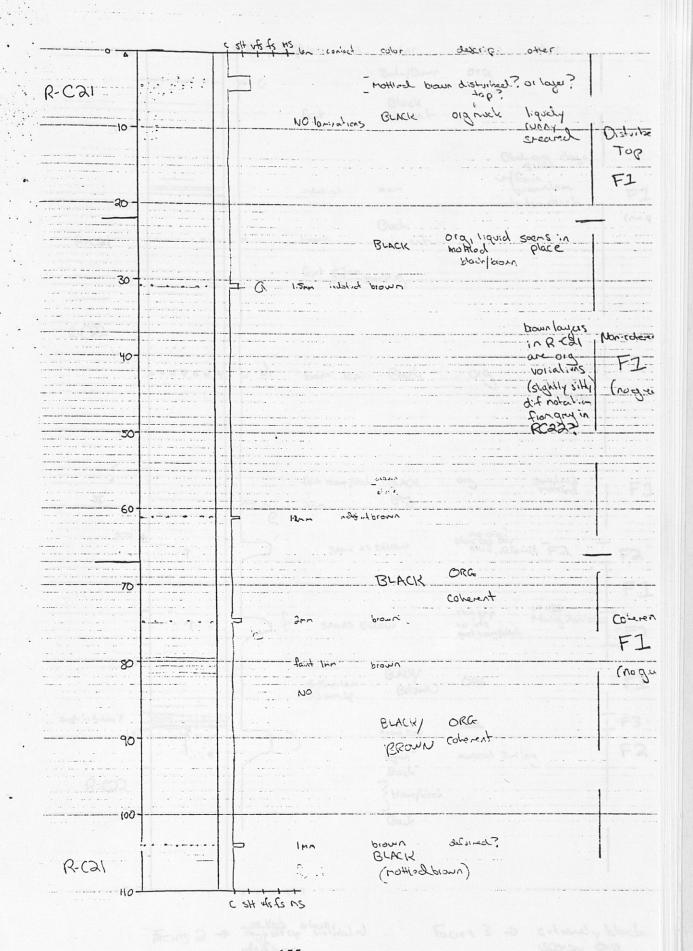
		-CORE 2									
Depth (cm) D	ensity 177.17	Depth (cm)		Depth (cm)		Depth (cm)	Density	Depth (cm)	Density	Depth (cm)	Density
	179.79	101			134.03	301	139.31		149.53		48.476
	185.53		159.03	202	130	302		402	140.71	502	107.5
	186.87		157.63 152.92	203	121.38	303			152.29		112.24
5	187.1	105		204	112.78	304		404		504	
	187.01	106		205	59.548	305			113.72		53,418
	187.15	107		206			154.65		120.71	506	42,594
	187.06	108				307			140.17	507	96.96
	187.14	109			126.58	308			141.35	508	106.92
	187.13	110			124.92		140.83	409		509	98,666
	187.06	111			115.24	310	158.24	410	148.5	510	
	187.11	112			116.62	311		411		511	_
13	187.09	113		213	127.33	312		412		512	43,013
	187.04	114		214		313		413		513	86.43
	187.08	115		215		315		414		514	100.77
16	187.02	116		216		316		415		515	99.79
17	187	117		217		317		417	125.13	516	
18	186.99	118		218						517	
19	187	119		219				419		518 519	
20	186.99	120	170.17		51.945	320			61.201	520	
21	187	121	168.9	221				421	20.078	521	30.618
22	187	122	159.9	222						522	
23	187	123		223	79.151	323				523	
24	187	124		224	65.525					524	
25	187	125		225	118.26	325					
26	187	126		226			144.83		129.18		25.235
27	187	127		227			141.83				
	186.94	128							150.09		
	186.21	129						429	146		
	183.13	130							135.79	530	
	175.79	131			26.842					531	
	175.49	132			23.537						
	176.11		162.67		27.759				132.01	533	17
	177.75	134			28.489				133.78	534	
	169.66		126.21		31.503						
	175.06										
	175.96										
39	189.71										
40	199.24										
41	202.37				150.69		152.2		20.48		
42	203.57				1 147.50						
43	203.92				162.3		2 141.0				
44	203.97				1 173.7		4 144.3	44	18.38		
45	203.77				176.0	6 34	144.3	2 44			
46	203.6										
47	202.96										
48	193.35										
49	175.41										
50	179.23						0 104.5		0 128.8		9 104.8
51	166.27				1 152.9		1 100.6		1 136.5		1 30.87
52	162.53				2 138.5		2 105.4		2 142.1		
53	155.84		3 147.4		3 119.9		3 128.7		3 140.5		
54	153.22										
55	155.23										
56	153.69										
57	151.86										
58	153.39										
59	149.6										
60	143.18										-
61	139.2										
62	134.6										
63	131.1										
64	121.7	1 16	4 120.0	3 26	4 118.7	1 36	4 157.0	2 46	4 147.7	1	
65	125.1	9 16	5 26.11	1 26	5 130.0	6 36	5 153.9	7 46	5 152.0	6	
66	129.9	5 16	6 18.81								
67	134.1										
68			8 65.64								
	136.0		9 106.5		9 93.64		9 125.7		9 139.7		-
	141.4		0 119.0		0 149.3		0 113.6		0 137.6		-
	154.2		1 127.2		1 156.1		1 97.37		1 123.0		-
	159.1		2 120.		2 160.2		2 149.5		2 126.3		-
	153.4	5 17	3 122.8	5 27	3 166.0		3 154.3		3 122.8		-
	137.2	5 17	4 86.89	6 27	4 157.8		4 149.7		4 136.7		-
	140.5		5 24.32		5 157.1		5 140.3	39 47	5 132.3	38	-
	165.2		6 19.3	27	6 171.0	37	6 152.6	47	6 129.5		-
	166.9		7 28.37		7 163.6		7 148.7		7 105	.4	-
	170.6		8 55.0		8 165.6		8 147.5		8 123.		-
	174.5		9 116.8		9 151.7		9 106.0		9 110.		-
	171.8		127.3		159.7		1 116		100.		+-
	168.1		1 130.5		1 160.7		116.9		1 115.		-
	169.5		135.2		159.8		32 132.0		32 130.		+
	170.1		134.1		3 158.5		33 133.		138		-
	167.8		130.9		163.7		136.		34 136. 35 129.		-
	173.5		139.1		5 155		145.				+
	186.8		36 132.7		6 146.9		36 147.		36 126. 37 134.		-
	193.6		37 132.2		157.		124				+
	182.9		136.5		161.		88 145.				-
	168.2		39 144.0		9 158.		150.		89 133.		-
	147.		55.64		0 152.		90 154		90 126.		
	147.		19.28		97.9		91 149.		91 122.		-
	147.1		25.32		92.2		92 146.		92 105.		-
	138.7		93 40.05		3 115		93 152.		93 110.		-
			94 52.42	21 29	129	.6 3	94 152		94 108.		-
94		7 19	95 91.74	11 29	115.		95 147.		95 67.2		
95	131.4										
95 96	141.6		96 119.2		6 127.		96 120.		96 55		-
95 96 97	141.6	88 19	97 12	24 25	146.	47 3	97 139.	46 4	97 98.2	23	1
95 96 97 98	141.6	8 19 8 19		78 29		47 <u>3</u> 05 <u>3</u>		46 4 27 4		23 06	=

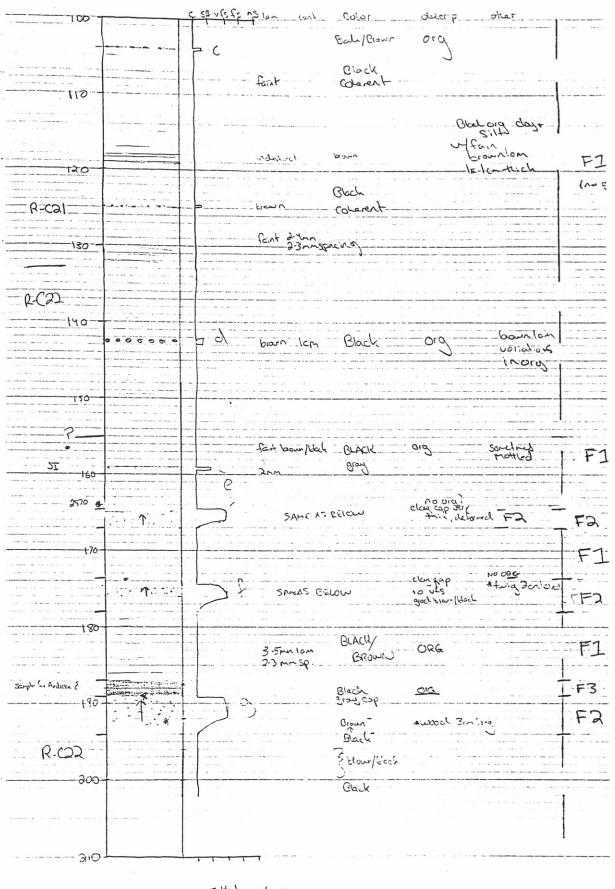
GRAIN SIZE DAT	The second secon									
CORE 2 - Layer i Sample #							-			CANADA DI MATERIA
Mean:	229	230	231	232	233	234	235	236	237	238
Median:	26.49 13.99	41.02	46.67	45.78	47.71	48.64	41.87	44.05	47.82	50.22
D(3,2):	4.08	30.1	35.09	34.51	35.42	36.42	32.1	31.56	34.85	36.9
Mode:	14.94	6.919 37.96	7.534	7.386	7.357	7.538	6.9	6.708	7.228	11.03
S.D.:	40.96	39.82	50.23	50.23	50.23	55.14	50.23	50.23	55.14	60.52
C.V.:	154.7	97.08	42.84 91.79	41.84	44.49	44.6	35.67	42.43	45.47	44.13
Skewness:	4.195	2.756	2.134	91.4 2.125	93.24	91.68	85.2	96.32	95.09	87.87
Kurtosis:	22.79	13.81	8.207	8.294	2.115	1.982	1.302	2.112	2.131	1.247
% <			0.201	0.294	7.778	6.925	1.614	7.324	7.844	1.106
10	2.864	6.453	6.882	6.774	6.708	6.735	0.050		0.000	
25	6.641	14.75	16.38	16.14	16.15	16.31	6.052	5.842	6.336	6.781
50	13.99	30.1	35.09	34.51	35.42	36.42	14.61	14.07 31.56	15.38	16.25
75	28.55	54.77	64	62.89	65.84	67.96	59.57	60.94	34.85 66.59	36.9
90	56.37	87.76	101.4	99.39	104.8	107	92.31	98.57	106.5	71.71 115.9
							32.01	30.57	100.5	110.5
						/olume V	olume \	olume V	olume V	olume
Diameter(µm) 1					% 9	6 9	6 9	6 9	6 %	
2	3.03 11.29	1.21	1.16	1.19	1.19	1.2	1.34	1.37	1.29	1.22
5		4.2	3.97	4.02	4.08	4.1	4.64	4.85	4.4	4.35
20	45.1 24.58	26.78	23.34	23.66	23.41	23.06	25.54	26.23	24.19	23.36
50	8.35	37.05	34.27	34.53	33.11	32.13	34.15	32.77	31.76	30.46
125	2.91	24.68	29.63	29.29	29.99	31.09	28.48	27.28	29.85	31.12
250	0.69	0.409	5.26 0.37	4.93	5.72	6.02	3.66	4.87	5.92	7.88
500	0.0031	0.0026	9.90E-05	0.321	0.446 0.0018	0.401	0.0017	0.376	0.506	0
1000	0	0.0020	9.902-05	0.0018	0.0018	0.0015	0	0	0.0016	0
2000	0	o	0	0	0	0	0 0	0	0	0
						,	0	J	0	- 0
CORE 2 - layer										
Sample#	440	441	442	443	444	445	447	448	449	
Mean: Median:	27.93	45.7	46.48	46.76	47	48.37	48.74	50.92	68.03	
D(3,2):	16.23	33.63	34.47	34.36	34.59	35.76	35.43	37.28	55.92	
Mode:	4.379	7.264 50.23	7.353	7.501	7.358	7.471	7.341	7.552	9.364	
S.D.:	16.4 36.39		50.23	50.23	50.23	55.14	55.14	55.14	87.9	
C.V.:	130.3	43.58 95.36	43.77	44.58	44.08	45.15	46.3	47.59	56.29	
Skewness:	3.629	2.344	94.17 2.24	95.34 2.28	93.78	93.33	94.98	93.47	82.74	
Kurtosis:	19.48	9.813	8.705	8.568	2.063	2.054	2.1	1.919	1.34	
% <	10.40	3.013	0.705	0.500	6.972	7.203	7.453	5.947	2.75	
10	3.325	6.418	6.617	6.773	6.54	6.627	6.549	6.702	8.778	
25	7.552	15.38	15.88	16.01	15.74	16.07	15.85	16.4	23.24	
50	16.23	33.63	34.47	34.36	34.59	35.76	35.43	37.28	55.92	
75	33.53	62.59	63.59	63.4	64.82	67.11	67.45	71.25	98.99	
90	63.28	99.84	101.1	101.6	103.5	107	108.9	113.9	143.5	
	Volume	Volume	Volume						Volume	
Diameter (µm)	2.48	%	%						%	
. 2	9.88	1.26 4.35	1.22 4.18	1.17	1.24	1.23	1.23	1.22	0.999	
5	41.86	24.54	23.86	4.07 23.95	4.24 23.96	4.18 23.35	4.22	4.13	3.08	
20	27.61	33.72	33.85	34.16	33.13	32.43	23.65 32.11	22.77 30.99	16.21 23.98	
50	11.74	28.63	29.21	28.85	29.4	30.29	29.79	31.13	39.15	
125	2.52	4.97	5.16	5.24	5.52	6.03	6.41	7.21	13.97	
250	0.392	0.472	0.481	0.579	0.458	0.478	0.516	0.544	0.951	
500	0	0.0026	0.0012	4.60E-05	0	6.90E-05	0.0021	0.0013	0.0024	
1000	. 0	0	0	0	0	0	0	0	0	
2000	0	0	0	0	0	0	0	0	0	
CORE 2 layer t		F00	F.10							
Sample # Mean:	538 32.27	539 44.22	540 49.52	541 50.77	542 49.79	543 46.92	544 49.23	545	546	547
Median:								62.7	60.98	72.91
D(3,2):	19.14 4.68	33.29 7.119		39.39 7.716	38.11 7.524	35.01 7.118	36.7 7.19	49.36 8.483	47.45 8.275	63.02 9.746
Mode:	18			60.52	55.14	55.14	55.14	80.08	72.95	96.49
S.D.;	40.23			44.45	43.79	42.96	45.11	53.98	53.79	57.06
C.V.:	124.6			87.55	87.94	91.56	91.63		88.22	78.26
Skewness:	3.436				1.631	1.925	1.856		1.566	1.211
Kurtosis:	17.57			5.173		6.374	5.536		3.737	2.423
% <	3.95	6.619	7.068	7.272	6.995	6.487	6.676	8.068	7.494	9.554
10 25						15.7	16.36			27.11
50							36.7			63.02
75							68.77			105.4
90							108.9		132.8	148.7
				Volume	Volume	Volume	Volume	Volume	Volume	Volume
	Volume %	Volume %	Volume %	Volume %	Volume %	%	%	%	%	%
Particle										
Diameter(µm)	1 0									
Diameter(μm) 1	1.9	4.08								
Diameter(µm) 1 2	7.98			21.08	21.94	23.84	22.0	18	18.86	14.04
Diameter(µm) 1 2 5	7.98 38.47	24.45	21.85							
Diameter(µm) 1 2 5 20	7.98 38.47 29.59	24.45 34.96	21.85	31.81	31.86	32.57	31.9	26.31	26.43	21.53
Diameter(µm) 1 2 5	7.98 38.47 29.59 15.33	24.45 34.96 28.58	21.85 32.63 32.05	31.81 33.61	31.86 32.42	32.57 30.16 5.48	31.9 31.08 6.37	26.31 36.93 11.74	26.43 36.18 11.02	21.53 42.14 15.88
Diameter(μm) 1 2 5 20 50	7.98 38.47 29.59 15.33 2.92	24.45 34.96 28.58	21.85 32.63 32.05	31.81 33.61 6.27 0.404	31.86 32.42 6.43 0.272	32.57 30.16 5.48 0.338	31.9 31.08 6.37 0.416	26.31 36.93 11.74 0.819	26.43 36.18 11.02 0.84	21.53 42.14 15.88 0.972
Diameter(µm) 1 2 5 20 50 125	7.98 38.47 29.59 15.33 2.92 0.578	24.45 34.96 28.58 4.26 0.309	21.85 32.63 32.05 6 0.455	31.81 33.61 6.27 0.404	31.86 32.42 6.43 0.272	32.57 30.16 5.48 0.338	31.9 31.08 6.37 0.416 2.30E-05	26.31 36.93 11.74 0.819 6 8.40E-05	26.43 36.18 11.02 0.84 0.0017	21.53 42.14 15.88 0.972 0.0038
Diameter(μm) 1 2 5 20 50 125 250	7.98 38.47 29.59 15.33 2.92 0.578 7.60E-05	24.45 34.96 28.58 4.26 0.309	21.85 32.63 32.05 6 0.455 6.90E-05	31.81 33.61 6.27 0.404 0	31.86 32.42 6.43 0.272 0	32.57 30.16 5.48 0.338 0	31.9 31.08 6.37 0.416 2.30E-05	26.31 36.93 11.74 0.819 6 8.40E-05	26.43 36.18 11.02 0.84 0.0017	21.53 42.14 15.88 0.972 0.0038

GRAIN SIZE DAT	A								
CORE 3 layer i								and the second	-117
sample #	134	135	136	137	138	139	140	141	142
Mean:	91	124.2	157.4	142.5	173.5	183	161.4	189.8	196.3
Median:	68.52	106.5	133.4	121.2	148.3	156.6	132	152.7	158.3
0(3,2):	10.86	14.72	17.22	15.6	17.09	18.2	15.87	16.76	17.34
Mode:	127.6	140.1	153.8	153.8	185.3	185.3	168.8	223.4	223.4
S.D.:	80.67	109.5	138.5	128.8	151.1	156.4	146.8	182.2	188.8
C.V.:	88.65	88.15	87.99	90.39	87.11	85.47	90.95	96.02	96.19
Skewness:	1.344	3.151	2.644	2.851	2.376	2.137		2.202	2.02
Kurtosis:	1.865	21.07	12.47	15.12	10.06	8.149	2.184	7.707	6.397
% <				10.12	10.00	0.149	8.455	7.707	6.397
10	10.93	16.84	20.39	17.28	20.36	20.93	16.82	16.29	15.64
25	28.13	50.22	67.07	55.75	71.28	74.75			
50	68.52	106.5	133.4	121.2	148.3		56.01	54.82	
75	132.3	168.7	206.9	190.2	230.2	156.6	132	152.7	158.3
90	202.9	241.3	303.9	277.5		245.3	219.9	264.2	
		241.0	303.9	2/1.5	336.4	359.7	334.2	392	413.2
Particle	Volume	Volume	Volume	Volume	V-1				
Diameter(µm)			%			Volume	Volume	Volume	Volume
1	0.843	0.642			%	%	%	%	%
2	2.38		0.529	0.591	0.49	0.479	0.579	0.544	
5	13.56	1.66	1.42	1.62	1.39	1.36	1.67	1.67	
20	21.6	8.24	6.96	8.11	7.04	6.92	8.37	8.88	
50		13.28	9.98	11.66	9.66	9.29	11.46	11.57	12.1
	32.88	33.53	26.71	28.62	21.92	20.32	24.5	19.11	17.4
125	21.98	32.58	37.03	35.18	37.61	36.78	32.86	29.82	28.
250	5.28	8.08	14.06	11.49	17.68	20.21	16.6	22.46	23.5
500	0.01	0.716	2.07	1.45	2.88	3.39	2.72	4.2	5.1
1000	0	0.165	0.298	0.256	0.391	0.388	0.248	0.829	0.82
2000	0	0	0	0	0	0	0	0	
Core 4 layer i							•		
Sample #	126	127	128	129	130	131	•		
Mean:	34.63	39.07	55.3	51.93	49.01	47.27			
Median:	23.72	28.66	45.6	42.02	37.65				
D(3,2):	5.692	6.457	8.568	7.984	7.697				
Mode:	28.69	37.96	60.52	60.52	55.14				
S.D.:	36.95	37.56	46.76	44.13	44.35				
C.V.:	106.7	96.13	84.55	84.99					
Skewness:	2.947	2.591	2.008						
Kurtosis:	14.5	12.48	7.686						
% <	14.5	12.40	7.000	5.918	7.307	9.019			
10	4.684	5.846	8.37	7.00	7.000	0.546			
25				7.62					
50									
75		53.21							
90	75.65	83.89	112.8	108.4	104.9	103.3	3		
		1111	70010	225					
Particle	Volume	Volume	Volume	Volume	Volume	Volume			
Diameter(µm)		%	%	%	%	%			
1	1.79								
2									
5		28.22	17.27	19.46	22.0	23.9	9		
20	34.82	35.87	30.93	31.55	32.8	32.7	3		
50	18.49								
125									
250									
500	2.30E-05	) 0	0.004		8.40E-0	0.002	1		
500 1000							1		

(cm) 1	model depth	14C years	years	Depth (cm)	model depth	14C years	calendar years	Depth (cm)	model depth	14C years	calendar years	Depth (cm)	model depth	14C years	calenda
2	1 2	13 25	12 25	76	76	958	935	151	151	1903	1857	226	210	2513	257
3	3	38	37	77 78	77 78	970	947	152	152	1915	1870	227	211	2523	258
4	4	50	49	79	79	983 995	959	153	153	1928	1882	228	212	2532	259
5	5	63	62	80	80	1008	972 984	154	154	1940	1894	229			
6	6	76	74	81	81	1021	996	155	155	1953	1907	230			
7	7	88	86	82	82	1033	1009	156 157	156 157	1966	1919	231			
8	8	101	98	83	83	1046	1021	158	158	1978 1991	1931 1943	232			
9	9	113	111	84	84	1058	1033	159	159	2003	1956	233 234			
10	10	126	123	85	85	1071	1046	160	160	2016	1968	235			
11	11	139	135	86	86	1084	1058	161	161	2029	1980	236			
12	12	151	148	87	87	1096	1070	162	162	2041	1993	237			
13	13	164	160	88	88	1109	1082	163	163	2054	2005	238	213	2535	26
14	14	176	172	89	89	1121	1095	164	164	2066	2017	239	214	2550	263
15	15	189	185	90	90	1134	1107	165				240	215	2566	26
16	16	202	197	91	91	1147	1119	166			. 7467	241	216	2582	26
17		214	209	92	92	1159	1132	167			7144	242	217	2597	269
18		227	221	93		1172	1144	168	165	2081	2025	243	218	2613	27
19		239	234	94		1184	1156	169	166	2091	2037	244	219	2628	27
20		252		95		1197	1169	170	167	2100	2049	245	220	2644	27
21	21	265		96		1210	1181	171	168	2110	2061	246	221	2660	27
22		277	271	97		1222	1193	172	169	2119	2074	247	222	2675	27
23		290	283	98		1235	1205	173	170	2129	2086	248	223	2691	28
24 25		302	295	99		1247	1218	174				249	224	2706	28
		315	308	100 100 100		1260	1230	175				250	225	2722	28
26 27		328	320	1000000		1273	1242	176				251	226	2738	28
		340	332	100 Miles (100 Miles		1285	1255	177				252	227	2753	28
28 29		353		1 19 41 695		1298	1267	178		2139		The state of the s		2769	29
30		365 378		10/0-6		1310	1279	179		2148		2010/09/201		2784	29
31		391		120,000		1323	1292	180		2158				2800	29
32		403	381 394	100 000		1336		181		2167				2816	29
33		416		0.000		1348	1316	100100000		2177				2831	29
34		428				1361	1328	The state of the s		2187				2847	30
35		441				1373		184		2196				2862	
36		454		15 1 15 1 15		1386		100 100 100 100 100 100 100 100 100 100		2206				2878	
37		466		1000		1399		15.49-17		2215		A COLUMN TO STATE OF THE PARTY		2894	
38		479		10.000		1411	1378	18.76		2225				2909	
39		491				1436		120000000000000000000000000000000000000		2235	2220			2925	
40		504				1449						264		2940	
41		517		0.0000000000000000000000000000000000000		1462						265		2956	
42		529		E 5.93		1474						266		2972	
43		542				1487		100-000				267		2987	
44		554				1499		1000		2244	2232			3003	
45		567		1000000		1512				2254				3034	
46		580		C. 180 05-12		1525		10710100						3034	. 34
47		592		No. of the second		1537						The state of the		3050	32
48		605		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1550		The second						3065	
49		617				1562		100000						3081	
50		630		0 0000000000000000000000000000000000000		1575		A CHARLES						3096	
51		643		1 10 10 10 10		1588		6 C 089/2150						3112	
52		655		10 10 10 10 10		1600								3128	
53		668		48.00.00		1613								3143	
54		680				1625						278		3159	
55		693				1638				2340	235			3174	
56		706				1651								3190	
57		718												320	
58		731												322	
59		743												323	
60		756												325	
61		769												326	
62														328	
63		794						21			7 245	2 28		329	
64		806												331	
65				36											
66				4 (1				2.1				THE RESERVE OF THE PARTY OF THE		334	
67															
68								2 - 32 - 32				29			
69												29			
70				9 2007						246	5 251				
71				41,42.20											
72								10 No. 200 No.				29			
73										248	4 253				
74								SELECTION OF SERVICE S							
75												Section of the sectio			
,,		34.										30			

Depth (cm)	model depth	14C years	calendar years	Depth	model	14C	calendar	Depth	model	14C	calendar	Depth	model	14C	calendar
301	276	3518	3878	(cm) 376	depth 350	years	years	(cm)	depth	years	years	(cm)	depth	years	years
302	277	3533	3898	377	351	4672 4688	5365	451	413	6065	6920	527			
303	278	3549	3918	378	352	4703	5386 5406	452 453	414 415	6097	6950	528			
304 305	279	3564	3938	379	353	4719	5426	454	416	6130 6162	6980 7010	529 530			
306	280	3580	2050	380	354	4734	5446	455	417	6194	7039	531			
307	281	3596	3958 3979	381 382	355	4750	5466	456	418	6227	7069	532			
308	282	3611	3999	383	356 357	4766 4777	5486	457	419	6259	7099	533	478	8316	9299
309	283	3627	4019	384	358	4799	5506 5529	458 459	420	6291	7129	534			
310	284	3642	4039	385	359	4821	5553	460	421 422	6324 6356	7159 7188	535 536	479	0055	0040
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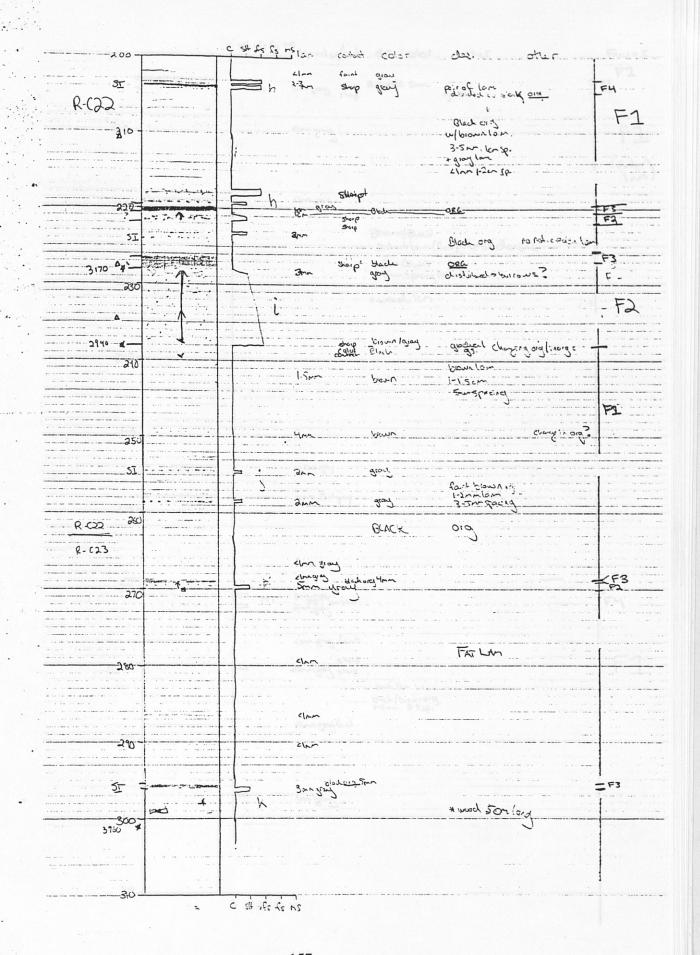




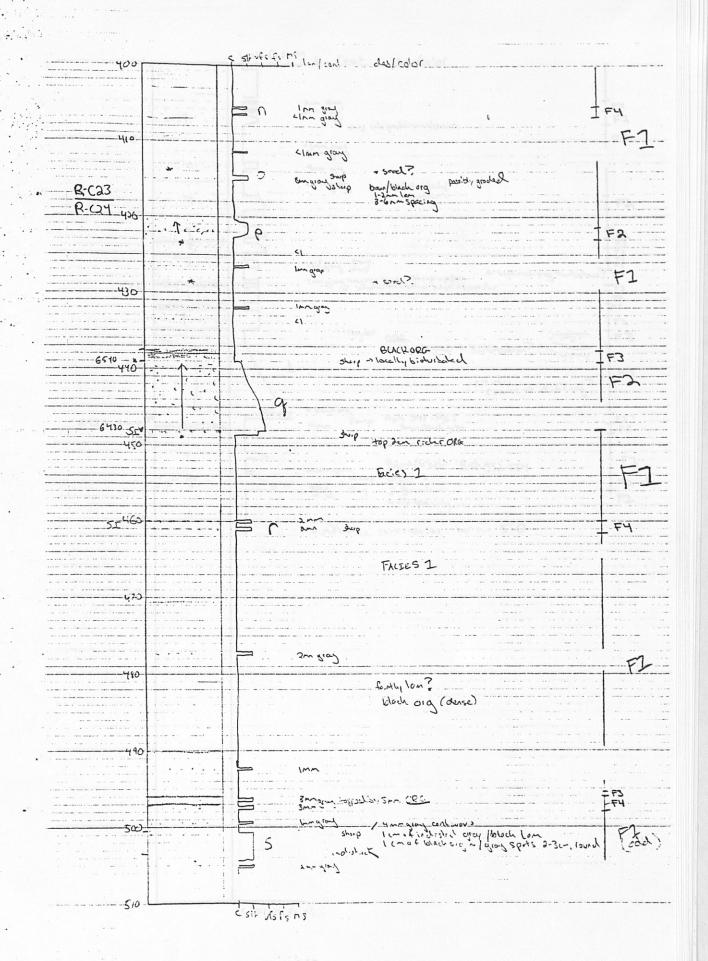
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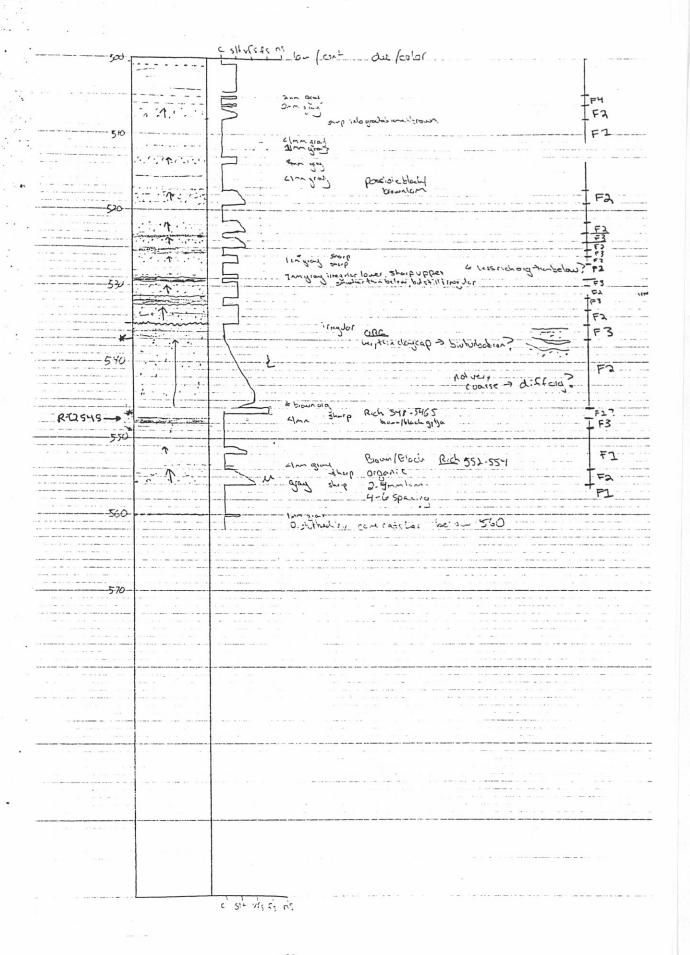
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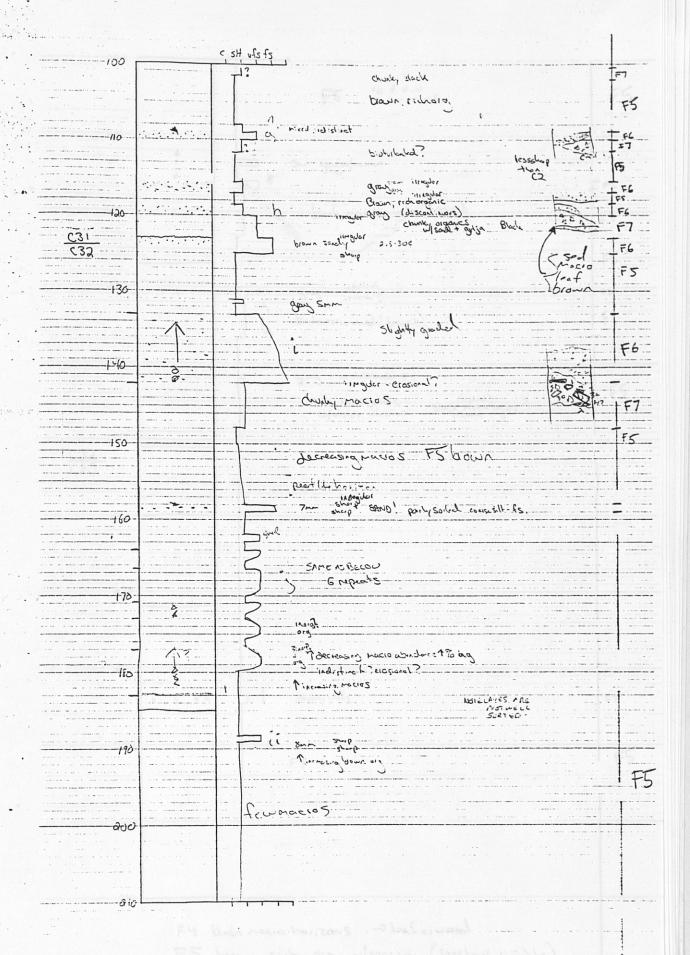


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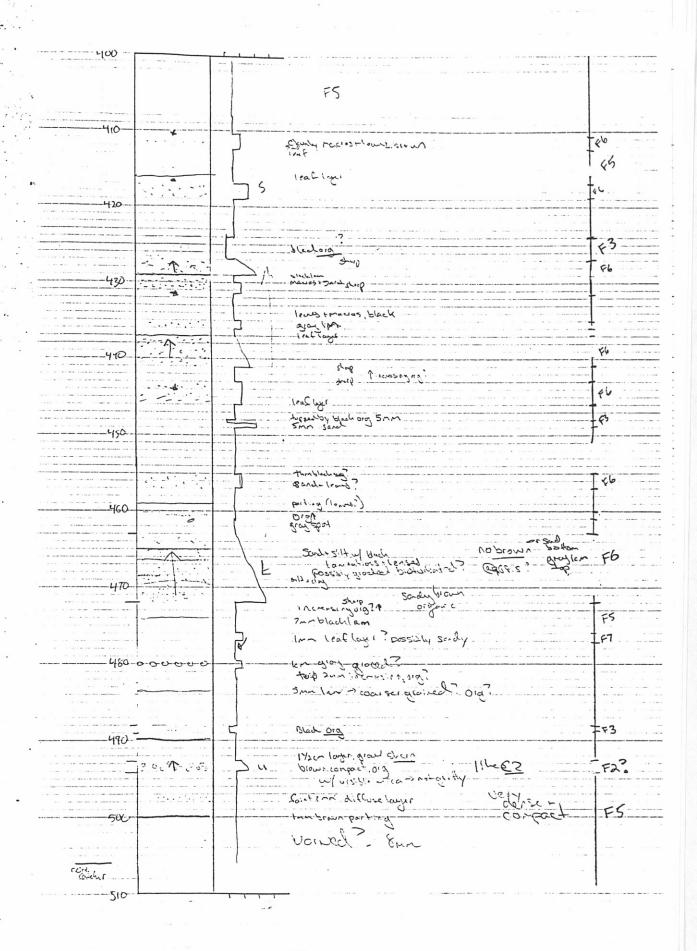


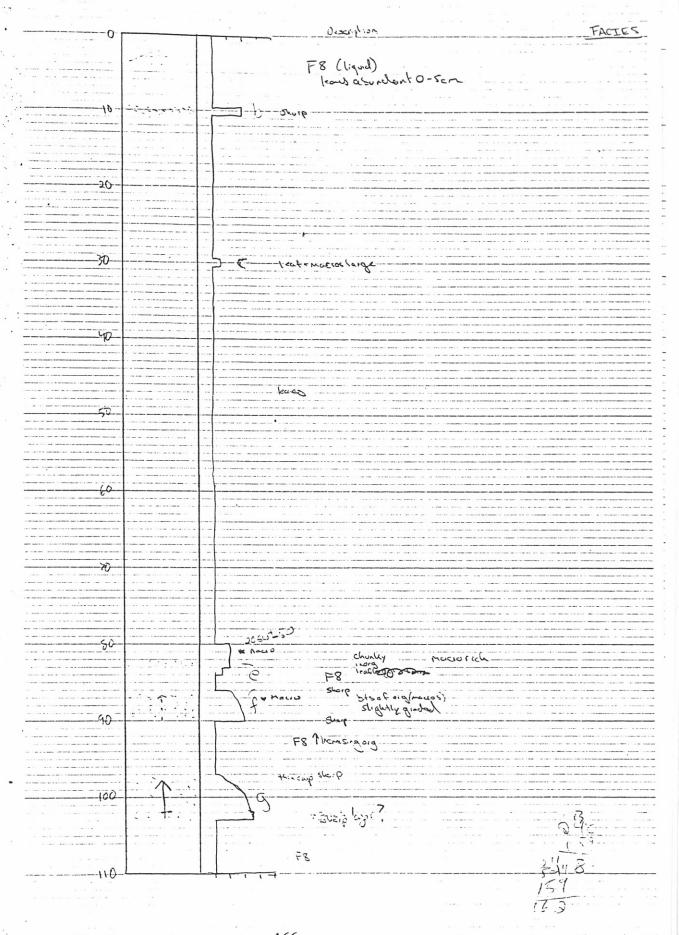
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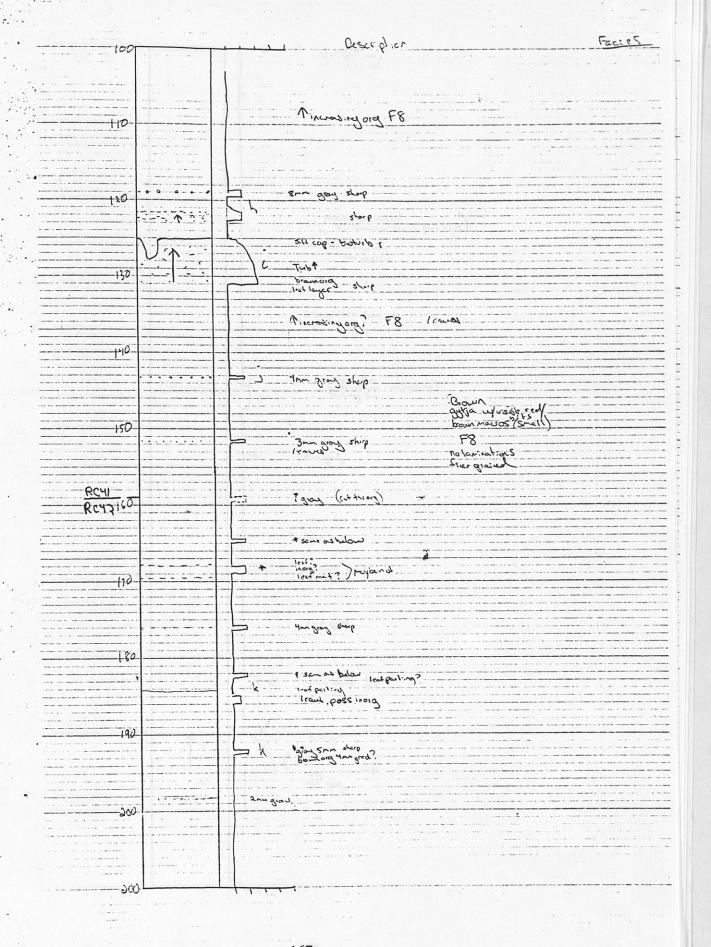


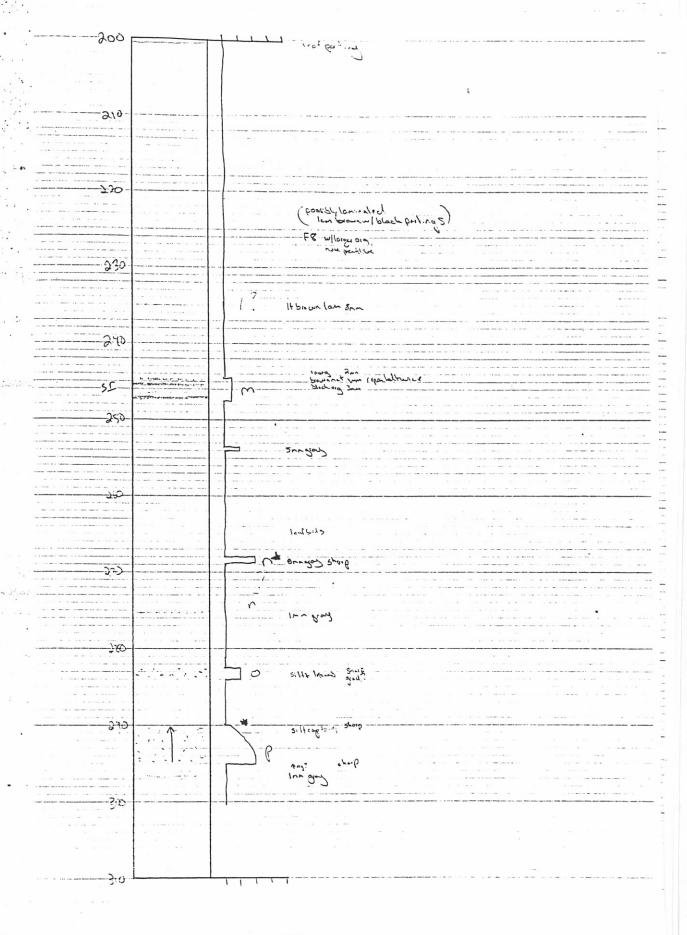
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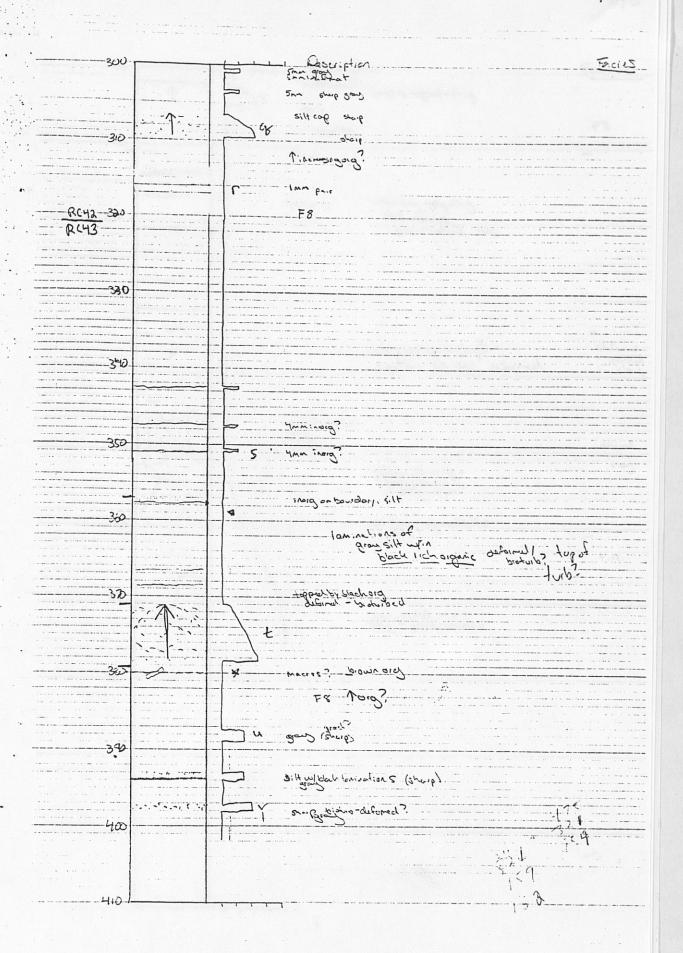
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